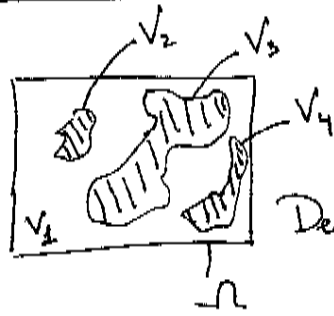


1

TWO FLUID EQUATIONS



Phases $i=1, 4$

Density: $\bar{\rho}_i = \frac{1}{\Omega} \int_{V_i} \rho_i dV$

$$\rho = \sum_{i=1}^N \rho_i$$

Velocity: $\bar{v}_i = \frac{1}{\int_{V_i} \rho_i} \int_{V_i} \rho_i \vec{v}_i dV$

$$\vec{v} = \frac{1}{\rho} \sum_{i=1}^N \rho_i \bar{v}_i$$

Internal Energy: $\bar{u}_i = \frac{1}{\int_{V_i} \rho_i} \int_{V_i} \rho_i u_i dV$; $u = \frac{1}{\rho} \sum_{i=1}^N \rho_i \bar{u}_i$

We can define the material derivative for each phase: $\frac{D_i}{Dt} = \frac{\rho}{\rho t} + \vec{v}_i \cdot \nabla$ and based on

this, the conservation of mass for each phase will be: $\int_V \frac{\rho \bar{\rho}_i}{\rho t} + \int_S \rho_i \vec{v}_i \cdot \vec{n} dS = \int_V \left(\sum_{\substack{j=1 \\ j \neq i}}^N J_{ji} \right) dV$

V and S are the total control volume and the exterior surface (with normal vector pointing outwards \vec{n}) and

J_{ji} is the flux of mass between phase j and phase i . $J_{ji} = -J_{ij}$
 using the divergence theorem we get the continuity equation

$$\frac{\rho \bar{\rho}_i}{\rho t} + \nabla \cdot (\rho_i \vec{v}_i) - \sum_{\substack{j=1 \\ j \neq i}}^N J_{ji} = 0$$

Individual phase continuity equation.

$\sum_{i=1}^N$

$$\frac{\rho S}{\rho t} + \nabla \cdot (\rho \vec{v}) = 0$$

Continuity eq.

$$\frac{\rho}{\rho t} \left(\sum_i \vec{v}_i \right) + \nabla \cdot \left(\sum_i \vec{v}_i \vec{v}_i \right) = \nabla \cdot \bar{\bar{\Sigma}}_i + \sum_i \vec{g}_i + \sum_{j=1}^N \vec{P}_{ij}$$

$\bar{\bar{\Sigma}}_i$ is the stress tensor in the phase i

\vec{P}_{ij} is the flux of momentum from phase j to i . It is defined so that $\vec{P}_{ii} = 0$ and $\vec{P}_{ij} = -\vec{P}_{ji}$

We define a relative velocity as:

$$\vec{w}_i = \vec{v}_i - \vec{v} \quad \vec{v} = \frac{1}{\rho} \sum_i \rho_i \vec{v}_i \quad \text{and, by definition,}$$

$$\sum_{i=1}^N \rho_i \vec{w}_i = 0$$

$$\sum_{i=1}^N \rho_i \vec{v}_i \vec{v}_i = \sum_{i=1}^N \rho_i \vec{v} \vec{v} + 2 \left(\sum_{i=1}^N \rho_i \vec{w}_i \right) \vec{v} + \sum_{i=1}^N \rho_i \vec{w}_i \vec{w}_i$$

$$\sum_{i=1}^N \rho_i \vec{g}_i = \rho \vec{g} \quad ; \quad \sum_{i=1}^N \bar{\bar{\Sigma}}_i = \bar{\bar{\Sigma}}$$

The equation of conservation of momentum for all the phases

$$\frac{\rho}{\rho t} (\rho \vec{v}) + \nabla \cdot (\rho \vec{v} \vec{v}) = \nabla \cdot \left[\bar{\bar{\Sigma}} - \sum_{i=1}^N \left(\rho_i \vec{w}_i \vec{w}_i \right) \right] + \rho \vec{g}$$

$$\sum_i \frac{D_i \vec{v}_i}{Dt} = \nabla \cdot \bar{\bar{\Sigma}}_i + \sum_i \vec{g}_i + \sum_{j=1}^N \left(\vec{P}_{ij} - \rho_j \vec{v}_i \right)$$

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Energy Equation

$$\frac{\rho(\sum_i \vec{S}_i \cdot \vec{E}_i)}{\rho t} + \nabla \cdot (\sum_i \vec{S}_i \cdot \vec{E}_i \vec{v}_i) = \nabla \cdot (\vec{W}_i - \vec{q}_i) + \sum_i \vec{S}_i \cdot \vec{S}_i \cdot \vec{v}_i + \sum_{\substack{j=1 \\ j \neq i}}^N E_{ji}$$

\vec{E}_i is the total energy for phase i , $\vec{E}_i = \vec{u}_i + \frac{|\vec{v}_i|^2}{2}$
 \vec{W}_i is the term that accounts for work done by moving external surfaces: $(-p\vec{I} + \vec{T}') \cdot \vec{v}_i$
 \vec{q}_i is the heat flux from phase i through the external surface.

E_{ji} is the exchange of energy between phase j and i

Adding all phases up, we get:

$$\int E = \sum_{i=1}^N \int \vec{S}_i \cdot \vec{E}_i = \int u + \frac{1}{2} \int |\vec{v}|^2 + \sum_{i=1}^N \frac{\int \vec{S}_i \cdot \vec{W}_i}{2}$$

$$\frac{\partial(\int E)}{\partial t} + \nabla \cdot (\int E \vec{v}) = \nabla \cdot [\vec{W} - \vec{q} - \sum_{i=1}^N (\vec{S}_i \cdot \vec{E}_i \vec{W}_i)] + \int \vec{S}_i \cdot \vec{v}_i + \sum_{i=1}^N \sum_{j \neq i} \vec{S}_i \cdot \vec{q}_i \cdot \vec{W}_i$$

$$\vec{W} = \sum_{i=1}^N \vec{W}_i, \quad \vec{q} = \sum_{i=1}^N \vec{q}_i$$

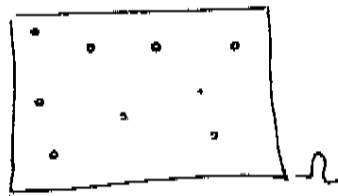
We can also write the conservation of energy for phase j as:

$$\int \vec{S}_i \frac{D_i \vec{E}_i}{Dt} = \nabla \cdot (\vec{W}_i - \vec{q}_i) + \sum_i \vec{S}_i \cdot \vec{S}_i \cdot \vec{v}_i + \sum_{\substack{j=1 \\ j \neq i}}^N (E_{ji} - J_{ji} \vec{E}_i)$$

4

Dispersed particles in a fluid continuous phase

Small spherical particles in a fluid with volume fraction much smaller than one $\alpha \ll 1$.



$$r_p \ll r_\Omega$$

$$N_\Omega \gg 1$$

The particles are small compared to the averaging volume and there are many of them.

Continuity

$$\frac{\rho}{\rho t} (1-\alpha) \rho_f + \nabla \cdot [(1-\alpha) \rho_f \vec{v}_f] = 0$$

$$\frac{\rho}{\rho t} (\alpha \rho_s) + \nabla \cdot [\alpha \rho_s \vec{v}_s] = 0$$

no phase change

Conservation of Momentum

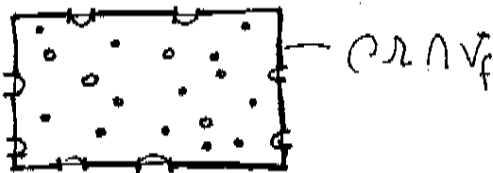
$$\frac{\rho}{\rho t} [(1-\alpha) \rho_f \vec{v}_f] + \nabla \cdot [(1-\alpha) \rho_f \vec{v}_f \vec{v}_f] = -\nabla [(1-\alpha) P_f] + \nabla \cdot [(1-\alpha) \vec{\tau}_f] -$$

$$-\nabla \cdot [(1-\alpha) \vec{\pi}_f] + (1-\alpha) \rho_f \vec{g} - \frac{1}{\Omega} \int_{S \in \Omega} P_f' \vec{n} dS_i + \frac{1}{\Omega} \int_{S_i \in \Omega} \vec{\tau}_f' \cdot \vec{n} dS_i$$

The tildes mean relative press and velocity

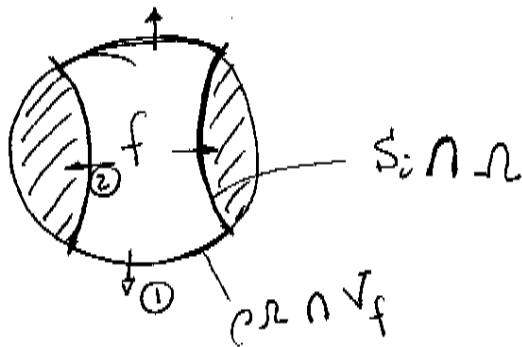
$$-\nabla [(1-\alpha) P_f] = -\nabla \cdot \left(\frac{1}{\Omega} \int_{V_f} P \vec{\mathbb{I}} dV \right) = -\frac{1}{\Omega} \int_{V_f} \nabla \cdot (P \vec{\mathbb{I}}) dV =$$

$$= -\frac{1}{\Omega} \int_{\partial V_f} P \vec{\mathbb{I}} \cdot \vec{n} dS = -\frac{1}{\Omega} \int_{\partial \Omega \cap V_f} P \vec{\mathbb{I}} \cdot \vec{n} dS$$



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This term $-\frac{1}{\rho} \int_{\partial \Omega} p \bar{\mathbb{I}} \cdot \vec{n} dS$ together with $-\frac{1}{\rho} \int_{S_i \cap \Omega} p_f' \vec{n} dS$ represent the total effect of pressure on the fluid



$$-\frac{1}{\rho} \int_{\partial \Omega} p \bar{\mathbb{I}} \cdot \vec{n} dS - \frac{1}{\rho} \int_{S_i \cap \Omega} p_f' \vec{n} dS \approx -\frac{1}{\rho} \int_{\partial \Omega} p_f' \vec{n} dS = -\frac{1}{\rho} \int_{\Omega} \nabla p_f' dV$$

So we get:

$$(1-\alpha) \rho_f \frac{\partial \vec{v}_f}{\partial t} + (1-\alpha) \rho_f \vec{v}_f \cdot \nabla \vec{v}_f = -\nabla p_f + \nabla \cdot [(1-\alpha) \bar{\mathbb{C}}_f'] - \nabla \cdot [(1-\alpha) \bar{\mathbb{T}}_f] + (1-\alpha) \rho_f \vec{g} + \frac{1}{\rho} \int_{S_i \cap \Omega} \bar{\mathbb{C}}_f' \cdot \vec{n} dS_i$$

We can also group together the viscous stresses:

$$\nabla \cdot \frac{1}{\rho} \int_{\partial \Omega} \bar{\mathbb{C}}_f' \cdot \vec{n} dV + \frac{1}{\rho} \int_{S_i \cap \Omega} \bar{\mathbb{C}}_f' \cdot \vec{n} dS_i \approx \nabla \cdot \bar{\mathbb{T}}_m$$

$\bar{\mathbb{T}}_m$ is the equivalent viscous stress tensor:

$$\bar{\mathbb{T}}_m = \mu \left[\nabla \vec{v}_m + (\nabla \vec{v}_m)^T \right] - \frac{2}{3} \mu (\nabla \cdot \vec{v}_m) \bar{\mathbb{I}}$$

$v_m = (1-\alpha) \vec{v}_f + \alpha \vec{v}_s$ and $\mu = \mu_f \left(1 + \alpha \frac{\mu_f + 5/2 \mu_s}{\mu_f + \mu_s} \right)$

$\left(1 + \frac{5}{2} \alpha \right) \mu_f$ for solids
 $(1+\alpha) \mu_f$ for bubbles