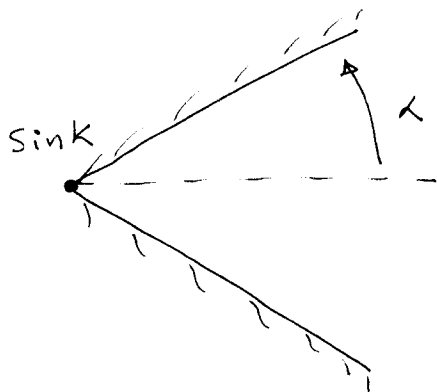


# Example Potential Flow coupled to Boundary Layer



The potential (inviscid, irrotational) approximation is valid away from the walls and predict a velocity field:

$$V_r(r) = \frac{m}{2\pi r} \quad ; \quad V_\theta = 0$$

Applying Bernoulli to the potential flow velocity.

$$P(r) + \frac{1}{2} \rho V^2 = P_\infty + \frac{1}{2} \rho V_\infty^2$$

$$P(r) = \left[ P_\infty + \frac{1}{2} \rho \left( V_\infty^2 - \frac{m^2}{4\pi^2 r^2} \right) \right]$$

To account for the no-slip condition at the walls, we need to introduce a  $\theta$  dependency to the velocity field, so that at  $\theta = \pm\alpha$  the velocity is zero, and as we move away from the wall  $\theta > -\alpha$  or  $\theta < \alpha$ , the velocity is insensitive to  $\theta$  and tends to  $V_r(r) = \frac{m}{2\pi r}$

Assuming a solution of the form:  $V_r = \frac{m}{2\pi r} f(\theta)$  and

$$\frac{P(r) - P_\infty}{\rho} = -\frac{m^2}{8\pi^2 r^2} g(\theta) \quad (V_\infty \rightarrow 0) \quad \text{we get:}$$

r-component of N-S

$$\rho \left( \frac{\partial V_r}{\partial t} + v_r \frac{\partial V_r}{\partial r} + \frac{v_\theta}{r} \frac{\partial V_r}{\partial \theta} - \frac{v_\theta^2}{r} + v_z \frac{\partial V_r}{\partial z} \right) = -\frac{\partial P}{\partial r} + \mu \left[ \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial V_r}{\partial r} \right) - \frac{2}{r^2} \frac{\partial v_\theta}{\partial \theta} + \frac{\partial^2 V_r}{\partial z^2} + \frac{1}{r^2} \frac{\partial^2 V_r}{\partial \theta^2} \right]$$

from continuity we get:

$$\frac{\partial \rho}{\partial t} + \frac{1}{r} \frac{\partial}{\partial r} (\rho r v_r) + \frac{1}{r} \frac{\partial}{\partial \theta} (\rho v_\theta) + \frac{\partial}{\partial z} (\rho v_z) = 0$$

since  $v_\theta = 0$  at  $\theta = \pm\alpha$

r-comp. N-S.

$$\int \frac{m}{2\pi\epsilon r} f(\theta) - \frac{m}{2\pi\epsilon r^2} f(\theta) = -\int \frac{2m^2}{8\pi^2\epsilon^2 r^3} g(\theta) + \mu \left[ \frac{1}{r} - \frac{m}{2\pi\epsilon r^2} - \frac{m}{2\pi\epsilon r^3} + \frac{1}{r^2} \frac{m}{2\pi\epsilon r} f''(\theta) \right]$$

$$-\frac{m^2}{4\pi^2\epsilon r^3} f^2(\theta) = -\frac{m^2}{4\pi^2\epsilon r^3} g(\theta) + \mu \frac{m}{2\pi\epsilon r^3} f''(\theta)$$

$$\frac{2\pi\mu}{m} f''(\theta) = -f^2(\theta) + g(\theta)$$

$\frac{2\pi\mu}{m} = \frac{1}{Re} = \epsilon \ll 1$  This is a singular perturbation problem where the small parameter multiplies the highest order derivative

$$\boxed{\epsilon f'' + f^2 = g}$$

\theta-comp N-S

$$\int \left( \frac{\partial V}{\partial t} + v_r \frac{\partial V}{\partial r} + \frac{v_\theta}{r} \frac{\partial V}{\partial \theta} + v_r \frac{\partial V}{\partial r} + v_\theta \frac{\partial V}{\partial \theta} \right) = -\frac{1}{r} \frac{\partial P}{\partial \theta} + \mu \left[ \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial v_\theta}{\partial r} \right) - \frac{v_\theta}{r^2} + \frac{1}{r^2} \frac{\partial^2 v_\theta}{\partial \theta^2} + \frac{2}{r^2} \frac{\partial v_r}{\partial \theta} + \frac{\partial^2 v_\theta}{\partial r^2} \right]$$

$$0 = -\frac{1}{r} \frac{-m^2}{8\pi^2\epsilon^2 r^2} g'(\theta) + \mu \frac{2}{r^2} \frac{m}{2\pi\epsilon r} f'(\theta)$$

$$g'(\theta) = \frac{8\pi\mu}{m} f'(\theta)$$

$$\boxed{g(\theta) = 4\epsilon f'(\theta)}$$

When  $\epsilon \rightarrow 0$ , we get  $f' = g$

$$g' = 0 \Rightarrow g(\theta) = \text{constant} = C_0$$

$$f''(\theta) = g(\theta) = C_0$$

We can impose as a condition that the flow rate between the walls is equal to the flow rate in the sink

$$\int_{-\alpha}^{\alpha} 2\pi r V_r d\theta = m$$

$$\int_{-\alpha}^{\alpha} \frac{m}{2\pi r} f(\theta) d\theta = m \Rightarrow \int_{-\alpha}^{\alpha} f(\theta) d\theta = 1 \Rightarrow \int_{-\alpha}^{\alpha} \sqrt{C_0} d\theta = 1 \Rightarrow$$

$$2\alpha \sqrt{C_0} = 1 \Rightarrow C_0 = \frac{1}{4\alpha^2}$$

but if we try to solve for other terms in  $\epsilon, \epsilon^2, \dots$

$$f(\theta) = f_0 + \epsilon f_1 + \epsilon^2 f_2 + \dots$$

$$g(\theta) = g_0 + \epsilon g_1 + \epsilon^2 g_2 + \dots$$

$$\epsilon (f_0'' + \epsilon f_1'') + (f_0 + \epsilon f_1)^2 = g_0 + \epsilon g_1$$

$$O(\epsilon) \quad \cancel{f_0''} + 2\epsilon f_0 f_1 = g_1 \quad f_0 = \sqrt{C_0} = \frac{1}{2\alpha}$$

$$f_1 = \frac{1}{2\epsilon f_0} \cdot g_1$$

$$O(\epsilon) \quad g_0 + \epsilon g_1 = 4\epsilon (f_0' + \epsilon f_1')$$

$$O(\epsilon) \quad g_1 = 4f_0' = 0 \Rightarrow g_1 = \text{constant} = C_1$$

$$\Downarrow$$

$$f_1 = \frac{C_1}{2\epsilon \frac{1}{2\alpha}} = \frac{\alpha C_1}{\epsilon}$$

By continuity

$$\int_{-\alpha}^{\alpha} 2\pi r \frac{m}{2\pi r} (f_0 + \epsilon f_1 + \epsilon^2 f_2 + \dots) d\theta = m$$

$$\int_{-\alpha}^{\alpha} f_0 d\theta = 1; \int_{-\alpha}^{\alpha} f_1 d\theta = 0; \int_{-\alpha}^{\alpha} f_2 d\theta = 0 \dots \dots$$

$$f_1 = \frac{\alpha C_1}{\epsilon} = 0 \Rightarrow g_1 = 0$$

It does not work.

To obtain the behaviour inside the boundary layer we need to rescale  $\theta$  so that the viscous term  $\frac{\rho^2}{\rho \partial z^2}$  is of the same order as the pressure gradient and the convective term inside the boundary layer:

$$\theta^* = \frac{\theta + \alpha}{\delta(\epsilon)}$$

$\theta = \pm \alpha \Rightarrow \theta^* = 0$  at the wall

$\theta < \alpha$  or  $\theta > \alpha \Rightarrow \theta^* \rightarrow \infty$  away from the wall.

$$\frac{d}{d\theta^*} = \delta(\epsilon) \frac{d}{d\theta}$$

$$\epsilon \cdot \frac{1}{\delta^2(\epsilon)} f''(\theta^*) + f^2 = g \Rightarrow \frac{\epsilon}{\delta^2(\epsilon)} = 1 \Rightarrow \delta(\epsilon) = \sqrt{\epsilon}$$

$$\frac{1}{\delta(\epsilon)} g'(\theta^*) = 4\epsilon \frac{1}{\delta(\epsilon)} f'(\theta^*)$$

$$\frac{1}{\sqrt{\epsilon}} g'(\theta^*) = \frac{4\epsilon}{\sqrt{\epsilon}} f'(\theta^*)$$

$$\left. \begin{aligned} \text{Make } f(\theta^*) &= \bar{f}_0 + \epsilon \bar{f}_1 + \epsilon^2 \bar{f}_2 + \dots \\ g(\theta^*) &= \bar{g}_0 + \epsilon \bar{g}_1 + \epsilon^2 \bar{g}_2 + \dots \end{aligned} \right\}$$

$$O(\epsilon^0) \Rightarrow \bar{g}'_0(\theta^*) = 0 \Rightarrow \bar{g}_0(\theta^*) = \text{constant} : \text{pressure}$$

$\bar{g}_0(\theta^*) = \text{constant} = g_0$  outside the b.l. does not change across the boundary layer, just as in the cartesian b.l.

$$\bar{f}_0''(\theta^*) + \bar{f}_0^2 = \text{constant} = \frac{1}{4\alpha^2}$$

drop the  $\theta$  and the  $-$

$$\rightarrow f' \frac{df'}{d\theta^*} = \left( \frac{1}{4\alpha^2} - f^2 \right) f'$$

$$\frac{1}{2} \int d f'^2 = \int \left( \frac{1}{4\alpha^2} - f^2 \right) \frac{df}{d\theta^*} \cdot d\theta^*$$

$$\int \frac{1}{2} f'^2 - \frac{1}{2} f - \frac{f^3}{3} + C \rightarrow \theta$$

When  $\theta^* \rightarrow \infty \Rightarrow f(\theta^*) \rightarrow 0$   
 $f'(\theta^*) \rightarrow \epsilon$

$$\int \frac{df}{\left( \frac{1}{4\alpha^2} f - \frac{f^3}{3} \right)^{1/2}} = \sqrt{2} \int d\theta^*$$