

1) Problem 7.1 of text

SS beam, $l = 40'$, $D = 80 \text{ psf}$, $L = 50 \text{ psf}$, $10' \text{ o.c.}$
 A36 steel, $W21 \times 73$; $g(x) = M_R - M_S$

$$M_{RN} = 15 \times 36 = 5436 \text{ in-k}$$

$$M_{RN} = \mu_R - 2\sigma_R \quad ; \quad \delta_R = 0.13$$

$$D_N = 80 \text{ psf} = \mu_D + \sigma_D \quad ; \quad \delta_D = 0.13 \rightarrow \mu_D (1 + 0.13) = 80$$

$$L_N = 50 \text{ psf} = \mu_L + 2\sigma_L \quad ; \quad \delta_L = 0.37 \rightarrow \mu_L (1 + 2(0.37)) = 50$$

$$\mu_D = \frac{80}{1.13} = 70.8 \text{ psf} \quad , \quad \sigma_D = 9.2 \text{ psf}$$

$$\mu_L = \frac{50}{1.74} = 28.7 \text{ psf} \quad ; \quad \sigma_L = 10.6 \text{ psf}$$

$$S = D + L$$

$$\mu_S = \mu_D + \mu_L = 70.8 + 28.7 = 99.5 \text{ psf}$$

$$\sigma_S = \sqrt{\sigma_D^2 + \sigma_L^2} = \sqrt{9.2^2 + 10.6^2} = 14.0 \text{ psf}$$

$$\delta_S = \frac{14.0}{99.5} = 0.14$$

$$M_S = \frac{S l^2}{8} \left\{ \frac{(10') (12'')}{(1000 \text{ #/k})} \right\}$$

$$\mu_{MS} = \mu_S \frac{l^2}{8} \left(\frac{(120)''}{1000} \right) = \frac{99.5 (40')^2 (120)}{8 (1000)} = 2388 \text{ in-k}$$

$$\sigma_{MS} = \delta_S (\mu_{MS}) = 0.14 (2388 \text{ in-k}) = 334.3 \text{ in-k}$$

$$\mu_R - 2\sigma_R = 5436 \text{ in-k}$$

$$\mu_R (1 - 2(0.13)) = 5436 \text{ in-k}$$

$$\mu_R = \frac{5436 \text{ in-k}}{0.74} = 7346 \text{ in-k} \quad ; \quad \sigma_R = 0.13 (7346) = 955 \text{ in-k}$$

a) $\phi_f = ?$

$$\phi_f = 1 - \Phi \left\{ \frac{\mu_{MR} - \mu_{MS}}{\sqrt{\sigma_{MR}^2 + \sigma_{MS}^2}} \right\} = 1 - \Phi \left(\frac{7346 - 2388}{\sqrt{837^2 + 955^2}} \right) = 1 - \Phi \left(\frac{4958}{1013} \right)$$

$$= 1 - \Phi(4.89) \cong 1 - \Phi(4.9) = 4.7987 \times 10^{-7} \quad \text{from Appendix I}$$

Problem 7.1 Continued

$$(b) \bar{\gamma} = \frac{\mu_{ML}}{\mu_{MS}} = \frac{7346 \text{ in-k}}{2388 \text{ in-k}} = \underline{\underline{3.08}} \quad \text{central safety factor}$$

$$\bar{\phi} = 1 - \epsilon \beta \delta_R \quad (7.11a)$$

$$\bar{\delta}_i = 1 + \epsilon \epsilon_m \beta \delta_{Si} \quad (7.18a)$$

$$\epsilon = \frac{\sqrt{\sigma_{MR}^2 + \sigma_{MS}^2}}{\sigma_{ME} + \sigma_{MS}} \quad (7.8)$$

$$\epsilon = \frac{\sqrt{955^2 + 334^2}}{955 + 334} = \frac{1012}{1289} = 0.785 \approx \underline{\underline{0.79}}$$

$$\epsilon_m = \frac{\sqrt{\sigma_{S1}^2 + \sigma_{S2}^2}}{\sigma_{S1} + \sigma_{S2}} = \frac{\sqrt{\sigma_D^2 + \sigma_L^2}}{\sigma_D + \sigma_L} = \frac{\sqrt{9.2^2 + 10.6^2}}{9.2 + 10.6} = \frac{14}{19.8} = \underline{\underline{0.71}}$$

$$\bar{\phi} = 1 - 0.79(4.90)(0.13) = \underline{\underline{0.50}}$$

$$\bar{\delta}_D = 1 + (0.79)(0.71)(4.90)(0.13) = \underline{\underline{1.36}}$$

$$\bar{\delta}_L = 1 + (0.79)(0.71)(4.90)(0.37) = \underline{\underline{2.02}}$$

$$(c) \phi = \frac{1 - \epsilon \beta \delta_R}{1 - k_R \delta_R} = \frac{1 - \epsilon \beta \delta_{ML}}{1 - k_{MR} \delta_{MR}} = \frac{1 - 0.79(4.9)(0.13)}{1 - 2(0.13)} = \frac{0.50}{0.74} = \underline{\underline{0.68}}$$

$$\gamma_D = \frac{\bar{\delta}_D}{1 + k_D \delta_D} = \frac{1.36}{1 + 0.13} = \underline{\underline{1.20}}$$

$$\gamma_L = \frac{\bar{\delta}_L}{1 + k_L \delta_L} = \frac{2.02}{1 + 2(0.37)} = \underline{\underline{1.16}}$$

Table 7.5 p. 218 Expanded

Random Variable	Mean	COV	Standard Deviation	Zeta	Lambda
As [in ²]	1.56	0.036	0.0562	0.0360	0.4440
Fy [ksi]	47.7	0.15	7.155	0.1492	3.8538
Fc' [ksi]	3.5	0.21	0.735	0.2077	1.2312
b [in]	8	0.045	0.36	0.0450	2.0784
d [in]	13.2	0.086	1.1352	0.0858	2.5765
eta [dimensionless]	0.59	0.05	0.0295	0.0500	-0.5289
M [kip-in]	326.25	0.17	55.46	0.1688	5.773

Don't use until lognormal case but shown here anyway

g(X) mean	865.56	Standard Deviation g(X)	155.63	beta-estimate	5.56
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Started with "3.0" below

Step 1 g(X) Mc-Mu = 0
Step 2 beta - see below in step 7-9

Step 3	As* [in ²]	1.56	1.53	1.53	1.53
	Fy* [ksi]	47.7	32.21	28.40	25.62
	Fc'* [ksi]	3.5	3.15	3.23	3.28
	b*[in]	8	7.96	7.97	7.98
	d*[in]	13.2	11.35	11.47	11.53
	eta*	0.59	0.59	0.59	0.59
	M* [kip-in]	326.25	385.55	410.24	417.61

final values

Step 4 MEANS	AsN [in ²]	1.56	1.56	1.56	1.56
	FyN [ksi]	47.7	47.7	47.7	47.7
	Fc'N [ksi]	3.5	3.5	3.5	3.5
	bN [in]	8	8	8	8
	dN [in]	13.2	13.2	13.2	13.2
	etaN	0.59	0.59	0.59	0.59
	MN [kip-in]	326.25	326.25	326.25	326.25
Sigmas	AsN [in ²]	0.05616	0.05616	0.05616	0.05616
	FyN [ksi]	7.155	7.155	7.155	7.155
	Fc'N [ksi]	0.735	0.735	0.735	0.735
	bN [in]	0.36	0.36	0.36	0.36
	dN [in]	1.1352	1.1352	1.1352	1.1352
	eta-N	0.0295	0.0295	0.0295	0.0295
	MN [kip-in]	55.4625	55.4625	55.4625	55.4625

Notice these don't change for the normal case.

Step 5	dg/dAs	480.056	290.544	268.674	249.911
	dg/dfy	15.70	13.81	14.52	14.97
	dg/dfc	33.34	18.22	13.52	10.64
	dg/db	14.58	7.21	5.48	4.38
	dg/dd	74.41	49.30	43.59	39.32
	dg/deta	-197.76	-96.81	-73.73	-59.02
	dg/dM	-1.00	-1.00	-1.00	-1.00

Derivatives provided in attached sheet.

Step 6	"Downstairs"	155.63	128.19	129.06	129.65
	alpha As	0.1732	0.1273	0.1169	0.1083
	alpha fy	0.7218	0.7708	0.8051	0.8263
	alpha fc	0.1574	0.1045	0.0770	0.0603
	alpha b	0.0337	0.0203	0.0153	0.0122
	alpha d	0.5428	0.4366	0.3834	0.3443
	alpha eta	-0.0375	-0.0223	-0.0169	-0.0134
	alpha M	-0.3564	-0.4327	-0.4297	-0.4278

Step 7-9 g(X)	beta estimate	3.000	3.500	3.833	3.833
	g(X)	539.31	116.66	45.84	0.90

← β

project:

CEE 518 Derivatives for Table 7.6 p.219

$$g(x) = M_c - M_u$$

$$M_c = A_s f_y d \left\{ 1 - \frac{\eta A_s f_y}{b d f_c'} \right\} = A_s f_y d - \frac{\eta A_s^2 f_y^2}{b f_c'}$$

$$\mu_{M_c} = \mu_{A_s} \mu_{f_y} \mu_d \left\{ 1 - \frac{\mu_\eta \mu_{A_s} \mu_{f_y}}{\mu_b \mu_d \mu_{f_c'}} \right\}$$

Evaluate derivatives of M_u for σ_{M_u} :

$$\frac{\partial M_u}{\partial A_s} = f_y d - \frac{2 \eta A_s f_y^2}{b f_c'}$$

$$\frac{\partial M_u}{\partial f_y} = A_s d - \frac{2 \eta A_s^2 f_y}{b f_c'}$$

$$\frac{\partial M_u}{\partial f_c'} = 0 - \frac{\eta A_s^2 f_y^2}{b} \left(\frac{-1}{f_c'^2} \right)$$

$$\frac{\partial M_u}{\partial b} = \frac{\eta A_s^2 f_y^2}{b^2 f_c'}$$

$$\frac{\partial M_u}{\partial d} = A_s f_y$$

$$\frac{\partial M_u}{\partial \eta} = \frac{-A_s^2 f_y^2}{b f_c'}$$

$$\begin{aligned} \therefore \sigma_{M_u}^2 &= \left(\frac{\partial M_u}{\partial A_s} \right)^2 \sigma_{A_s}^2 + \left(\frac{\partial M_u}{\partial f_y} \right)^2 \sigma_{f_y}^2 + \left(\frac{\partial M_u}{\partial f_c'} \right)^2 \sigma_{f_c'}^2 + \left(\frac{\partial M_u}{\partial b} \right)^2 \sigma_b^2 + \left(\frac{\partial M_u}{\partial d} \right)^2 \sigma_d^2 \\ &\quad + \left(\frac{\partial M_u}{\partial \eta} \right)^2 \sigma_\eta^2 \end{aligned}$$

$$\sigma_{M_u}^2 = \left(\frac{\partial g}{\partial M} \right)^2 \sigma_{M_u}^2 = (-1)^2 \sigma_{M_u}^2 = \sigma_{M_u}^2$$

Table 7.5 p. 218

Expanded

Random Variable	Mean	COV	Standard Deviation	Zeta	Lambda
As [in ²]	1.56	0.036	0.05616	0.03599	0.4440
Fy [ksi]	47.7	0.15	7.155	0.14917	3.8538
Fc' [ksi]	3.5	0.21	0.735	0.20774	1.2312
b [in]	8	0.045	0.36	0.04498	2.0784
d [in]	13.2	0.086	1.1352	0.08584	2.5765
eta [dimensionless]	0.59	0.05	0.0295	0.04997	-0.5289
M [kip-in]	326.25	0.17	55.46	0.16879	5.7734

g(X) mean 865.56 Standard Deviation g(X) 1486.56 beta-estimate 0.5823
start w/ "3.0" below

Step 1 g(X) Mc-Mu = 0
 Step 2 beta - see below in step 7-9

Step 3	As* [in ²]	1.56	1.53	1.53	1.53
	Fy* [ksi]	47.7	31.78	34.24	33.08
	Fc'* [ksi]	3.5	3.08	3.12	3.07
	b* [in]	8	7.18	7.19	7.05
	d* [in]	13.2	11.30	11.47	11.27
	eta*	0.59	0.59	0.59	0.59
	M* [kip-in]	326.25	380.33	455.73	503.53

final values

Step 4 SIGMAS	AsN [in ²]	0.0561	0.0551	0.0551	0.0550
	FyN [ksi]	7.1152	4.7399	5.1069	4.9342
	Fc'N [ksi]	0.7271	0.6405	0.6489	0.6379
	bN [in]	0.3598	0.3229	0.3232	0.3169
	dN [in]	1.1331	0.9701	0.9846	0.9670
	etaN	0.0295	0.0296	0.0296	0.0296
	MN [kip-in]	55.0679	64.1963	76.9230	84.9914

Means	AsN [in ²]	1.56	1.56	1.56	1.56
	FyN [ksi]	47.17	44.33	45.21	44.82
	Fc'N [ksi]	3.42	3.41	3.41	3.41
	bN [in]	7.99	7.95	7.95	7.93
	dN [in]	13.15	13.01	13.04	13.01
	eta-N	0.59	0.59	0.59	0.59
	MN [kip-in]	321.60	316.58	296.92	277.83

Step 5	dg/dAs	480.056	276.409	297.998	281.0260
	dg/dfy	15.70	13.31	13.32	12.9744
	dg/dfc	33.34	20.51	23.20	22.7831
	dg/db	14.58	8.81	10.08	9.9297
	dg/dd	74.41	48.61	52.40	50.5162
	dg/deta	-197.76	-106.73	-122.32	-117.9690
	dg/dM	-1.00	-1.00	-1.00	-1.0000

Step 6 "Downstairs"	alpha As	0.1740	0.1468	0.1401	0.1297
	alpha fy	0.7211	0.6085	0.5807	0.5376
	alpha f'c	0.1565	0.1268	0.1285	0.1220
	alpha b	0.7524	0.6756	0.6843	0.6615
	alpha d	0.5443	0.4549	0.4403	0.4102
	alpha eta	-0.0376	-0.0305	-0.0309	-0.0294
	alpha M	-0.3555	-0.6193	-0.6566	-0.7137

Step 7-9 beta estimate 3.000 3.500 4.091 4.0910 ← β
 g(X) 539.31 105.74 72.80 -4.40

Table 7.5 p. 218
Expanded

Random Variable	Mean	COV	Standard Deviation
As [in2]	1.56	0.036	0.056
Fy [ksi]	47.7	0.15	7.155
Fc' [ksi]	3.5	0.21	0.74
b [in]	8	0.045	0.36
d [in]	13.2	0.086	1.14
eta	0.59	0.05	0.030
[dimensionless]			
M [kip-in]	326.25	0.17	55.46

Rand	As	Rand	Fy	Fc'	b	d	rand	eta	rand	m	Mc	g(x)
0.51	1.56	0.03	33.99	3.58	7.43	13.40	0.57	0.55	0.60	339.88	653.12	313.24
0.18	1.51	0.70	51.38	2.92	8.23	12.46	0.26	0.61	0.30	297.05	812.64	515.59
0.31	1.53	0.31	44.20	3.15	7.83	12.68	0.32	0.58	0.33	302.11	751.48	449.37
0.53	1.56	0.39	45.78	3.01	7.56	15.38	0.97	0.62	0.69	354.06	962.83	608.77
0.95	1.65	0.79	53.43	3.74	7.97	12.64	0.31	0.56	0.99	461.97	969.22	507.25
0.17	1.51	0.83	54.44	3.47	7.61	14.12	0.79	0.59	0.10	256.02	1009.11	753.09
0.70	1.59	0.91	57.51	2.66	7.85	13.35	0.55	0.61	0.98	437.57	976.15	538.58
0.23	1.52	0.85	55.13	3.47	7.54	13.87	0.72	0.58	0.97	430.71	1004.88	574.17
0.49	1.56	0.62	49.88	3.95	8.40	16.06	0.99	0.56	0.24	287.73	1148.33	860.60
0.12	1.50	0.99	65.21	4.30	8.22	13.48	0.60	0.46	0.33	302.32	1156.13	853.81
0.08	1.48	0.79	53.56	3.51	7.71	14.82	0.92	0.60	0.34	303.71	1036.64	732.93
0.39	1.54	0.95	59.74	3.53	7.50	13.62	0.65	0.57	0.77	367.97	1074.98	707.01
0.28	1.53	0.38	45.55	3.47	8.08	13.78	0.70	0.80	0.90	398.70	852.40	453.70
0.37	1.54	0.44	46.59	3.52	8.07	13.63	0.65	0.61	0.79	370.91	868.65	497.75
0.98	1.68	0.32	44.42	3.81	7.02	12.74	0.34	0.68	0.02	215.44	824.85	609.41
0.54	1.56	0.28	43.55	2.08	8.27	13.25	0.52	0.57	0.01	196.86	749.10	552.24
0.77	1.60	0.54	48.48	3.16	7.54	14.52	0.88	0.60	0.43	316.88	974.47	657.59
0.65	1.58	0.49	47.56	3.19	7.68	11.07	0.03	0.88	0.72	358.89	688.20	329.32
0.77	1.60	0.07	37.14	3.26	8.16	15.50	0.98	0.57	0.58	338.08	845.65	507.57
0.78	1.60	0.02	33.21	3.03	8.00	13.95	0.75	0.66	0.23	284.84	666.30	381.46
0.82	1.61	0.02	33.06	2.93	7.92	13.53	0.61	0.62	0.01	191.85	645.42	453.58
0.15	1.50	0.05	36.19	4.75	8.39	14.00	0.76	0.60	0.56	335.13	716.52	381.40
0.63	1.58	0.55	48.55	3.44	7.90	12.64	0.31	0.57	0.16	269.94	845.82	575.87
0.31	1.53	0.91	57.43	3.52	7.56	13.82	0.71	0.58	0.91	398.98	1049.42	650.45
0.35	1.54	0.71	51.75	2.48	7.95	14.22	0.82	0.56	0.55	333.39	950.75	617.37
0.92	1.64	0.51	47.80	2.53	8.17	12.50	0.27	0.62	0.45	318.76	794.61	475.85
0.52	1.56	0.59	49.40	3.82	8.23	14.23	0.82	0.63	0.97	427.16	979.65	552.49
0.40	1.55	0.09	38.28	4.08	7.98	12.13	0.17	0.62	0.56	334.29	650.69	316.40

Monte Carlo Normal

0.61	1.58	0.47	47.23	0.34	3.20	0.21	7.71	0.07	11.56	0.94	0.64	0.81	374.52	717.06	342.54
0.79	1.60	0.40	45.85	0.01	1.81	0.62	8.11	0.24	12.38	0.85	0.62	0.46	320.84	681.91	361.07
0.93	1.64	0.85	55.03	0.76	4.03	0.68	8.17	0.59	13.47	0.51	0.59	0.43	315.96	1071.62	755.66
0.87	1.62	0.96	60.01	0.04	2.25	0.13	7.60	0.22	12.32	0.31	0.58	0.39	311.33	881.00	569.67
0.87	1.62	0.69	51.29	0.52	3.53	0.34	7.85	0.17	12.11	0.99	0.66	0.82	376.69	841.93	465.24
0.67	1.59	0.75	52.56	0.83	4.20	0.91	8.47	0.98	15.60	0.06	0.54	0.14	265.59	1194.04	928.46
0.76	1.60	0.27	43.34	0.78	4.08	0.30	7.81	0.81	14.19	0.32	0.58	0.83	380.19	896.83	516.63
0.58	1.57	0.61	49.65	0.63	3.75	0.66	8.15	0.68	13.74	0.71	0.61	0.73	360.99	951.46	590.46
0.39	1.54	0.26	43.17	0.14	2.70	0.01	7.18	0.89	14.56	0.76	0.61	0.63	345.16	830.74	485.59
0.36	1.54	0.31	44.23	0.27	3.05	0.23	7.73	0.19	12.20	0.15	0.56	0.10	256.64	720.64	464.00
0.20	1.51	0.22	42.12	0.24	2.97	0.25	7.76	0.27	12.51	0.29	0.57	0.31	298.11	695.92	397.82
0.83	1.61	0.01	30.42	0.19	2.85	0.37	7.88	0.55	13.34	0.73	0.61	0.91	401.56	589.65	188.09
0.42	1.55	0.12	39.12	0.81	4.16	0.51	8.01	0.21	12.30	0.91	0.63	0.61	342.04	675.39	333.35
0.46	1.55	0.62	49.93	0.78	4.07	0.94	8.56	0.10	11.73	0.26	0.57	0.41	314.34	811.90	497.56
0.98	1.67	0.99	63.60	0.99	5.37	0.00	6.97	0.01	10.55	0.02	0.53	0.03	217.80	964.18	746.38
0.13	1.50	0.42	46.23	0.71	3.91	0.00	6.97	0.29	12.59	0.59	0.60	0.88	390.83	765.50	374.67
0.21	1.52	0.04	34.75	0.86	4.29	0.68	8.17	0.50	13.21	0.33	0.58	0.15	268.26	649.80	381.54
0.96	1.66	0.21	41.98	0.47	3.44	0.72	8.21	0.97	15.38	0.23	0.57	0.48	323.46	972.85	649.39
0.74	1.60	0.35	44.93	0.96	4.80	0.57	8.07	0.19	12.18	0.80	0.61	0.41	313.51	791.90	478.39
0.41	1.55	0.21	41.94	0.01	1.83	0.81	8.32	0.61	13.53	0.42	0.58	0.22	282.82	716.63	433.81
0.78	1.60	0.01	31.35	0.24	2.99	0.47	7.98	0.70	13.81	0.94	0.63	0.17	272.52	626.74	354.22
0.76	1.60	0.82	54.14	0.87	4.34	0.93	8.54	0.99	15.84	0.05	0.54	0.11	257.03	1262.12	1005.09
mean	1.57	0.47	46.92	0.48	3.44	0.44	7.90	0.54	13.41	0.53	0.59	0.49	324.43	859.36	534.93
stdev	0.05	0.31	8.24	0.28	0.74	0.29	0.38	0.30	1.23	0.30	0.03	0.30	61.20	165.70	170.88

approximately, no failures!
 need to increase "n" to

10,000 or so for accuracy.

$$\beta = \Phi^{-1}(1-p_f) = \Phi^{-1}(1.0)$$

≈ 4.9

undisturbed
 actually,
 choose
 0.99999.