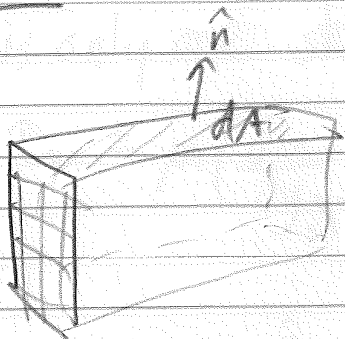


lecture 8

Oct 11, 2018



shear force:

$$\vec{F}_v = - \iint_A \underline{\underline{\tau}} \cdot \hat{n} dA$$

tensor rank 2
vector

gives a vector

$$\vec{F}_p = \left(\iint -p dA \right) \hat{n}$$



$\sum \vec{F} = 0 \Rightarrow$ no acceleration, steady state

$$Q = \iint_A \vec{v} \cdot \hat{n} dA$$

Channel: $Q = \int_{-h}^h u dy$

$$= U_m \int_{-h}^h \left(1 - \frac{y^2}{h^2} \right) dy$$

$$s = \frac{y}{h}$$

$$hs = dy$$

$$= U_m h \int_{-h}^h (1 - s^2) dy$$

$$= U_m h \left[s^2 - \frac{s^3}{3} \right]_{-h}^h = U_m h \left(1 - (-1) + \frac{1}{3} - \left(-\frac{1}{3}\right) \right)$$

$$= \frac{4}{3} U_m h = \frac{2}{3} \frac{h^3}{\mu} \left| \frac{dP}{dx} \right|$$

$$\left| \frac{dp}{dx} \right| = \frac{3}{2} \frac{Q \mu}{h^3}$$

$$\frac{dp}{dx} \propto Q$$

$$\frac{dp}{dx} \uparrow \rightarrow Q \uparrow$$

$$\frac{dp}{dx} \propto \mu$$

$$\mu \uparrow \rightarrow \frac{dp}{dx} \uparrow$$

$$\frac{dp}{dx} \propto \frac{1}{h^3}$$

$$h \downarrow \rightarrow \frac{dp}{dx} \uparrow$$

average velocity: $\langle U \rangle = \frac{Q}{2h} = \frac{1}{3} \frac{h^2}{\mu} \left| \frac{dp}{dx} \right| = \frac{2U_m}{3}$

$$= \frac{\int_{-h}^h u dy}{h - (-h)}$$

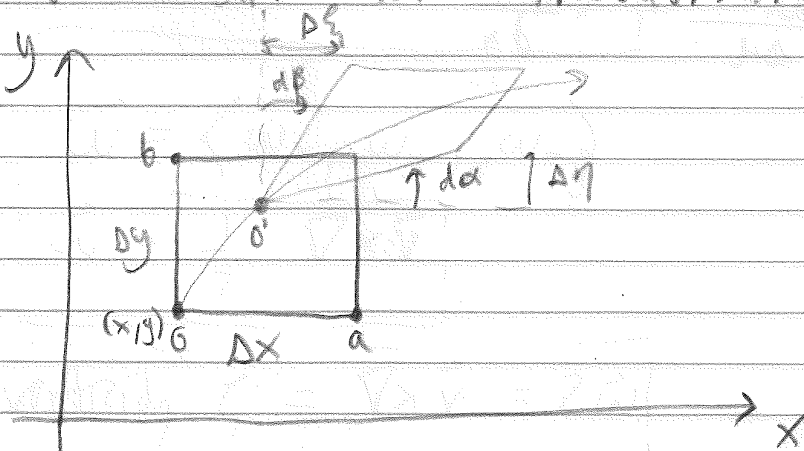
Vorticity

Smits 6.1

→ describes rotation of a fluid element (vortex)

→ can be used in turbulent flow

→ if it doesn't exist → irrotational



1. rotation

2. translation

3. deformation
(strain rate)

At time t , velocity at $(x, y) = (u_0, v_0)$

During Δt , the fluid particle moves from O to O'
with coordinates $(x + u_0 \Delta t, y + v_0 \Delta t)$

Simultaneously, the line OA and OB rotates around O

The rotation rate of OA is

$$\omega_{OA} = \lim_{\Delta t \rightarrow 0} \frac{\Delta \alpha}{\Delta t}$$

$$\frac{\Delta \eta}{\Delta x} = \tan(\Delta \alpha) \approx \Delta \alpha \quad (\text{small angle})$$

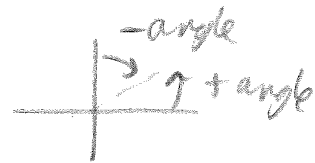
$$v_A = v_0 + \frac{\partial v}{\partial x} \Delta x$$

$$\Delta \eta = \frac{\partial v}{\partial x} \Delta x \Delta t$$

$$\Delta \eta = (v_A - v_0) \Delta t$$

$$\Delta \alpha = \frac{\Delta \eta}{\Delta t} = \frac{\partial v}{\partial x} \Delta t$$

$$\omega_{OA} = \lim_{\Delta t \rightarrow 0} \frac{\frac{\partial v}{\partial x} \Delta t}{\Delta t} = \frac{\partial v}{\partial x}$$



$$u_{0y} = \lim_{\Delta t \rightarrow 0} \frac{-\Delta B}{\Delta t}$$

$$\frac{\Delta \zeta}{\Delta y} = \tan(\Delta \beta) \approx \Delta \beta$$

$$u_p = u_0 + \frac{du}{dy} \Delta y$$

$$\Delta \zeta = (u_p - u_0) \Delta t$$

$$\Delta \zeta = \frac{du}{dy} \Delta y \Delta t$$

$$\lim_{\Delta t \rightarrow 0} \frac{-\frac{du}{dy} \Delta t}{\Delta t} = -\frac{du}{dy}$$

$$\omega_z = \frac{1}{2} \left(\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right)$$

average of two terms
xy plane \rightarrow z comp. ω

$$\omega_x = \frac{1}{2} \left(\frac{\partial w}{\partial y} - \frac{\partial v}{\partial z} \right)$$

yz plane \rightarrow x comp. ω

$$\omega_y = \frac{1}{2} \left(\frac{\partial u}{\partial z} - \frac{\partial w}{\partial x} \right)$$

xz plane \rightarrow y comp. ω

$$\vec{\omega} = \langle \omega_x, \omega_y, \omega_z \rangle$$

$$\begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ u & v & w \end{vmatrix}$$

$$\vec{\omega} = \frac{1}{2} \nabla \times \vec{v}$$

$$\text{vorticity } \zeta = \nabla \times \vec{v} = 2\vec{\omega}$$

The fluid element

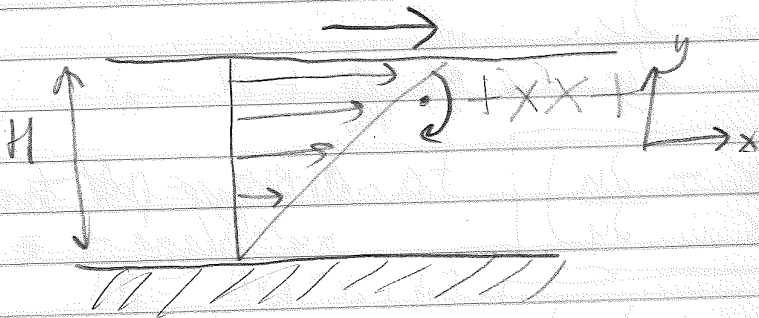
1) advects (u_0, v_0)

2) rotates $\frac{1}{2} \left(\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right)$

3) deforms $\frac{1}{2} \left(\frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} \right)$

Examples

Plane Couette flow

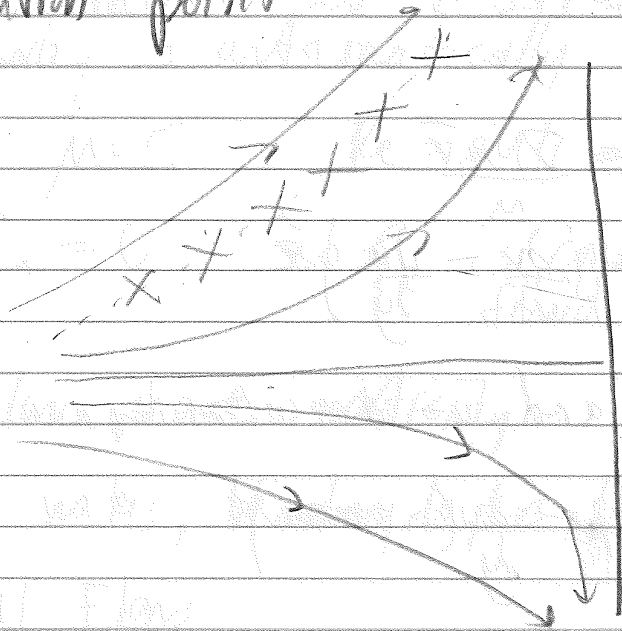


$$u = \frac{U}{h} y \quad v = 0$$

$$\zeta = \zeta_z = \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} = -\frac{U}{h}$$

clockwise rotation
at a rate of $\frac{U}{2h}$

stagnation point



$$u = -ax$$
$$v = ay$$

$$\zeta = \frac{dv}{dx} - \frac{du}{dy} = 0 \quad \text{irrotational}$$

The rest of the flow is irrotational.

$$-\frac{d}{dy} \left(\frac{\rho \mu}{\rho t} = \rho g + \mu \left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} \right) - \frac{d\rho}{dt} \right)$$

Lecture 9

$$\frac{d}{dx} \left(\frac{\rho \mu}{\rho t} = \rho g + \mu \left(\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right) - \frac{d\rho}{dt} \right) \quad \text{Oct 15, 2018}$$

$$\vec{\omega} = \frac{1}{2} \nabla \times \vec{v}$$

3D flow: $\zeta = \nabla \times \vec{v}$

2D flow: $\zeta_z = \left(\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right) \hat{z}$

In 2D, for x- and y- momentum eqn:

$$\frac{\partial}{\partial x} (\text{y-mom.}) - \frac{\partial}{\partial y} (\text{x-mom.})$$

Continuity for incompressible flow:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$

$$\Rightarrow \rho \frac{D \zeta_z}{Dt} = \mu \left(\frac{\partial^2 \zeta_z}{\partial x^2} + \frac{\partial^2 \zeta_z}{\partial y^2} \right) = \mu \nabla^2 \zeta_z$$

heat equation!

Stream function:

$$u = \frac{\partial \psi}{\partial y} \quad v = -\frac{\partial \psi}{\partial x}$$

$$\zeta_z = \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y}$$

$$\zeta_z = -\nabla^2 \psi$$

vorticity can be determined by ψ and vice versa

these combined can be solved instead of N-S
Continuity is automatically satisfied.

Assume $\mu=0$ $Re = \frac{\rho U L}{\mu} \rightarrow \infty$

$\frac{D\zeta_z}{Dt} = 0$ so ζ_z is conserved following a fluid particle

Many flows have vorticity

e.g. wakes, boundary layers, shear layers (jets)

Potential Flows

Smits 6.2

Consider the flow past a cylinder (Smits (chap 6))
 $Re \gg 1$

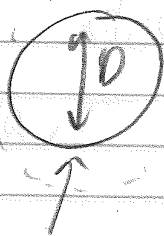
U_∞

u

\rightarrow

\rightarrow

irrotational



wake
rotational

BL
rotational

$$\nabla \times \vec{v} = 0$$

Vorticity is generated by viscous effects
i.e. boundary layer, and swept into
wake.

the rest of the flow is irrotational.

Advantages to split into two parts:
rotational + irrotational

$$\vec{\zeta} = \nabla \times \vec{v} = \vec{0}$$

$$\nabla \times (\nabla \phi) = 0$$

from calculus

$\phi = \text{any scalar}$

$$\phi = (\vec{x}, t)$$

Suggest $\vec{v} = \nabla \phi$

gradient of "velocity potential"

$$\vec{\zeta} = \nabla \times (\nabla \phi) = \vec{0}$$

$$u = \frac{\partial \phi}{\partial x}, \quad v = \frac{\partial \phi}{\partial y}, \quad w = \frac{\partial \phi}{\partial z}$$

$\phi = \text{const.}$

