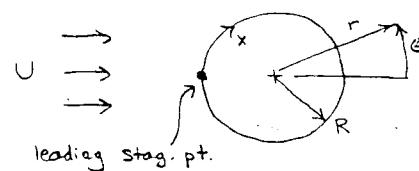


#### 8-4. Boundary Layer Separation on a Cylinder

Consider flow past a circular cylinder, as shown in Fig. 8-5. Assume that the pressure is given by the solution for irrotational flow.

- Use the results of Example 8.3-1 to determine  $u(x)$ , where  $x=0$  at the leading stagnation point.
- State the differential equation obtained for this geometry using the Kármán-Pohlhausen method.
- Use the equation from part (b) to compute  $\delta(0)$ .
- Solve the differential equation for  $h(x)$  numerically and determine the location of the separation point. You should obtain an angle of  $107^\circ$ ; the exact value for this idealized pressure field is reported to be  $104.5^\circ$  (Schlichting, 1968, p. 203). (Hint: The fourth-order Runge-Kutta method is satisfactory for the integration. To avoid the singularity at  $x=0$ , start the integration at a small, but nonzero, value of  $x$ .)

#### 8-4. Boundary Layer Separation on a Cylinder



- Determine  $u(x)$  from the results of Ex. 8.3-1, where  $x=0$  is the leading stagnation point. From eq. (8.3-12),

$$u = -U_\theta(R, \theta) = 2U \sin \theta.$$

Note that changes in  $x$  are proportional to changes in  $\theta$ , and that  $x=\infty$  for  $\theta=\pi$  and  $x=\pi R$  for  $\theta=0$ . Thus,

$$x(\theta) = a + b\theta$$

$$x(0) = \pi R \Rightarrow a = \pi R, \quad x(\pi) = 0 \Rightarrow b = R.$$

$$x(\theta) = R(\pi - \theta) \Rightarrow \theta = \pi - \frac{x}{R}$$

$$\sin \theta = \sin \left( \pi - \frac{x}{R} \right) = \sin \frac{x}{R}$$

$$\boxed{u(x) = 2U \sin \frac{x}{R}}$$

- State the DE for the cylinder obtained using Kármán-Pohlhausen. From eq. (8.4-52), the DE is of the form

$$\frac{dh}{dx} = \frac{2}{U} f(\lambda, \mu)$$

Setting  $L=R$  and using eqs (8.4-51),

$$\tilde{x} = \frac{x}{R}$$

$$h(\tilde{x}) = \left(\frac{\delta}{R}\right)^2 Re = \left(\frac{\delta}{R}\right)^2 \left(\frac{UR}{D}\right)$$

$$\tilde{u}(\tilde{x}) = \frac{u}{U} = 2 \sin \tilde{x}$$

$$\tilde{L}(\tilde{x}) = h \frac{d\tilde{u}}{d\tilde{x}} = 2h \cos \tilde{x}$$

$$\tilde{R}(\tilde{x}) = h^2 \tilde{u} \frac{d^2 \tilde{u}}{d\tilde{x}^2} = h^2 (2 \sin \tilde{x})(-2 \sin \tilde{x}) = -4h^2 \sin^2 \tilde{x}$$

Substitute these expressions into eq. (8.4-52) :

$$\frac{dh}{d\tilde{x}} = \frac{1}{\sin \tilde{x}} f(\tilde{L}, \tilde{R})$$

$$f(\tilde{L}, \tilde{R}) = \frac{[2 + (\frac{1}{6} - 2I_1 - I_4)\tilde{L} - (2I_2 - I_5)\tilde{L}^2 + 2I_3\tilde{L}^3 - (I_2 - 2I_3)\tilde{L}\tilde{R}]}{[I_1 + 3I_2\tilde{L} - 5I_3\tilde{L}^2]}$$

The constants  $I_n$  ( $n=1, 2, \dots, 5$ ) are given by eqs. (8.4-46) - (8.4-50). To obtain a more workable form, relate  $\tilde{L}$  and  $\tilde{R}$  to  $h$  and combine some of the constants.

$$\left(\frac{1}{6} - 2I_1 - I_4\right)\tilde{L} = 2\left(\frac{1}{6} - 2I_1 - I_4\right)h \cos \tilde{x} \equiv A_1 h \cos \tilde{x}$$

$$(I_5 - 2I_2)\tilde{L}^2 = 4(I_5 - 2I_2)h^2 \cos^2 \tilde{x} \equiv A_2 h^2 \cos^2 \tilde{x}$$

$$2I_3\tilde{L}^3 = 16I_3h^3 \cos^3 \tilde{x} \equiv A_3 h^3 \cos^3 \tilde{x}$$

$$-I_2\tilde{R} = -I_2(-4h^2 \sin^2 \tilde{x}) = 4I_2h^2 \sin^2 \tilde{x} \equiv B_1 h^2 \sin^2 \tilde{x}$$

$$2I_3\tilde{L}\tilde{R} = 2I_3(2h \cos \tilde{x})(-4h^2 \sin^2 \tilde{x}) = -16I_3h^3 \sin^2 \tilde{x} \cos \tilde{x}$$

$$\equiv B_2 h^3 \sin^2 \tilde{x} \cos \tilde{x}$$

$$3I_2\tilde{L} = 3I_2(2h \cos \tilde{x}) = 6I_2h \cos \tilde{x} \equiv C_1 h \cos \tilde{x}$$

$$-5I_3\tilde{L}^2 = -5I_3(4h^2 \cos^2 \tilde{x}) = -20I_3h^2 \cos^2 \tilde{x} \equiv C_2 h^2 \cos^2 \tilde{x}$$

The DE is now

$$\frac{dh}{d\tilde{x}} = \frac{2 + A_1 h \cos \tilde{x} + A_2 h^2 \cos^2 \tilde{x} + A_3 h^3 \cos^3 \tilde{x} + B_1 h^2 \sin^2 \tilde{x} + B_2 h^3 \sin^2 \tilde{x} \cos \tilde{x}}{\sin \tilde{x} (I_1 + C_1 h \cos \tilde{x} + C_2 h^2 \cos^2 \tilde{x})}$$

(c) Use the result of part (b) to compute  $\delta(0)$ .

For a symmetric object which is rounded at the leading stagnation point (e.g., a cylinder),  $dh/dx=0$  at  $x=0$ . Thus, the numerator on the right-hand side of the DE must vanish at  $x=0$ . Letting  $h(0)=h_0$ ,

$$0 = 2 + A_1 h_0 + A_2 h_0^2 + A_3 h_0^3$$

The physically significant root, calculated numerically, is

$$h_0 = 3.5262$$

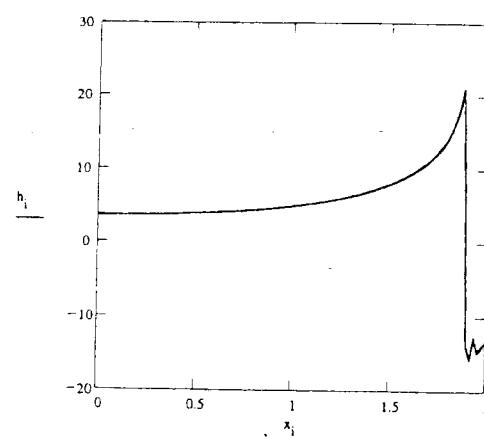
(d) Determine  $h(x)$  numerically and find the separation pt.

Plots are shown on the following pages. The separation point ( $\tilde{x}_s$ ) is defined by  $\tilde{L}(\tilde{x}_s) = -12$ . It is found that

$$\tilde{x}_s = \frac{x_s}{R} = 1.873$$

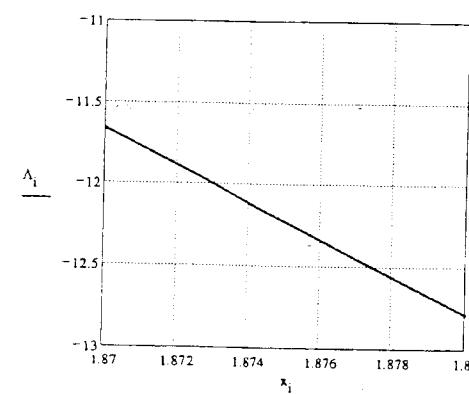
$$\text{Separation angle} = \left(\frac{1.873}{\pi}\right)(180^\circ) = 107.3^\circ$$

Dimensionless boundary layer thickness:



Note that the solution breaks down at about  $x = 1.9$ .

Shape factor near the separation point:



Boundary layer separation ( $A_i = -12$ ) occurs at  $x = 1.873$ .

Shape factor:

