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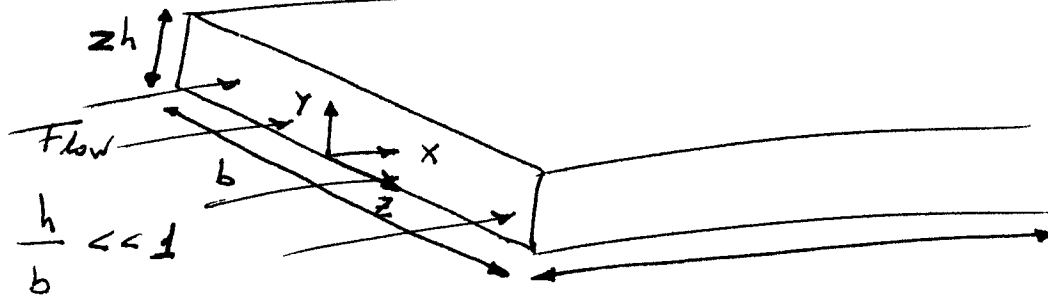
Turbulent Boundary Layer

Canonical Flows: { Channel Flow
Pipe Flow
Boundary layer



Free Shear Flows: Canonical Cases { Jet
Mixing Layer
Wake

CHANNEL FLOW



The Reynolds number for this flow can be defined in several ways:

$$Re_{max} = \frac{U_0 \cdot 2h}{\nu} \quad ; \quad Re_{AVE} = \frac{U_{AVE} \cdot h}{\nu}$$

and any combination in between $\frac{U_0 \cdot h}{\nu}$ or $\frac{U_{AVE} \cdot 2h}{\nu}$

The averaged momentum equation in the axial direction is just: $0 = \nu \frac{d^2 \langle U_x \rangle}{dy^2} - \frac{d}{dy} \langle U_x' v_y' \rangle - \frac{1}{\rho} \frac{\partial \langle P \rangle}{\partial x}$

②

Which can be rewritten as:

$$\frac{dZ}{dy} = \frac{dP_w}{dx}$$

because $\frac{dP_w}{dx} = \frac{\rho \langle P \rangle}{\rho x}$ and we define

$$Z = \underbrace{\int \mu \frac{d\langle U_x \rangle}{dy}}_{\text{viscous stress}} - \underbrace{\int \langle U_x' U_y' \rangle}_{\text{Reynolds stresses}}$$

Because of symmetry $-\frac{dP_w}{dx} = \frac{Z_w}{h}$ (Balance of forces in a control volume)

and therefore $Z(y) = Z_w \left(1 - \frac{y}{h}\right)$

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Law of the Wall

According to the Boundary Layer principle due to the Prandtl (1925), for High Reynolds numbers $Re \gg 1$, there is a very thin layer where the flow is dominated by viscous effects. In this region $\frac{y}{\delta(h)} \ll 1$ and the flow is independent of h or U_0 . This is called the "inner region".

$$\frac{d\langle U_x \rangle}{dy} = \frac{u_z}{y} \Phi_{\text{I}} \left(\frac{y}{\delta_v} \right) : \text{In the inner region the only length scale is } \delta_v = \frac{\nu}{u_z} \text{ and the only velocity scale is } u_z = \sqrt{\frac{h}{S} \left(-\frac{dP_w}{dx} \right)}$$

based on τ_w

We saw previously that the general solution to this problem can be written, based on dimensional analysis, as

$$\frac{d\langle U_x \rangle}{dy} = \frac{u_z}{y} \Phi \left(\frac{y}{\delta_v}, \frac{y}{h} \right)$$

(4)

In the "inner layer" $\frac{y}{h} \rightarrow 0$ and

$$\overline{\Phi}_I \left(\frac{y}{s_v} \right) = \lim_{\frac{y}{h} \rightarrow 0} \overline{\Phi} \left(\frac{y}{s_v}, \frac{y}{h} \right)$$

Defining u^+ as $\frac{\langle V_x \rangle}{u_z}$ we get

$$\frac{d u^+}{d y^+} = \frac{1}{y^+} \overline{\Phi}_I (y^+) \text{ and integrating we get}$$

$$\boxed{u^+ = f(y^+)} \text{ Law of the Wall.}$$

There is an "outer region" where $y^+ = \frac{y}{s_v} \gg 1$

$$\text{and therefore } \frac{d \langle V_x \rangle}{d y} = \frac{u_z}{y} \overline{\Phi} \left(\frac{y}{s_v} \rightarrow \infty, \frac{y}{h} \right)$$

$$\text{so } \frac{d \langle V_x \rangle}{d y} = \frac{u_z}{y} \overline{\Phi}_o \left(\frac{y}{h} \right)$$

We can integrate this to define Velocity Defect

$$\text{Law: } \int_y^h \frac{d \langle V_x \rangle}{d y} = \langle V_x(h) \rangle - \langle V_x(y) \rangle = \int_y^h \frac{u_z}{y} \overline{\Phi}_o \left(\frac{y}{h} \right) dy$$

$$\boxed{\frac{\langle V_x(h) \rangle - \langle V_x(y) \rangle}{u_z} = F \left(\frac{y}{h} \right)} \text{ Velocity Defect Law}$$

⑤

In every singular perturbation problem, there is an overlap region where the solutions obtained asymptotically for the inner and outer regions must match:

$$\lim_{y/\delta_v \rightarrow \infty} \overline{\Phi}_I (y/\delta_v) = \lim_{y/h \rightarrow 0} \overline{\Phi}_O (y/h)$$

$$\frac{y}{u_z} \frac{d\langle V_x \rangle}{dy} = \overline{\Phi}_I (y/\delta_v) = \overline{\Phi}_O (y/h)$$

for a range $\delta_v \ll y \ll h$

This equation can only be satisfied if both

$$\left. \begin{array}{l} \overline{\Phi}_I (y/\delta_v) \xrightarrow{y/\delta_v \rightarrow \infty} \text{constant} \\ \overline{\Phi}_O (y/h) \xrightarrow{y/h \rightarrow 0} \text{constant} \end{array} \right\} \frac{y}{u_z} \frac{d\langle V_x \rangle}{dy} = \frac{1}{\kappa}$$

Millikan (1939)

$$\int d\left(\frac{\langle V_x \rangle}{u_z}\right) = \frac{1}{\kappa} \int \frac{dy}{y} \Rightarrow u^+ = \frac{1}{\kappa} \ln y^+ + \text{constant } A$$

$$\Downarrow$$

$$\frac{V_0 - \langle V_x \rangle}{u_z} = -\frac{1}{\kappa} \ln\left(\frac{y}{h}\right) + B_1$$

$A \approx 5.2$
 $\kappa \approx 0.41$