

$$a) \dot{m} = \frac{V_1 A_1}{v_1}$$

Ideal gas? Yes $Pv = RT$

$$v_1 = \frac{RT_1}{P_1} = \frac{0.287 \frac{\text{kJ}}{\text{kg K}} \cdot 290 \text{ K}}{100 \text{ kPa}} = 0.832 \frac{\text{m}^3}{\text{kg}}$$

$$\dot{m} = \frac{6 \text{ m/s} \cdot 0.10 \text{ m}^2}{0.832} = 0.72 \frac{\text{kg}}{\text{s}}$$

$$b) q + w_{\text{other}} + h_1 + \frac{V_1^2}{2} - \left(h_2 + \frac{V_2^2}{2} \right) = 0$$

$$w_{\text{other}} = h_2 - h_1 + \frac{V_2^2 - V_1^2}{2}$$

$$w_{\text{other}} = (555.74 - 290.16) \frac{\text{kJ}}{\text{kg}} + \frac{(2 \text{ m/s})^2 - (6 \text{ m/s})^2}{2} \frac{\text{kJ}}{\text{kg}} \cdot \frac{1000 \text{ m}^2}{\text{s}^2}$$

$$W_{\text{other}} = w_{\text{other}} \cdot \dot{m} = 191.4 \text{ kW}$$

c) Negligible kinetic energy change

$$2. \quad \eta_{th} = 1 - \frac{T_L}{T_H} \quad \text{maximum}$$

$$\eta_{max} = 1 - \frac{300}{500} = \frac{2}{5} = 0.4$$

$$\eta_{claim} = \frac{410}{1000} = 0.41 \quad \text{Not possible}$$

$$3. \quad \eta_{compressor} = \frac{h_{2s} - h_1}{h_{2a} - h_1}$$

If the compressor is isentropic, then $s_2 = s_1$,

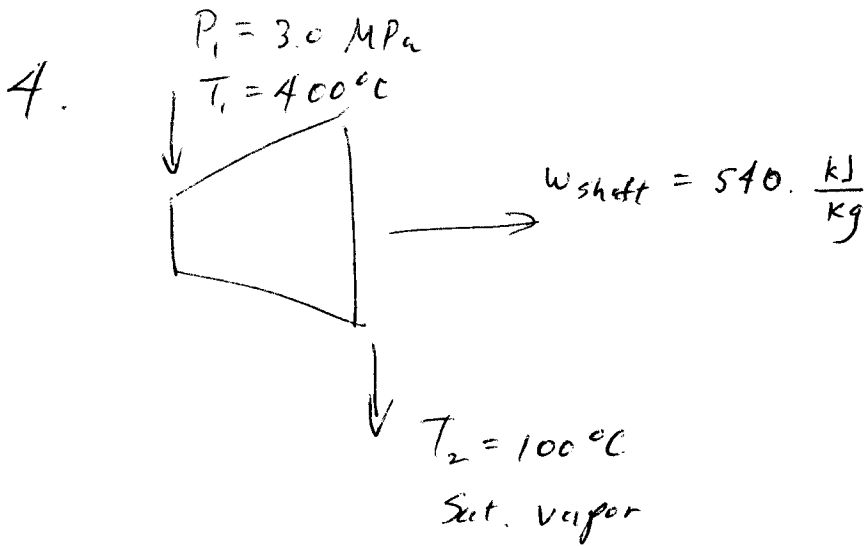
$$\text{and } s_2^{\circ} = s_1^{\circ} + R \ln \left(\frac{P_2}{P_1} \right)$$

$$\begin{aligned} s_2^{\circ} &= 1.66802 \frac{\text{kJ}}{\text{kg K}} + 0.287 \frac{\text{kJ}}{\text{kg K}} \ln \left(\frac{0.7}{0.1} \right) \\ &= 2.2265 \frac{\text{kJ}}{\text{kg K}} \end{aligned}$$

$$T_{2s} = 503.4 \text{ K}$$

$$h_{2s} = 506.54 \frac{\text{kJ}}{\text{kg}}$$

$$\eta_{compressor} = \frac{506.54 - 290.16}{555.74 - 290.16} = 81.5\%$$



a)

$$q + w_{\text{other}} = h_2 - h_1 = 2675.6 \frac{\text{kJ}}{\text{kg}} - 3231.7 \frac{\text{kJ}}{\text{kg}}$$

where $w_{\text{other}} = -540 \frac{\text{kJ}}{\text{kg}}$

$q = -16.1 \frac{\text{kJ}}{\text{kg}}$ transferred from turbine to surroundings

b)

$$s_2 - s_1 = s_{\text{gen}} + \sum \left(\frac{\delta q}{T} \right)_{\text{boundary}}$$

$$s_2 = 7.3542 \frac{\text{kJ}}{\text{kgK}}$$

$$s_1 = 6.9235 \frac{\text{kJ}}{\text{kgK}}$$

$$(7.3542 - 6.9235) \frac{\text{kJ}}{\text{kgK}} = s_{\text{gen}} - \frac{16.1 \frac{\text{kJ}}{\text{kg}}}{500 \text{ K}}$$

$$s_{\text{gen}} = 0.4629 \frac{\text{kJ}}{\text{kgK}}$$

c) For an isentropic turbine, $s_2 = s_1 = 6.9235 \frac{\text{kJ}}{\text{kg} \cdot \text{K}}$

In that case, the exit would be two-phase.

$$x = \frac{6.9235 - 1.3072}{6.047} = 0.9288$$

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$$h_{2s} = 419.17 \frac{\text{kJ}}{\text{kg}} + x \cdot 2256.4 \frac{\text{kJ}}{\text{kg}} = 2514.86 \frac{\text{kJ}}{\text{kg}}$$

$$W_{\text{other}} = h_{2s} - h_1 = (2514.86 - 3231.7) \frac{\text{kJ}}{\text{kg}} = -716.8 \frac{\text{kJ}}{\text{kg}}$$

isentropic

$$W_{\text{shutt}} = 716.8 \frac{\text{kJ}}{\text{kg}} \quad \text{greater than actual}$$

isentropic