

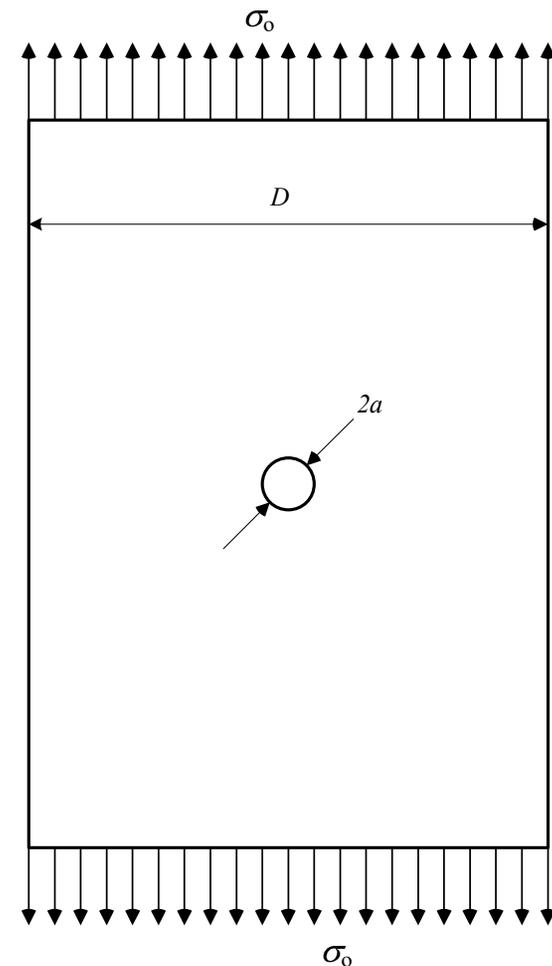
# Stress Concentrations

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- A “stress concentration” refers to an area in a object where stress increases over a very short distance (i.e., where a high stress gradient exists)
- Stress concentrations typically occur due to some localized change in geometry (near holes, fillets, corners, grooves, cracks, etc)
- These changes in geometry are often called “stress risers”

# Stress Concentration Near a Circular Hole

- In 1898 Ernst Kirsch (a German engineer) published a solution for the elastic stresses near a circular hole in an isotropic “infinitely large” thin plate (the Kirsch solution is derived in Sec 3.13 of the Shukla and Dally textbook)
- In practice, a thin plate can be considered to be “infinitely large” if the hole diameter is small compared to the in-plane plate dimensions (if  $a/D < \sim 0.05$ , say)



# Stress Concentration Near a Circular Hole

- Stresses along the x-axis in an infinite plate predicted by the Kirsch solution:

$$\sigma_{rr} = \sigma_{xx} = \frac{\sigma_o}{2} \left( 1 - \frac{a^2}{x^2} \right) \frac{3a^3}{x^2}$$

$$\sigma_{\theta\theta} = \sigma_{yy} = \frac{\sigma_o}{2} \left( 2 + \frac{a^2}{x^2} + \frac{3a^4}{x^4} \right)$$

$$\tau_{r\theta} = \tau_{xy} = 0$$

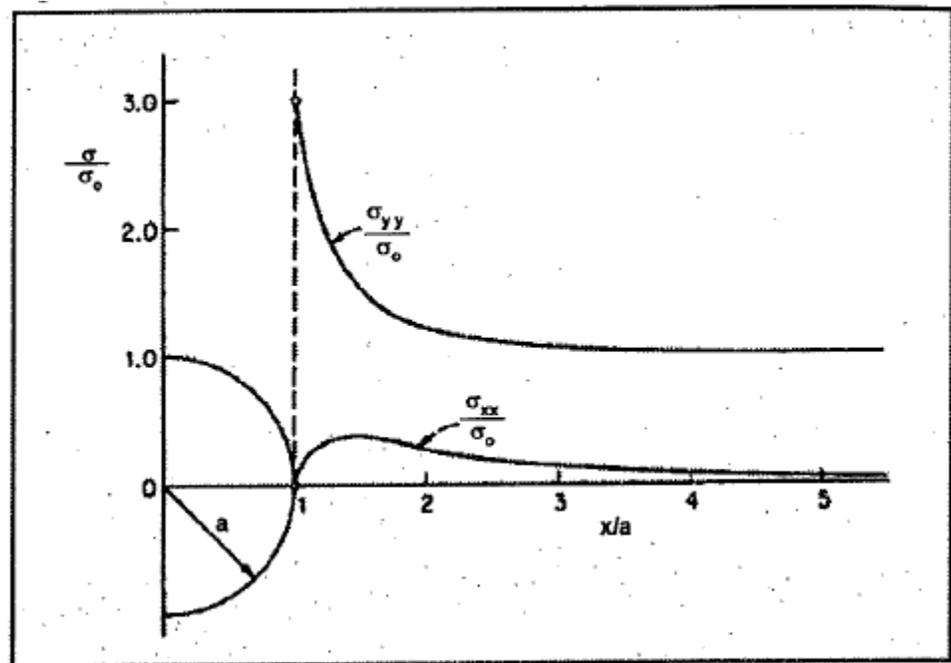


Figure 3.6: Distribution of  $\sigma_{xx}/\sigma_o$  and  $\sigma_{yy}/\sigma_o$  along the x-axis

# Stress Concentration Near a Circular Hole

- Stresses at the edge of the hole (at  $x = a$ ):

$$\sigma_{rr} = \sigma_{xx} = 0$$

$$\sigma_{\theta\theta} = \sigma_{yy} = 3\sigma_o$$

$$\tau_{r\theta} = \tau_{xy} = 0$$

- The stress concentration factor for a circular hole in an infinite plate:

$$K_t = \frac{\sigma_{yy}}{\sigma_o} = 3$$

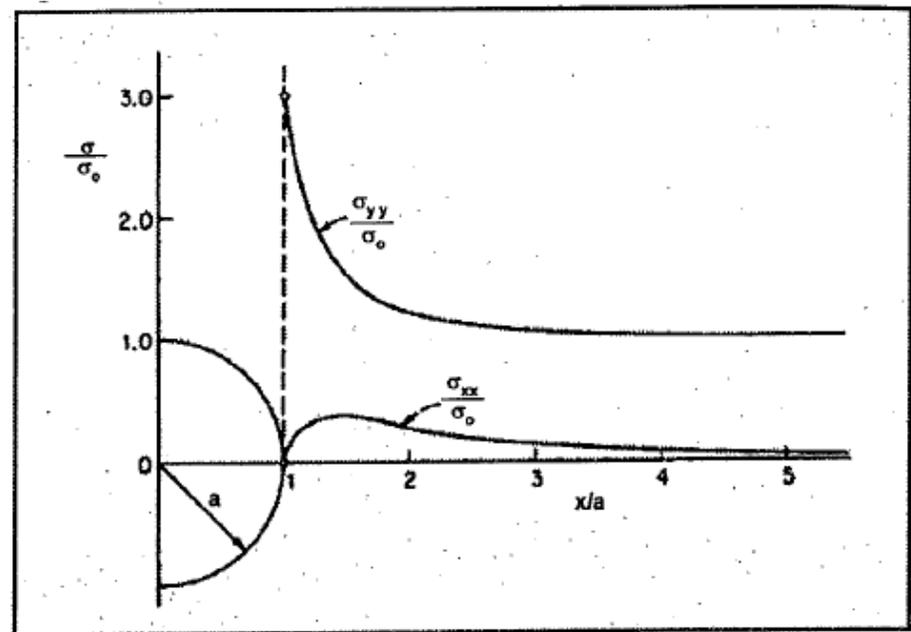
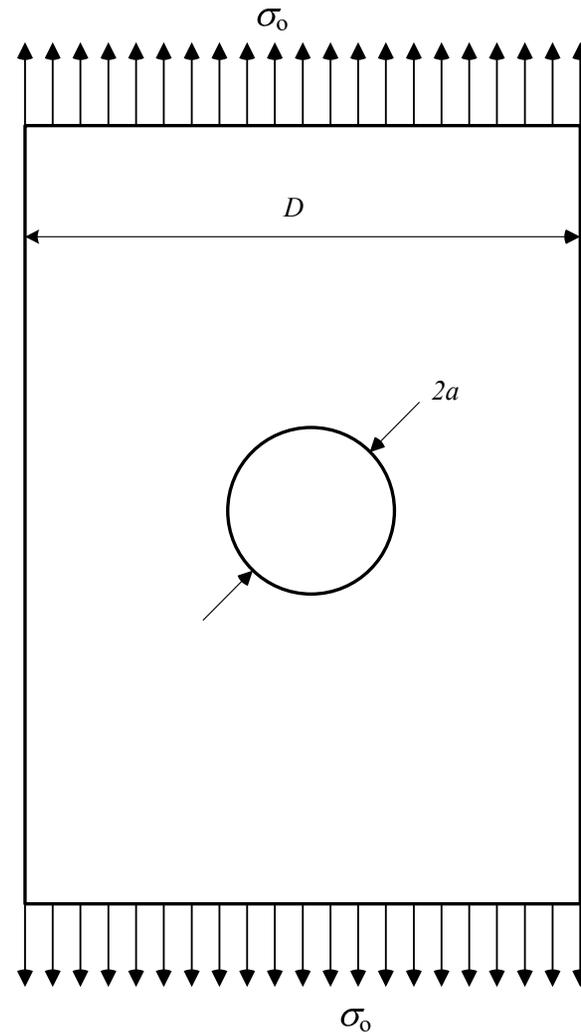


Figure 3.6: Distribution of  $\sigma_{xx}/\sigma_o$  and  $\sigma_{yy}/\sigma_o$  along the x-axis

# Stress Concentration Near a Circular Hole

- If  $a/D > 0.05$  then the plate is “finite” and the Kirsch solution is no longer valid
- Stress concentration factors for a circular holes in finite plates have been measured experimentally for a range of  $a/D$  ratios (usually using photoelasticity), and tabulated in the form of curve-fits in reference handbooks ...required several years and many contributors



# Stress Concentration Near a Circular Hole

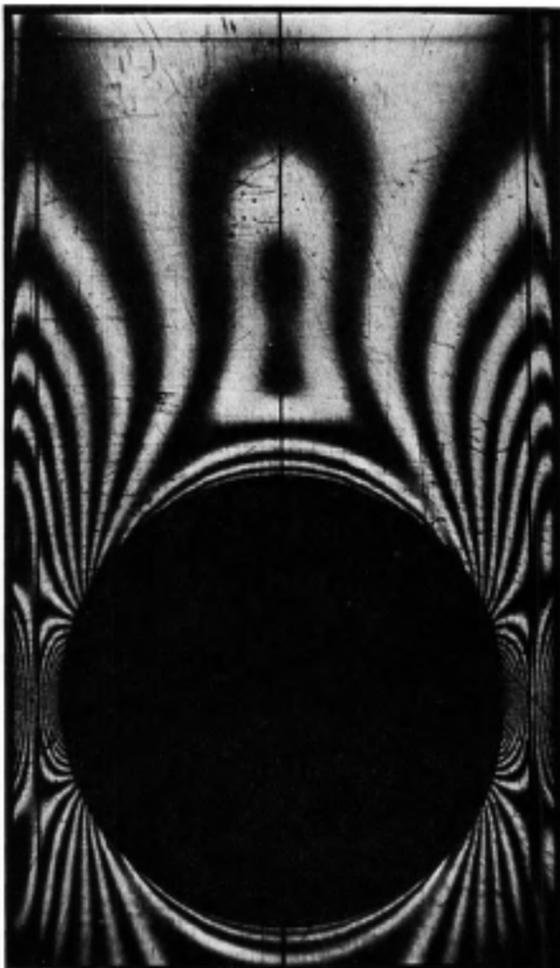


FIG. 8 BAR WITH LARGE HOLE

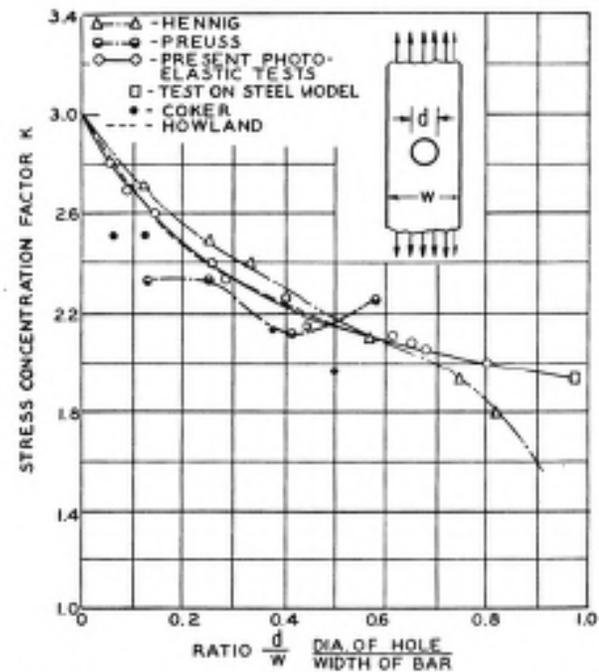


FIG. 10 STRESS CONCENTRATION FACTOR VS.  $d/w$  FOR FLAT BAR WITH HOLE

- Example: Wahl, A.M., and Beeuwkes, R., “Stress Concentration Produced by Holes and Notches”, Transaction of the ASME; Applied Mechanics, Vol 56 (11) , 1930

# Stress Concentration Near a Circular Hole

- Two different definitions of the stress concentration factors are in common use:

-based on the gross stress :

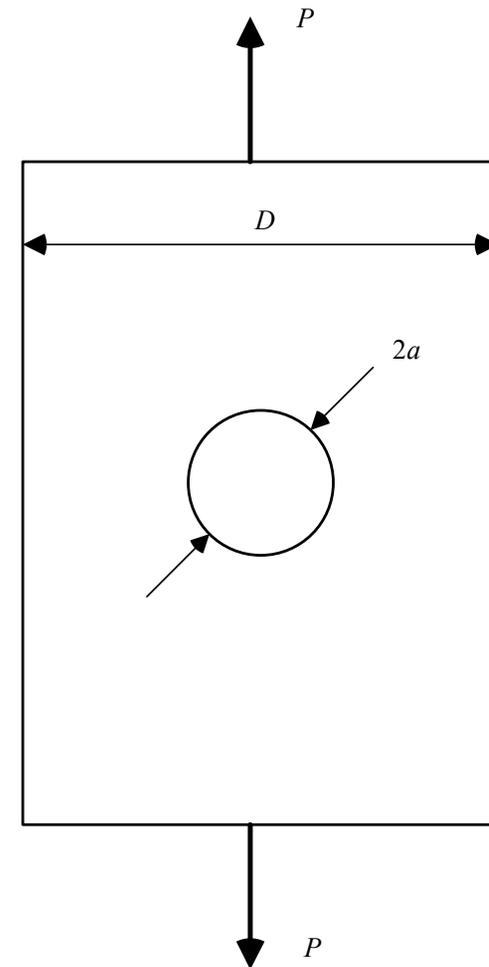
$$K_t^g = \frac{\sigma_{yy}^{\max}}{\sigma_g} \quad \text{where} \quad \sigma_g = \frac{P}{t * D}$$

( $\sigma_g$  remains constant as  $a$  increases)

-based on the net stress:

$$K_t^n = \frac{\sigma_{yy}^{\max}}{\sigma_n} \quad \text{where} \quad \sigma_n = \frac{P}{t * (D - 2a)}$$

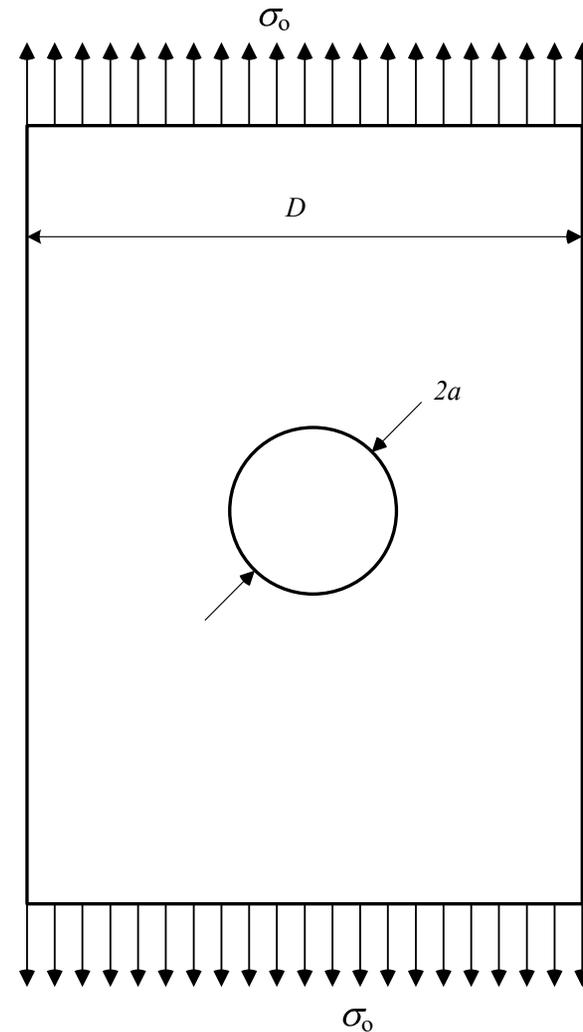
( $\sigma_n$  increases as  $a$  increases)



# Stress Concentration Near a Circular Hole

- Example: from Roark's Formulas for Stress and Strain (2002):

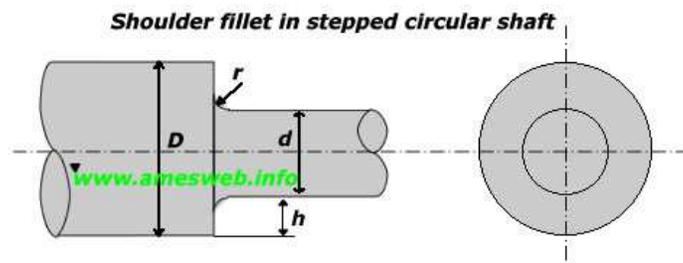
$$K_t^n = 3.00 - 3.14\left(\frac{2a}{D}\right) + 3.67\left(\frac{2a}{D}\right)^2 - 1.53\left(\frac{2a}{D}\right)^3$$



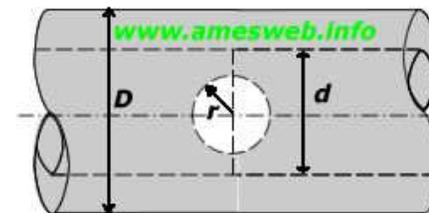
# Tabulated Stress Concentration Factors

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- Stress concentration factors for many types of “stress risers” have been tabulated...for example:
  - Young, W.C., and Budynas, R.G., Roark’s Formulas for Stress and Strain, 7<sup>th</sup> edition, McGraw-Hill, (2002)
  - online tabulations: <http://www.amesweb.info/>



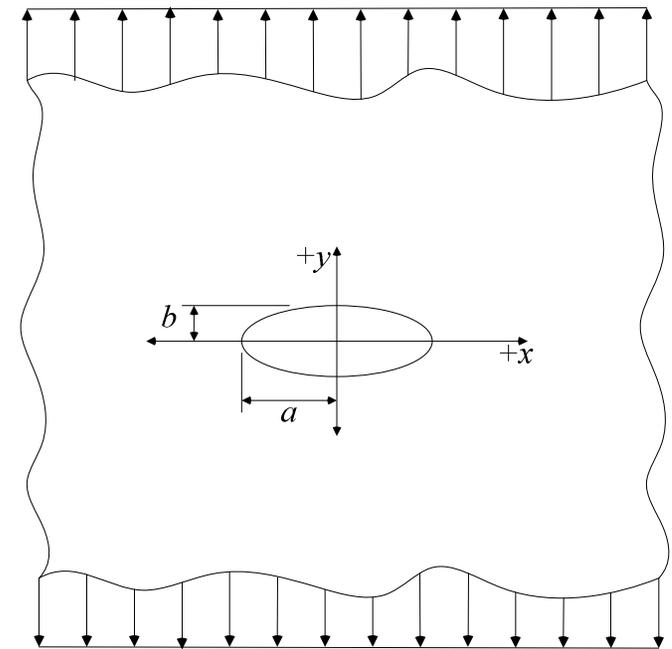
**Transverse circular hole in round bar**



# Stress Concentration Near an Elliptical Hole

- In 1913 Charles Inglis (a British mathematician) published a solution for the elastic stresses near an elliptical hole in an isotropic infinitely large thin plate (the Inglis solution is discussed in Sec 4.2)
- In this case the stress concentration depends on both the aspect ratio of the hole ( $a/b$ ) and on the size of the plate

$\sigma =$  uniaxial stress applied to infinitely large plate



# Stress Concentration Near an Elliptical Hole

- For an infinite plate the stresses along the  $x$ -axis (i.e., for  $x \geq a$ ,  $y = 0$ ) are given by:

$$\sigma_{xx}(x) = F_{1(s)} - F_{2(s)}$$

$$\sigma_{yy}(x) = F_{1(s)} + F_{2(s)}$$

$$\tau_{xy}(x) = 0$$

where:

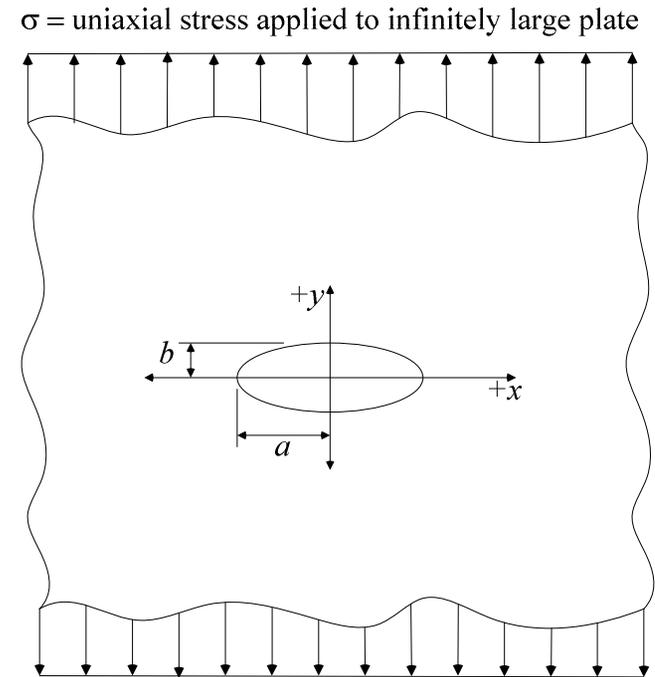
$$F_{1(s)} = \frac{\sigma}{2} \left[ 1 + \frac{2(1+m)}{s^2 - m} \right]$$

$$F_{2(s)} = \frac{\sigma}{2} \left\{ 1 + \frac{m^2 - 1}{s^2 - m} \left[ 1 + \left( \frac{m-1}{s^2 - m} \right) \left( \frac{3s^2 - m}{s^2 - m} \right) \right] \right\}$$

$$s = \frac{x}{2B} + \sqrt{\left( \frac{x}{2B} \right)^2 - m}$$

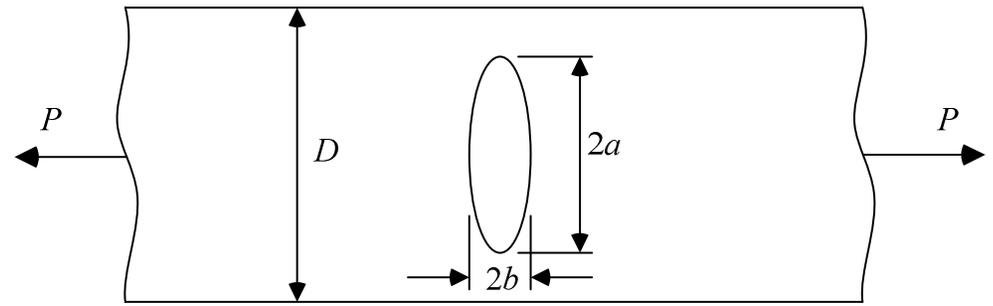
$$B = \frac{1}{2}(a+b)$$

$$m = \frac{a-b}{a+b}$$



# Stress Concentration Near an Elliptical Hole

- For a finite plate:



$$K_t^n = C_1 + C_2 \left( \frac{2a}{D} \right) + C_3 \left( \frac{2a}{D} \right)^2 + C_4 \left( \frac{2a}{D} \right)^3$$

$$C_1 = 1.000 + 0.000\sqrt{a/b} + 2.000a/b$$

$$C_2 = -0.351 - 0.021\sqrt{a/b} - 2.483a/b$$

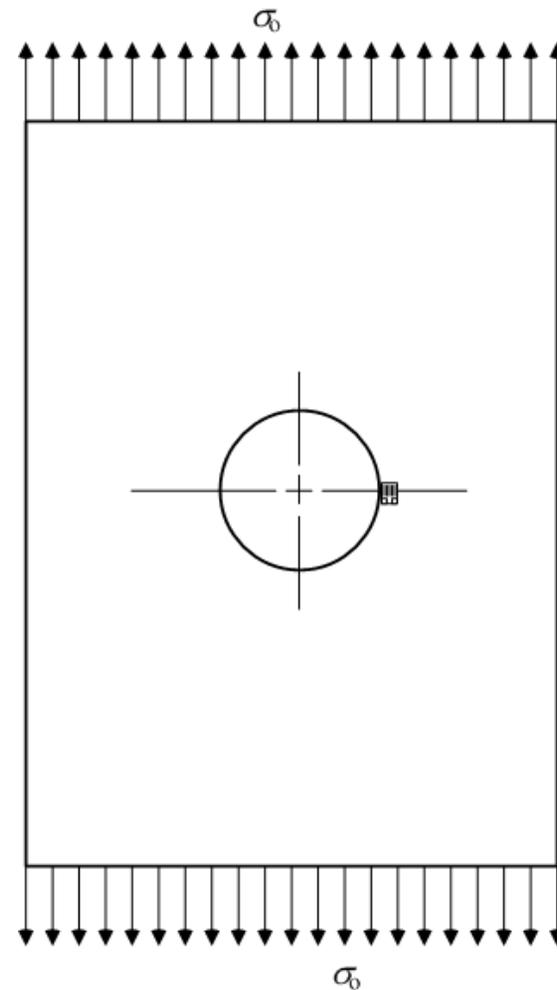
$$C_3 = 3.621 - 5.183\sqrt{a/b} + 4.494a/b$$

$$C_4 = -2.270 + 5.204\sqrt{a/b} - 4.011a/b$$

# Measuring Stress Concentrations Using Strain Gages

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- In general, even the smallest of commercial resistance strain gages are too large to measure strain concentrations near stress risers:

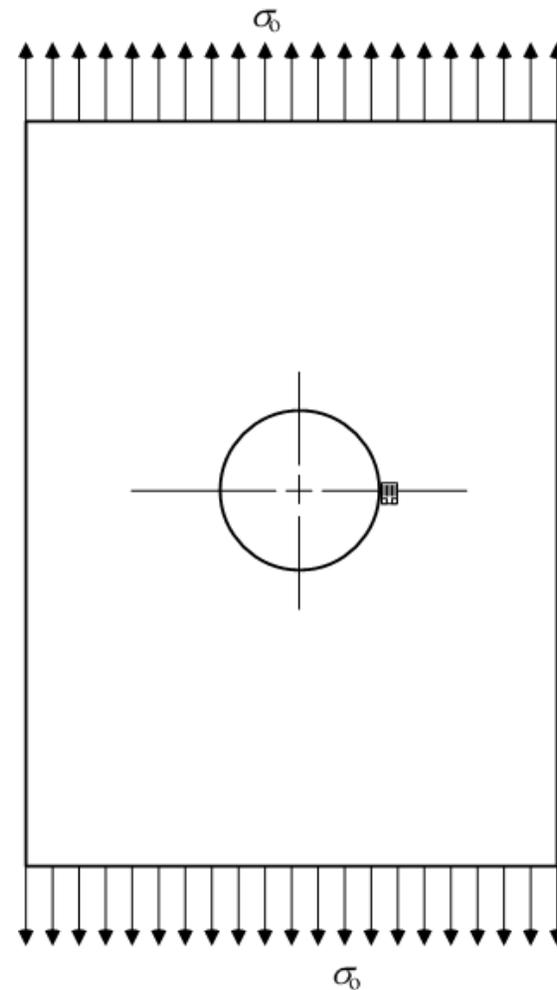


# Measuring Stress Concentrations Using Strain Gages

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FIG. 8 BAR WITH LARGE HOLE

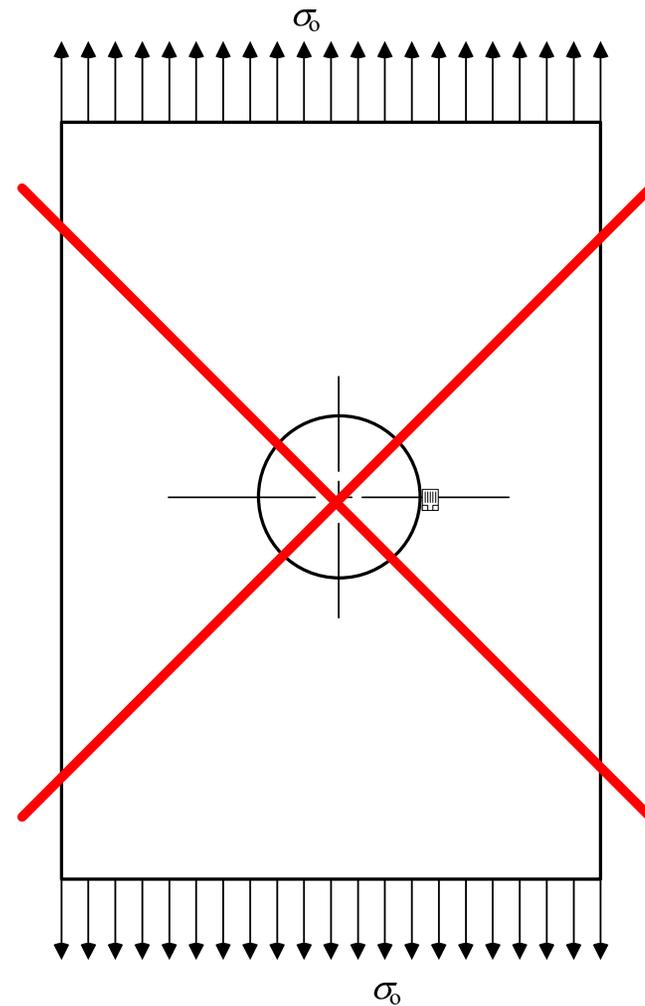


# Measuring Stress Concentrations Using Strain Gages

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- In general, even the smallest of commercial resistance strain gages are too large to measure strain concentrations near stress risers:

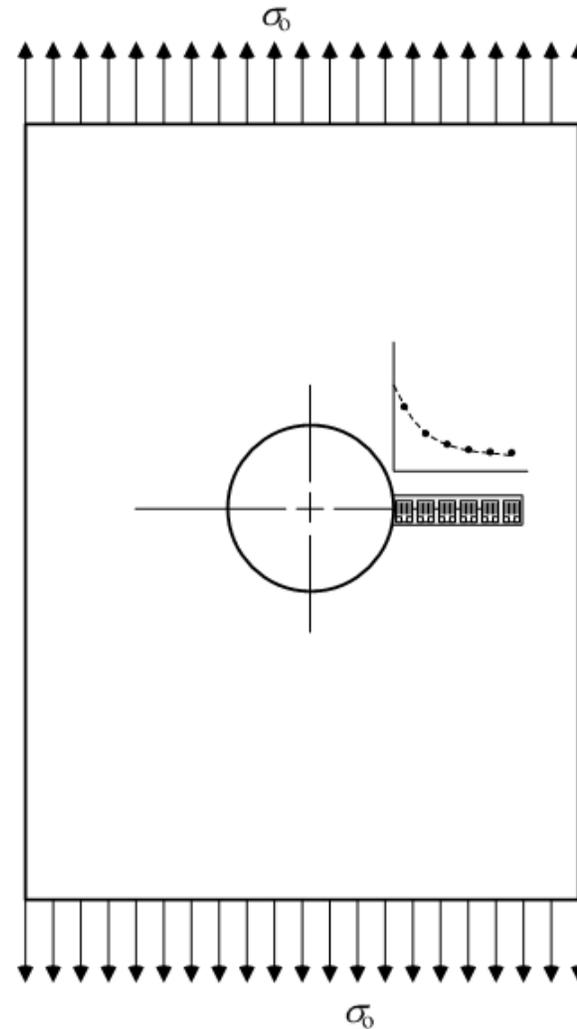
...a poor experimental approach



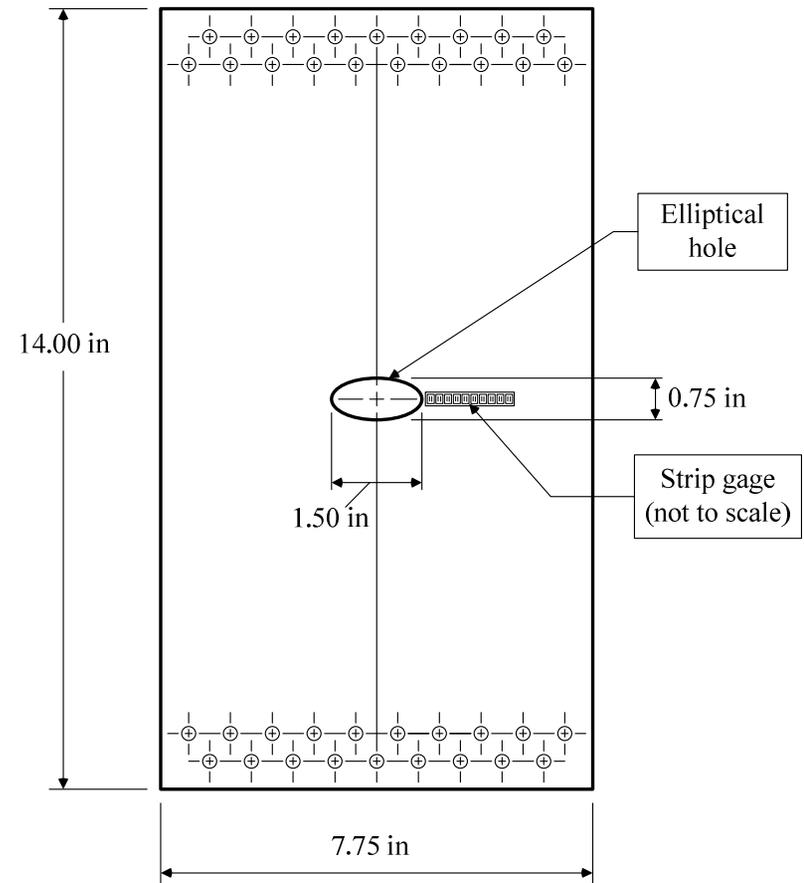
# Measuring Stress Concentrations Using Strain Gages

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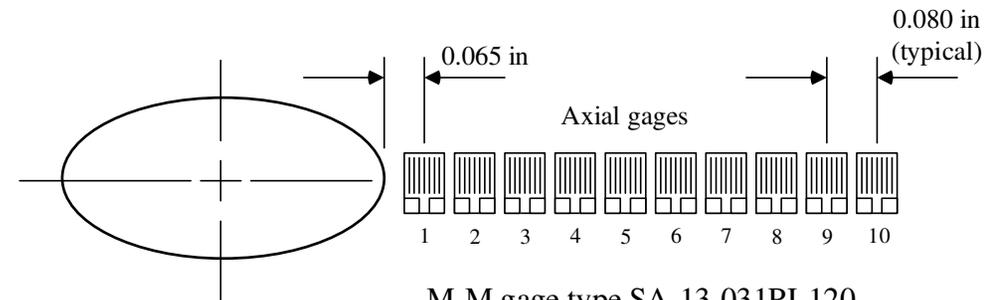
- Instead, use a commercial “strip gage” and extrapolate experimental measurements to edge of stress riser



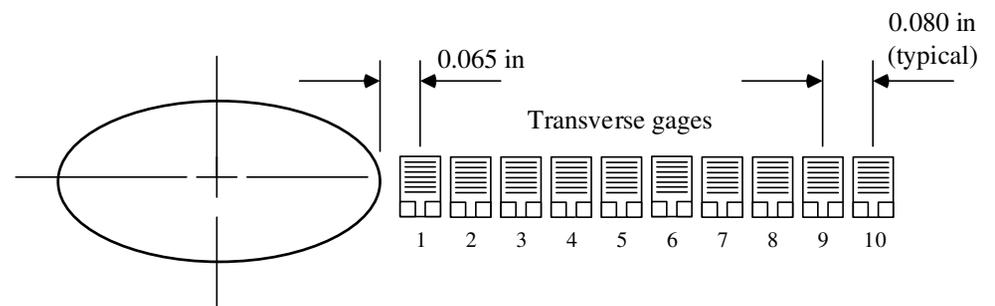
# Pseudo Lab #6: Stress and Strain Concentrations



# Pseudo Lab #6: Stress and Strain Concentrations



M-M gage type SA-13-031PJ-120  
Gage factor = 2.12,  $K_t = 2.0\%$



M-M gage type EA-13-031MF-120  
Gage factor = 2.09,  $K_t = 1.2\%$

# Corrections for Biaxial Rosettes With Differing Transverse Sensitivity Coefficients

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$$\epsilon_x = \frac{(1 - \nu_o K_t^x) \epsilon_{mx} - (1 - \nu_o K_t^y) K_t^x \epsilon_{my}}{1 - K_t^x K_t^y}$$

$$\epsilon_y = \frac{(1 - \nu_o K_t^y) \epsilon_{my} - (1 - \nu_o K_t^x) K_t^y \epsilon_{mx}}{1 - K_t^x K_t^y}$$

$\epsilon_{mx}, \epsilon_{my}$  = strains measured in the  $x$ - and  $y$ - directions

$K_t^x, K_t^y$  = Transverse sensitivity coefficients for gages in the  $x$ - and  $y$ - directions

# Pseudo Lab #6: Stress and Strain Concentrations

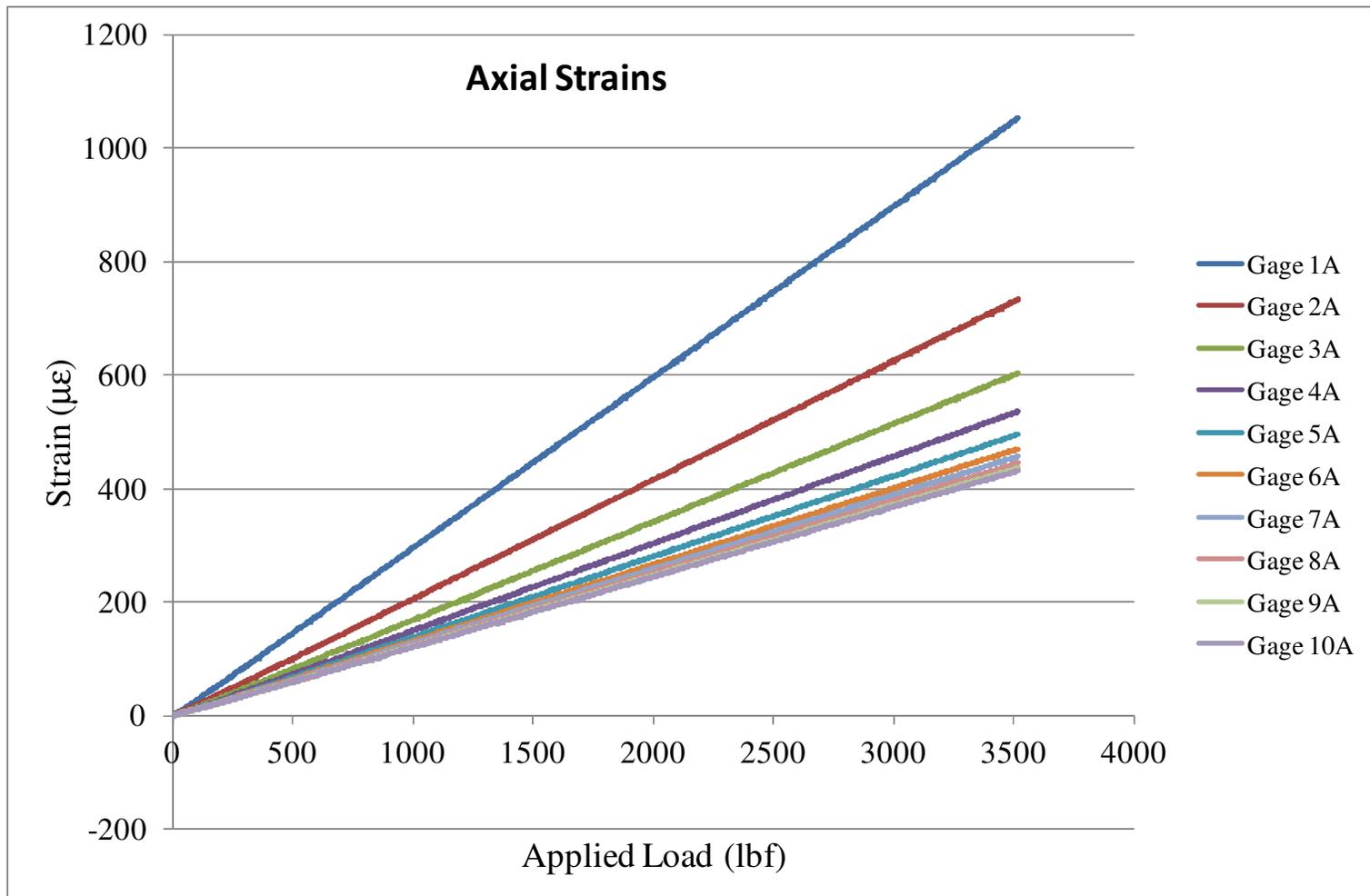
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## Goals:

- To compare stress distributions measured near an elliptical hole in a finite thin plate to those predicted for an infinite thin plate, and
- To compare the stress concentration factor measured for an elliptical hole in a finite thin plate to the value expected from a reference handbook.

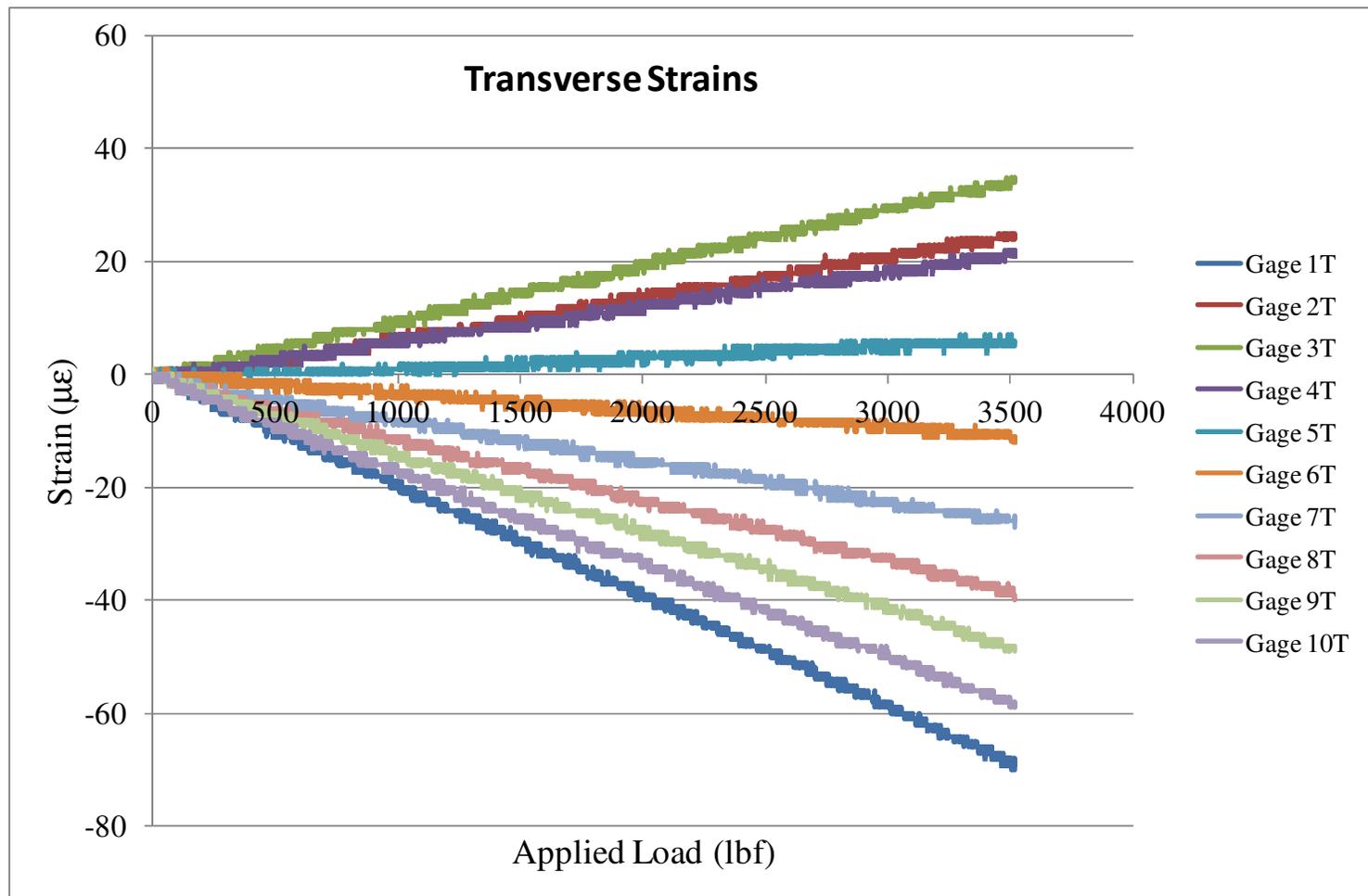
# Pseudo Lab #6: Stress and Strain Concentrations

## “Official Data” – Axial Strains



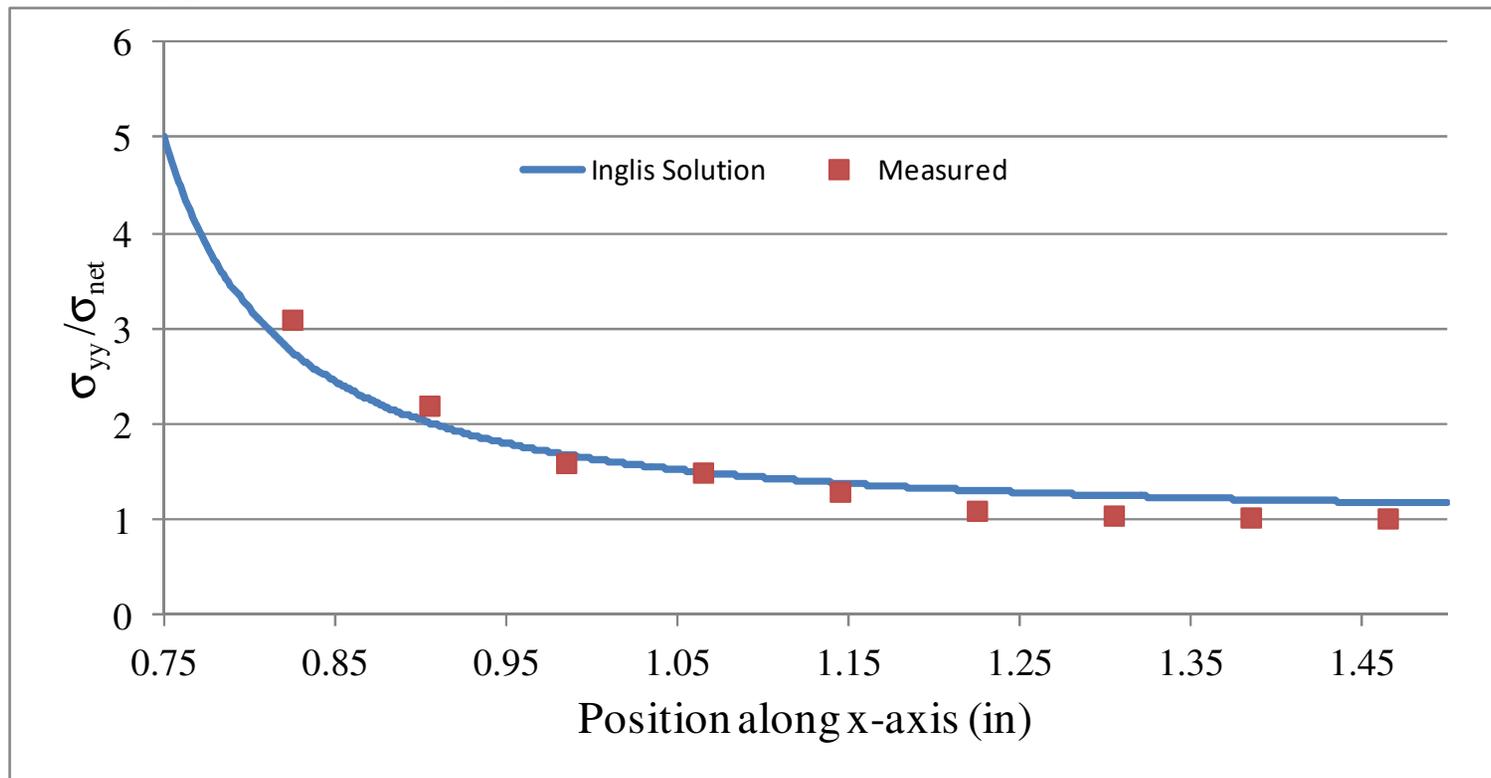
# Pseudo Lab #6: Stress and Strain Concentrations

## “Official Data” – Transverse Strains



# Pseudo Lab #6: Stress and Strain Concentrations

Goal 1: Compare stress distributions measured near an elliptical hole in a finite thin plate to those predicted for an infinite thin plate (Suggestion: compare normalized stresses)



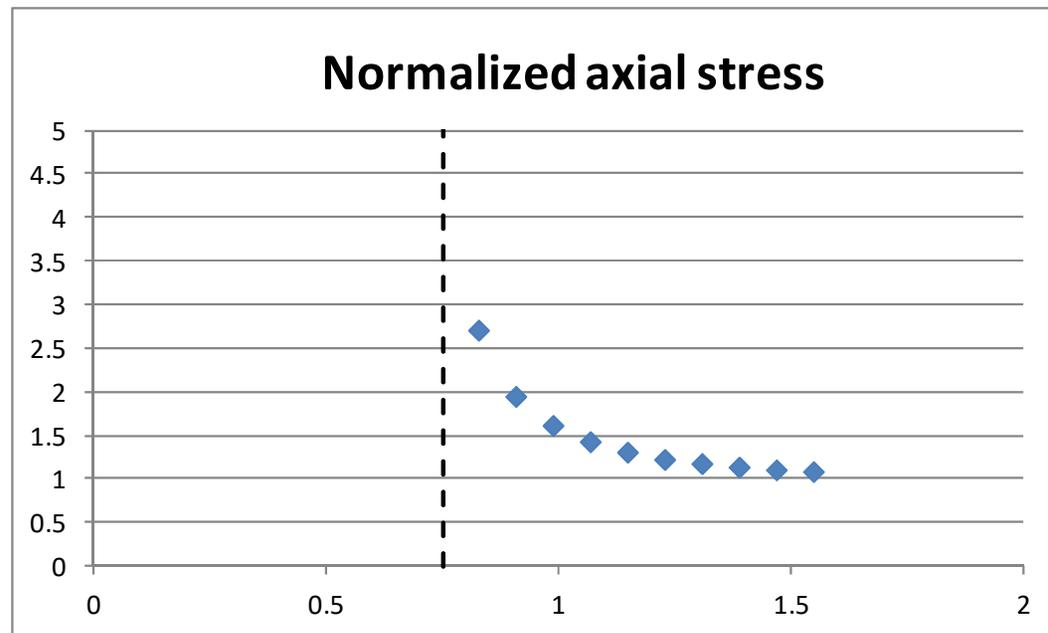
Note: as mentioned during class lecture, the measured values shown here are fictitious

# Pseudo Lab #6: Stress and Strain Concentrations

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Goal 2: To compare the stress concentration factor measured for an elliptical hole in a finite thin plate to the value expected from a reference handbook.

(Suggestion: extrapolate a curve fit)

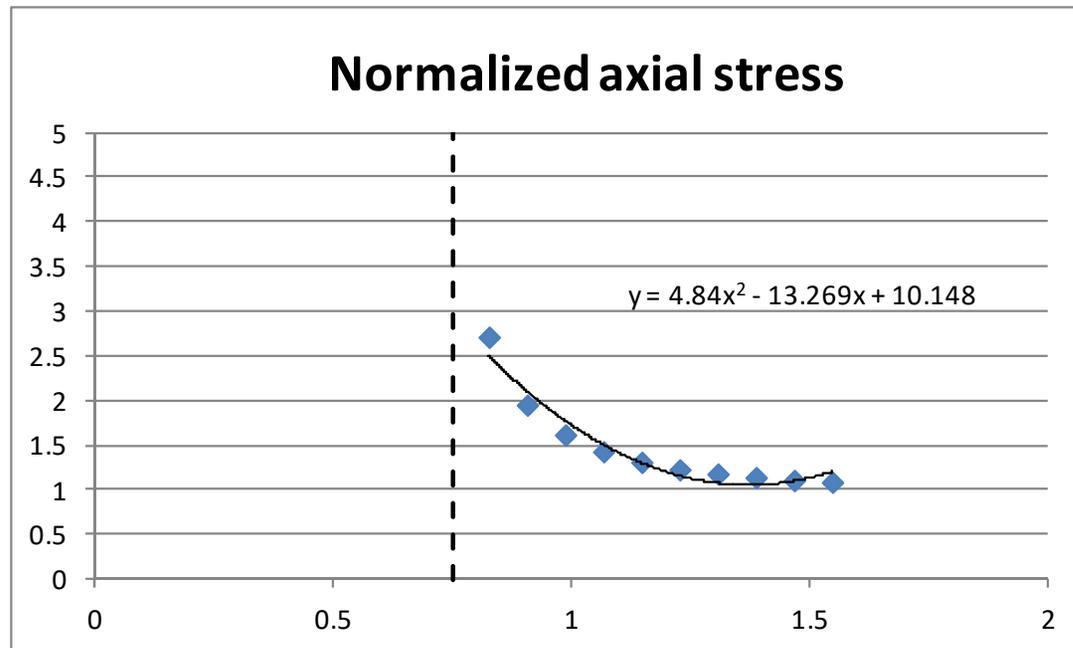


# Pseudo Lab #6: Stress and Strain Concentrations

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Goal 2: To compare the stress concentration factor measured for an elliptical hole in a finite thin plate to the value expected from a reference handbook.

....fit of fictitious data using a 2<sup>nd</sup>-order polynomial:

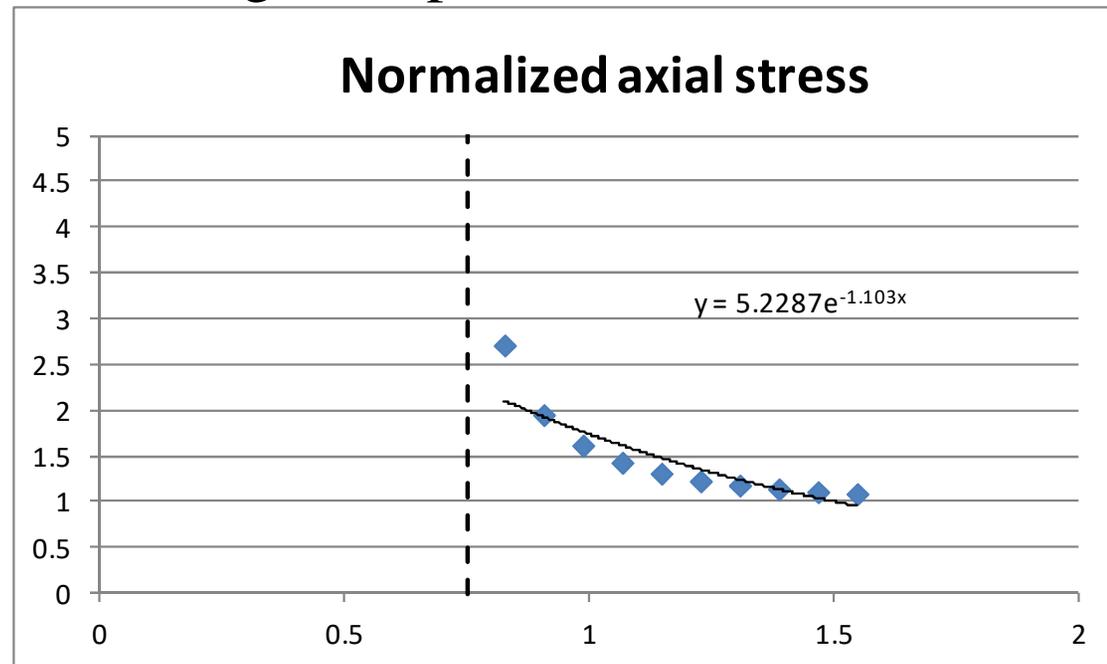


# Pseudo Lab #6: Stress and Strain Concentrations

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Goal 2: To compare the stress concentration factor measured for an elliptical hole in a finite thin plate to the value expected from a reference handbook.

....fit of fictitious data using an exponential:

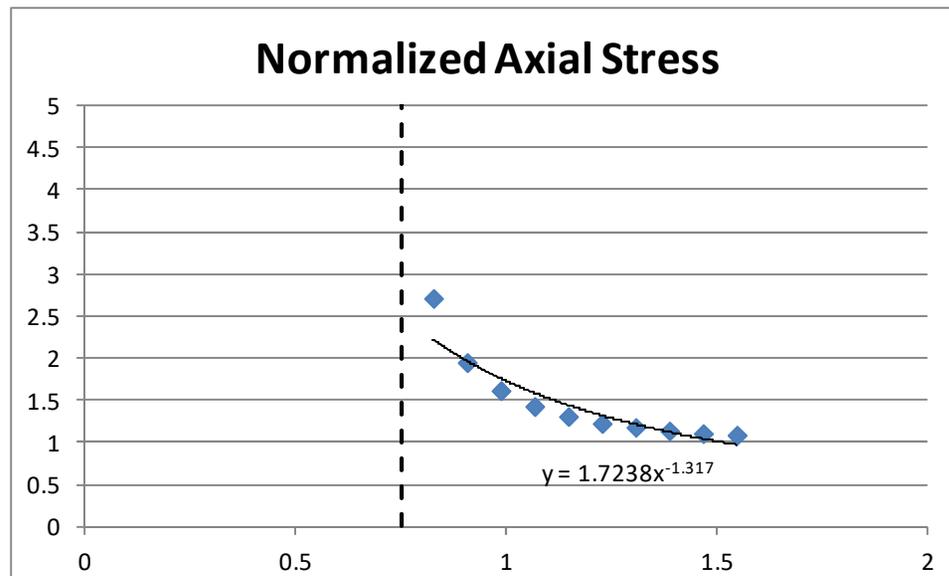


# Pseudo Lab #6: Stress and Strain Concentrations

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Goal 2: To compare the stress concentration factor measured for an elliptical hole in a finite thin plate to the value expected from a reference handbook.

....fit of fictitious data using a power law



# Pseudo Lab #6: Stress and Strain Concentrations

Goal 2: To compare the stress concentration factor measured for an elliptical hole in a finite thin plate to the value expected from a reference handbook.

....fit of fictitious data using an polynomial and (1/normalized stress)

