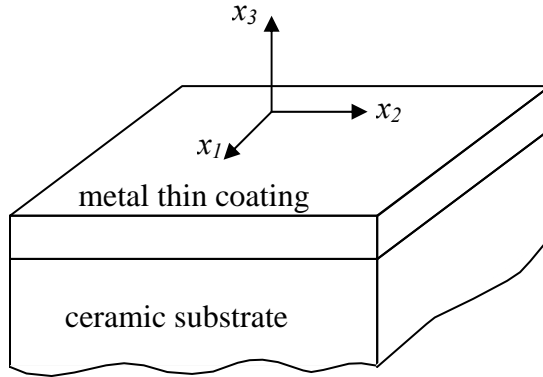


ME/MSE 485 Homework #4, due on Feb. 14 noon(to ME office), 2011

Consider a thin metal coating on a thick ceramic substrate, which underwent a uniform temperature change  $\Delta T$ .



CTE misfit strain

$$\varepsilon^* = (\alpha_c - \alpha_s) \Delta T \quad (1)$$

$$\varepsilon^* = (\varepsilon_{11}^*, \varepsilon_{22}^*, 0)$$

where  $\alpha_s$  and  $\alpha_c$  are CTE of the substrate and coating, respectively. The elastic constants of the coating and substrate are  $E_c$  and  $\nu_c$ , and  $E_s$  and  $\nu_s$ , respectively.

Use the following material data:

$$E_c = 70 \text{ GPa}, \nu_c = 0.34, E_s = 290 \text{ GPa}, \nu_s = 0.2, \alpha_s = 6 \times 10^{-6}/\text{C}, \alpha_c = 16 \times 10^{-6}/\text{C}.$$

Assume that the metal coating was deposited by evaporation at high temperature (220 C) and cooled down to room temperature (20C). It is assumed that the stress state is assumed to be zero at the processing temperature, 220 C. The length (width) of the coating and substrate is  $b = 20$  mm.

Answer to the following questions:

1. Assume that the coating is much thinner than substrate and it is isotropic. Calculate the in-plane thermal stress in the metal coating,  $\sigma_c$ , at room temperature. Is this tensile or compressive stress ?
2. If the thickness of the coating ( $h_c$ ) = 1 mm, and that of the substrate ( $h_s$ ) = 5 mm, calculate the in-plane thermal stress in the coating,  $\sigma_c$ , and in the substrate,  $\sigma_s$ . How is this  $\sigma_c$  compared with  $\sigma_c$  of problem 1 above ?
3. If we assume there exist a thin interfacial compound(its thickness is 0.1 mm) made of 50% metal and 50% ceramic , thus, its thermomechanical properties ( $E$ ,  $G$ ,  $\nu$ ,  $\alpha$ ) are estimated by law of mixtures model, and  $G$  is the shear modulus that can be estimated by  $G=E/(2*(1+\nu))$ . Calculate the maximum shear stress at the interface. Where is the location of such maximum shear stress ?