

Rules: Closed Book Exam: Please put away all notes and electronic devices

Reminders:

- Wherever possible, show equations you use to answer questions.
- We give **partial credit** for the various steps needed to solve a problem, so include equations and steps. If you combine steps, but you get the right answer, you still get credit for all the steps.

Equations Provided on the Exam:

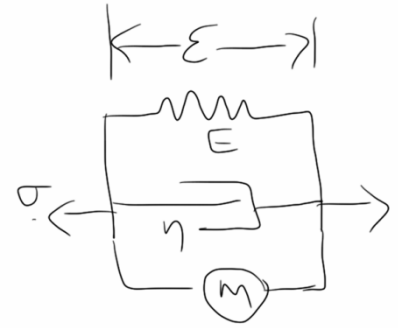
- $G = \frac{E}{2(1+\nu)}$
- $\sigma_{av} = \frac{\sigma_x + \sigma_y}{2}$
- $R = \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau^2}$
- $\sigma_{x\theta} = \sigma_{av} + \frac{\sigma_x - \sigma_y}{2} \cos(2\theta) + \tau \sin(2\theta)$
- $\tau_{\theta} = -\frac{\sigma_x - \sigma_y}{2} \sin(2\theta) + \tau \cos(2\theta)$
- $\sigma_{1,2} = \sigma_{av} \pm R$
- $\tau_{MAX} = R$
- $\epsilon_x = \frac{1}{E} \sigma_x - \frac{\nu}{E} \sigma_y - \frac{\nu}{E} \sigma_z$
- $\gamma_{xy} = \frac{1}{G} \tau_{xy} = \frac{2(1+\nu)}{E} \tau_{xy}$
- $\sigma_x = \frac{E}{(1+\nu)(1-2\nu)} ((1-\nu)\epsilon_x + \nu\epsilon_y + \nu\epsilon_z)$
- $\tau_{xy} = G\gamma_{xy} = \frac{E}{2(1+\nu)} \gamma_{xy}$
- $e = \frac{\Delta V}{V_0} = \epsilon_x + \epsilon_y + \epsilon_z$
- $\delta = \int_0^L \frac{N(x)}{E(x)A(x)} dx$
- $k_a = \frac{EA}{L}$
- $k_t = \frac{GJ_p}{L}$
- $k_c = \frac{3EI}{L^3}$
- $\int_A y^2 dA = I$
- $I = \frac{\pi}{4} r^4$
- $I = \frac{H^3 W}{12}$
- $I = \frac{H^3 W}{36}$, (neutral plane is at H/3 from flat edge).
- $\int_A r^2 dA = I_p$
- $I_p = \frac{\pi}{2} r^4$
- $\tau = \frac{Tr}{I_p}$
- $\kappa = M/EI$
- $\sigma_x(x, y) = -\frac{M(x)}{I} y$
- rectangle: $\tau(x, y) = \frac{V(x)}{2I} \left(\frac{H^2}{4} - y^2\right)$, $\max = \frac{3V(x)}{2A}$
- circle: $\max(\tau(x)) = \frac{4V(x)}{3A}$
- hollow circle: $\max(\tau(x)) = \frac{4V(x)}{3A} \frac{(r_2^2 + r_2 r_1 + r_1^2)}{r_2^2 + r_1^2}$
- $\frac{d^2 y}{dx^2} = \frac{M(x)}{EI}$
- $\sigma_L = \frac{pr}{2t}$
- $\sigma_C = \frac{pr}{t}$
- $\sigma = \frac{pr}{2t}$
- $\sigma_t = 0$
- $\sigma_C = \frac{pr}{t} = \frac{pr_0(1+\epsilon_C)}{t_0(1+\epsilon_T)}$
- $F_C = \frac{EI\pi^2}{L^2}$ (2 pins); $F_C = \frac{EI\pi^2}{4L^2}$ (solid support)
- $r = \sqrt{I/A}$; L/r is slenderness ratio
- $f(r) = \frac{k_B T}{L_p} \left(\frac{1}{4(1-r/L_0)^2} - \frac{1}{4} + \frac{r}{L_0} \right)$
- $f \approx \frac{3k_B T}{2L_p} \frac{r}{L_0}$
- $r_{rms} = \sqrt{2L_0 L_p}$
- $E = \frac{U''(r_0)}{r_0} = \frac{k}{r_0}$ if linear
- $\frac{P_2}{P_1} = \exp\left(\frac{-\Delta G^0}{k_B T}\right)$
- $k_B T = 4e - 21 J$ at room & body temp.
- $\Delta G(f) = \Delta G^0 - f \cdot \Delta x(f)$
- $f_{eq} \Delta x^0 + f_{eq}^2 \left(\frac{1}{k_2} - \frac{1}{k_1}\right) - \Delta G^0 = 0$
- $K_{eq}^0 = \frac{P_2}{P_1} = \exp\left(\frac{-\Delta G^0}{k_B T}\right)$
- $K_{eq}(f) = K_{eq}^0 \exp\left(\frac{f \Delta x^0}{k_B T}\right)$
- $P_2 = \frac{K_{eq}}{1 + K_{eq}}$
- Voigt $E\epsilon + \eta \frac{d\epsilon}{dt} = \sigma$
- Maxwell $\sigma + \frac{\eta}{E} \frac{d\sigma}{dt} = \eta \frac{d\epsilon}{dt}$
- Kelvin $\sigma + \frac{\eta}{E_S} \frac{d\sigma}{dt} = E_P \epsilon + \eta \left(\frac{E_P + E_S}{E_S}\right) \frac{d\epsilon}{dt}$
- Transforms:
 - $\delta(t - \tau) = e^{-\tau s}$
 - $t \cdot \phi(t) = 1/s^2$
 - $(1 - e^{-at})\phi(t) = \frac{a}{s(s+a)}$
 - $\sin(\omega t) \phi(t) = \frac{\omega}{s^2 + \omega^2}$
 - $\cos(\omega t) \phi(t) = \frac{s}{s^2 + \omega^2}$

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Use this page if you need extra room for any questions. Just write "continued on empty page" or something so we know to look here.

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3. (50) Muscle fiber can be modeled as a stress-producing motor in parallel and series with viscous and elastic elements as shown in the figure. In the sign convention we use for this class, the contractive stress produced by the motor element is considered positive since it has the same effect as tensile stress applied to the element. This stress is independent of the strain or rate of strain of the element. That is, the element equation for the motor is $\sigma = \sigma_m(t)$, where $\sigma_m(t)$ is an input function that is controlled by the nerves. Since it does not depend on system behavior, think of it like a time-variable parameter.



- a) (15 points) Build a mathematical model from this diagram, to derive an equation for the strain of the fiber, ϵ , vs the external stress applied to the fiber, σ .

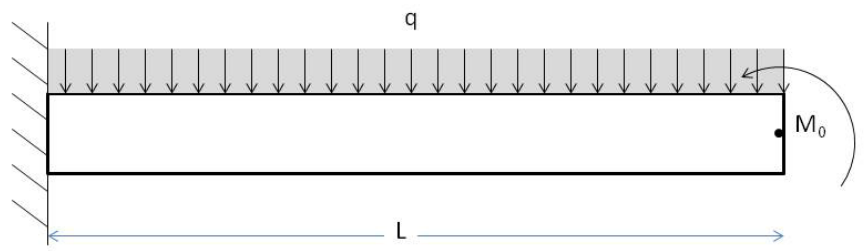
- a. (25 points) Using the differential equation you derived above, derive an algebraic equation for the strain, $\epsilon(t)$, of the muscle fiber, when the muscle starts to contract at $t = 0$ with a force of M , so $\sigma_m(t) = M\phi(t)$, and there is an external tensile stress on the fiber of $\sigma(t) = W\phi(t)$.

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- b. (10 points) interpret your solution for $\epsilon(t)$ to explain the requirements on the parameters $M, W, E,$ and η for the muscle fiber to be able to contract in this experiment. *If you didn't get a final solution, describe the requirement is for contraction, and explain how you would answer the question if you had a solution for $\epsilon(t)$.*

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4. (40) A beam is attached to a solid support at $x = 0$, and is free at $x = L$. There is a uniform external load, q , across the beam. An external moment M_0 is applied at $x = L$, in the direction shown below. The cross section of the beam is a square with sides of length H , and the Young's modulus is E . You can assume that the deflection is small.



a) (15) Find the internal shear force, $V(x)$ and internal bending moment, $M(x)$ everywhere in the beam.

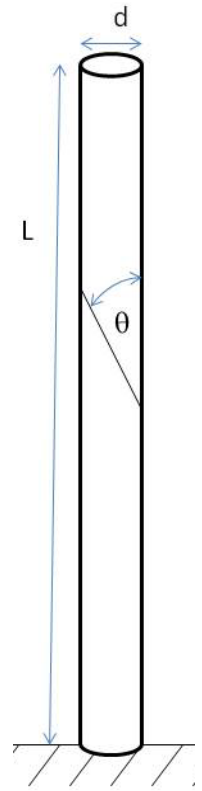
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b) (15) In the special case where $q = \frac{8M_0}{L^2}$, draw the shear force and bending moment diagrams

c) (10) in the same special case, identify the values of x and y that you would need to test for failure.

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5. (30) A column has a weld as shown in the figure. What is the maximum force, F , that the column can withstand? Express your answer in terms of the following values:
- θ = angle of the weld, from the vertical
 - L = length
 - d = diameter
 - E = the Young's modulus
 - USS_w = ultimate shear stress allowed parallel to the weld
 - UTS_w = ultimate tensile stress allowed normal to the weld



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6. (30) A thin-walled cylindrical pressure vessel of radius r and thickness t is subjected simultaneously to an internal pressure p and a compressive force F at the ends, as shown in the figure. The material has linear elasticity with Young's modulus E and Poisson ratio ν , and you can assume small deformations. How much force F , do you need to apply in order to produce zero longitudinal strain in the cylinder walls?

