

# Diffraction

## Fraunhofer and Fresnel Diffraction

Reports due this week



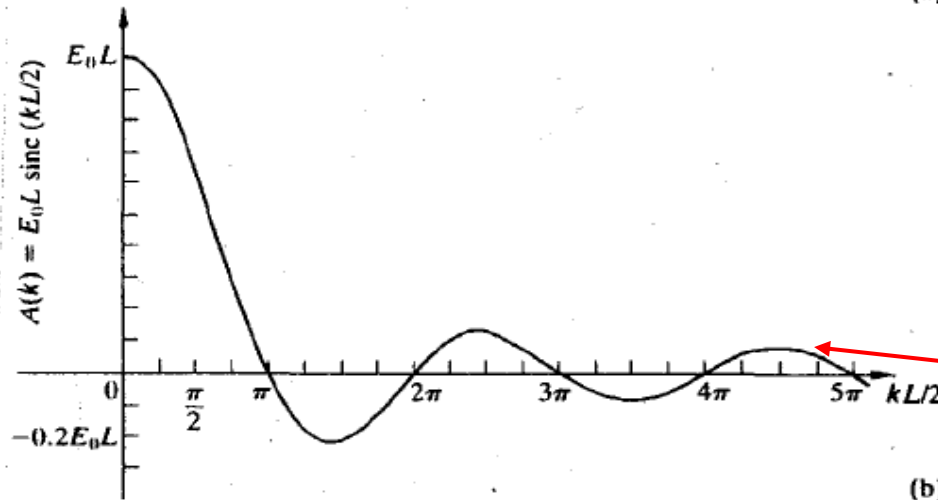
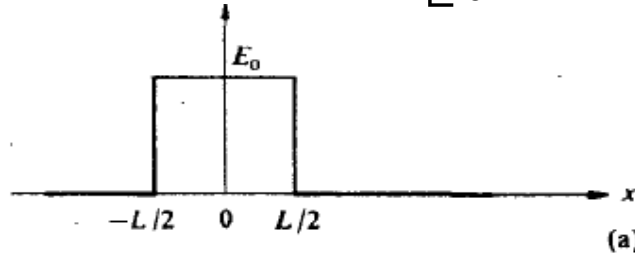
A Fabry-Perot wave meter. Free spectral range: 3000 GHz.  
Finesse 100,000.

Two light sources have a frequency difference of 4000 GHz. Can we resolve these two light sources?

A sodium atom has a doublet emission with a frequency difference of 0.1 GHz. Can we resolve the fine structure?

# Fourier Integrals and Fourier Transforms

$$f(x) = \frac{1}{\pi} \left[ \int_0^{\infty} A(k) \cos(kx) dk + \int_0^{\infty} B(k) \sin(kx) dk \right]$$



$$A(k) = \int_{-\infty}^{\infty} f(x) \cos(kx) dx$$

$$B(k) = \int_{-\infty}^{\infty} f(x) \sin(kx) dx$$

$$A(k) = E_0 L \frac{\sin(kL/2)}{kL/2}$$

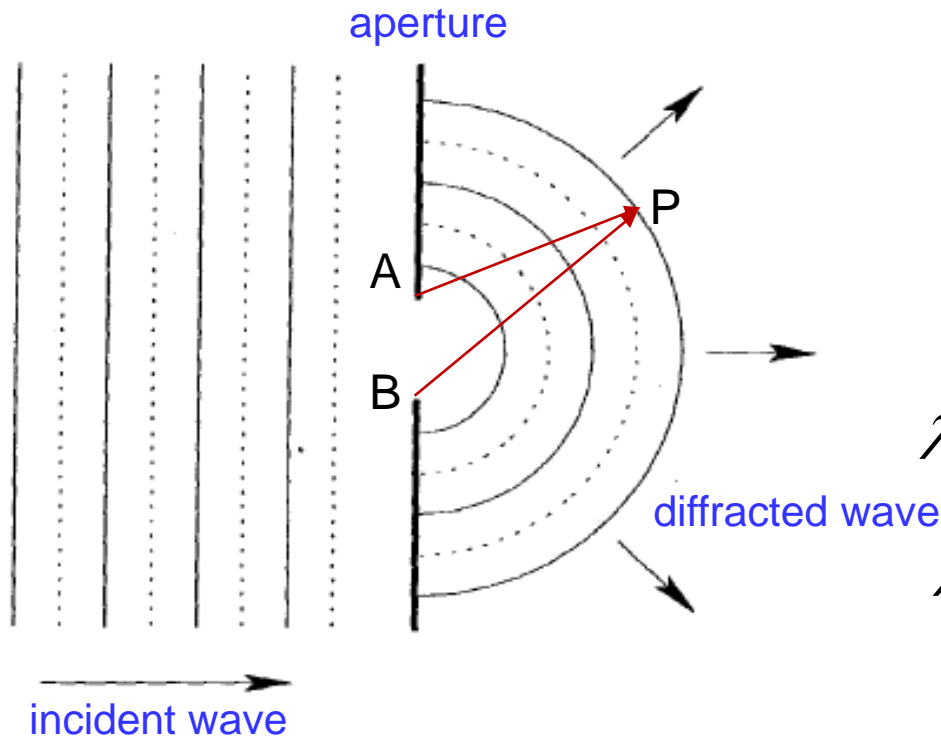
The sinc function.

Inverse relationship between widths  
FT in single-slit Fraunhofer diffraction

Hecht, Pg 312, Fig. 7.34

The square pulse and its transform

# Diffraction



$$\Delta_{\max} = |\overline{AP} - \overline{BP}| \leq AB$$

Manifestation of the wave nature of light – light “bends” around corners.

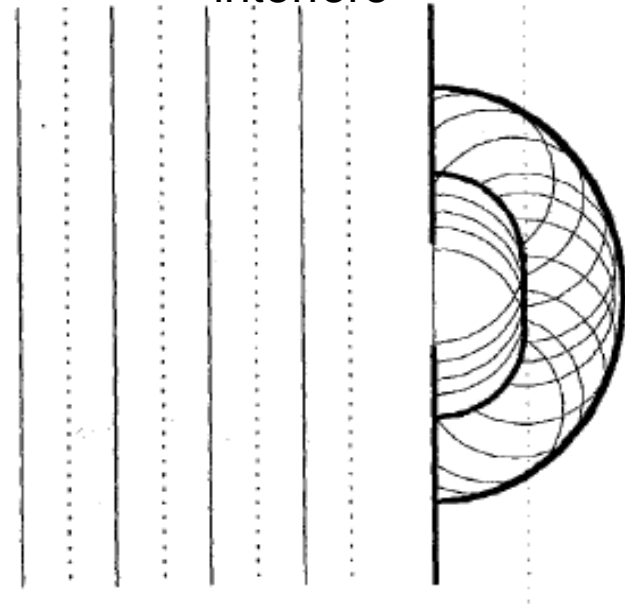
When  $\lambda \sim$  **smallest dim**

$\lambda > AB$  Wave spreads in large angle

$\lambda < AB$  Multitude of wavelets emitted from the aperture interfere

## Huygens-Fresnel Principle:

Every unobstructed point of a wavefront acts as a source of spherical secondary wavelets. The field at any point is the superposition of all of the secondary wavelets.



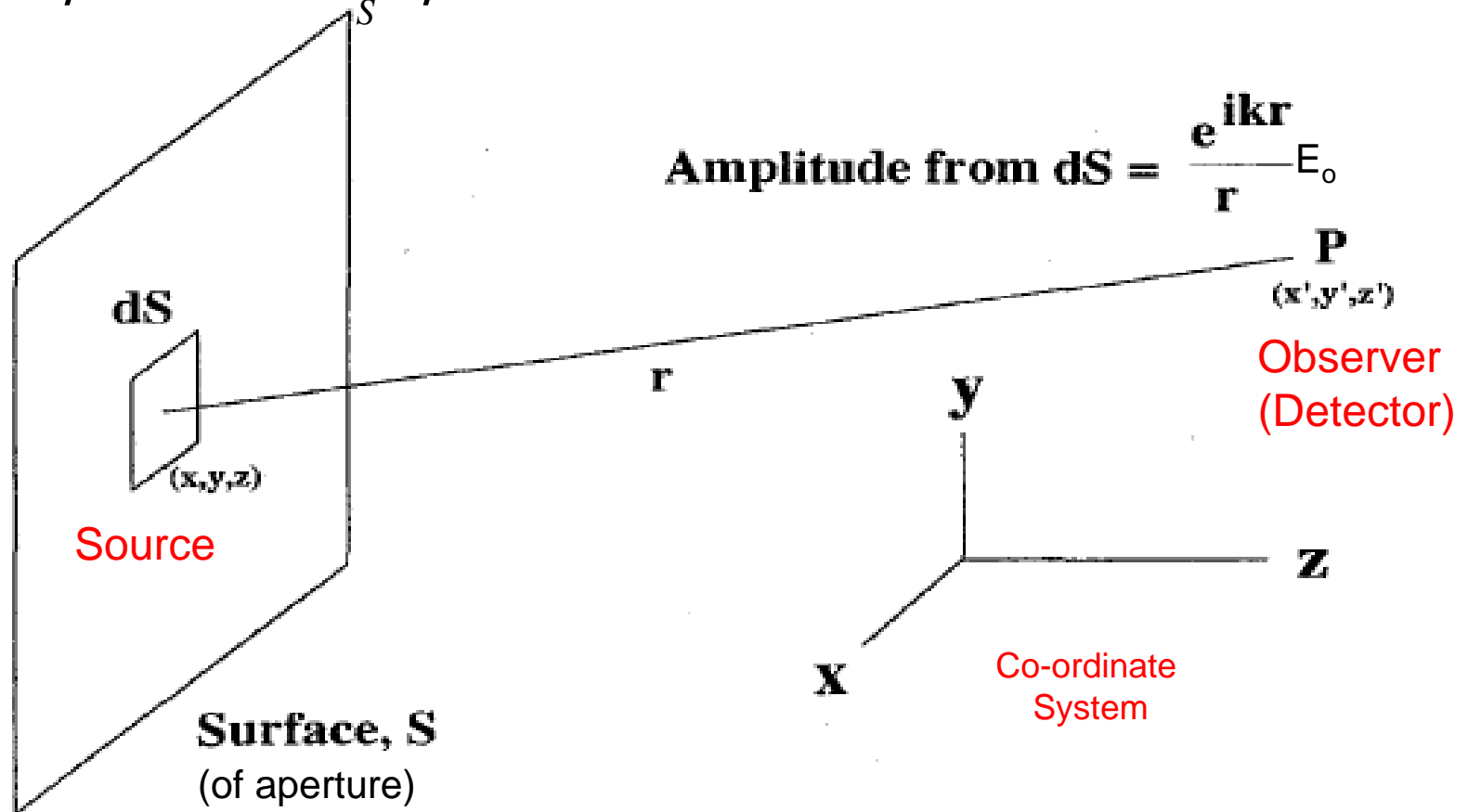
# Analytical Approach

$$E_{spher} \propto E_0 \frac{e^{ikr}}{r}$$

Individual Huygens wavelet generated from surface S

$$E = E_0 \sum_s \frac{e^{ikr}}{r} \Delta S \rightarrow E_0 \int_s \frac{e^{ikr}}{r} dS$$

Superposition of Huygens wavelets at r.  
Time dependence is same for all (same frequency)



# Analytical Approach - II

## Coordinate System:

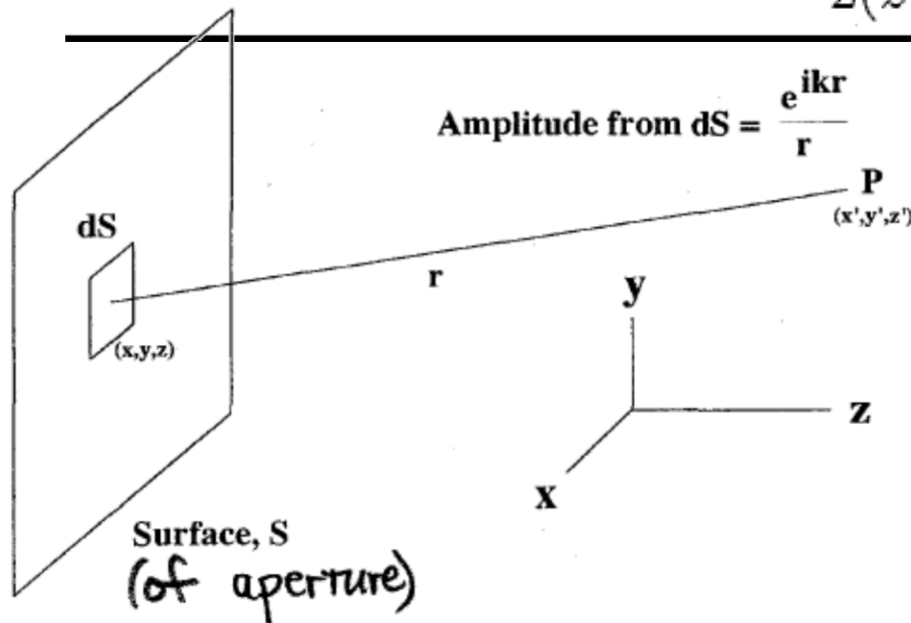
Source Point (on surface):  $x, y, z$

Observation Point (at  $P$ ):  $x', y', z'$

$$r = \sqrt{(x' - x)^2 + (y' - y)^2 + (z' - z)^2}$$

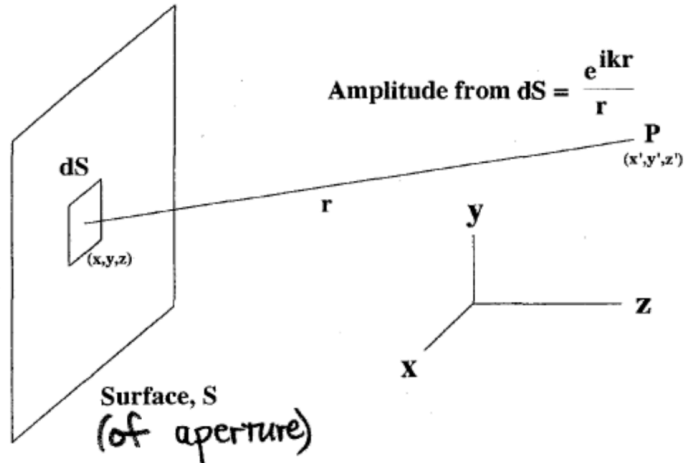
Assume that  $z' - z \gg x' - x, y' - y$ , and expand the square root:

$$\begin{aligned} r &\approx (z' - z) \left\{ 1 + \frac{1}{2} \frac{(x' - x)^2 + (y' - y)^2}{(z' - z)^2} \right\} \\ &= (z' - z) + \frac{x'^2 + y'^2}{2(z' - z)} - \frac{(x'x + y'y)}{(z' - z)} + \frac{x^2 + y^2}{2(z' - z)} \end{aligned}$$



$$z - z' = d$$

The distance between source plane and detector plane.



Fraunhofer Diffraction: Far field diffraction

$$E \propto \int_S e^{ik \left\{ (z' - z) + \frac{x'^2 + y'^2}{2(z' - z)} - \frac{x'x + y'y}{(z' - z)} + \frac{x^2 + y^2}{2(z' - z)} \right\}} dS$$

$$E \propto \int_S e^{ik \left\{ \frac{x'x + y'y}{d} + \frac{x^2 + y^2}{2d} \right\}} dS$$

Can ignore quadratic terms if

We assume the incoming wave is homogeneous

$$k \left( \frac{x^2 + y^2}{2d} \right) \ll 1$$

**Criterion for Fraunhofer  
Diffraction**

$$d \gg \frac{w^2}{\lambda}$$

$w$  is largest dim  
of aperture

# 1-D Fraunhofer Diffraction – Single Slit

Aperture

Screen

Incident Wave

$z=0$

$z=d$

$y$

$+w/2$

$-w/2$

$y'$

$0$

$\theta$

$E \propto \int_{-w/2}^{+w/2} e^{\frac{iky'y}{d}} dy \quad (k = \frac{2\pi}{\lambda})$

Huygens' Recipe  
Fraunhofer limit

$I \propto |E|^2 \propto \left| \frac{2d}{iky'} \sin \frac{kwy'}{2d} \right|^2 = w^2 \left[ \frac{\sin \frac{kwy'}{2d}}{\frac{kwy'}{2d}} \right]^2$

SINC sq. function

In general, related to  
Fourier Transform  
of aperture function

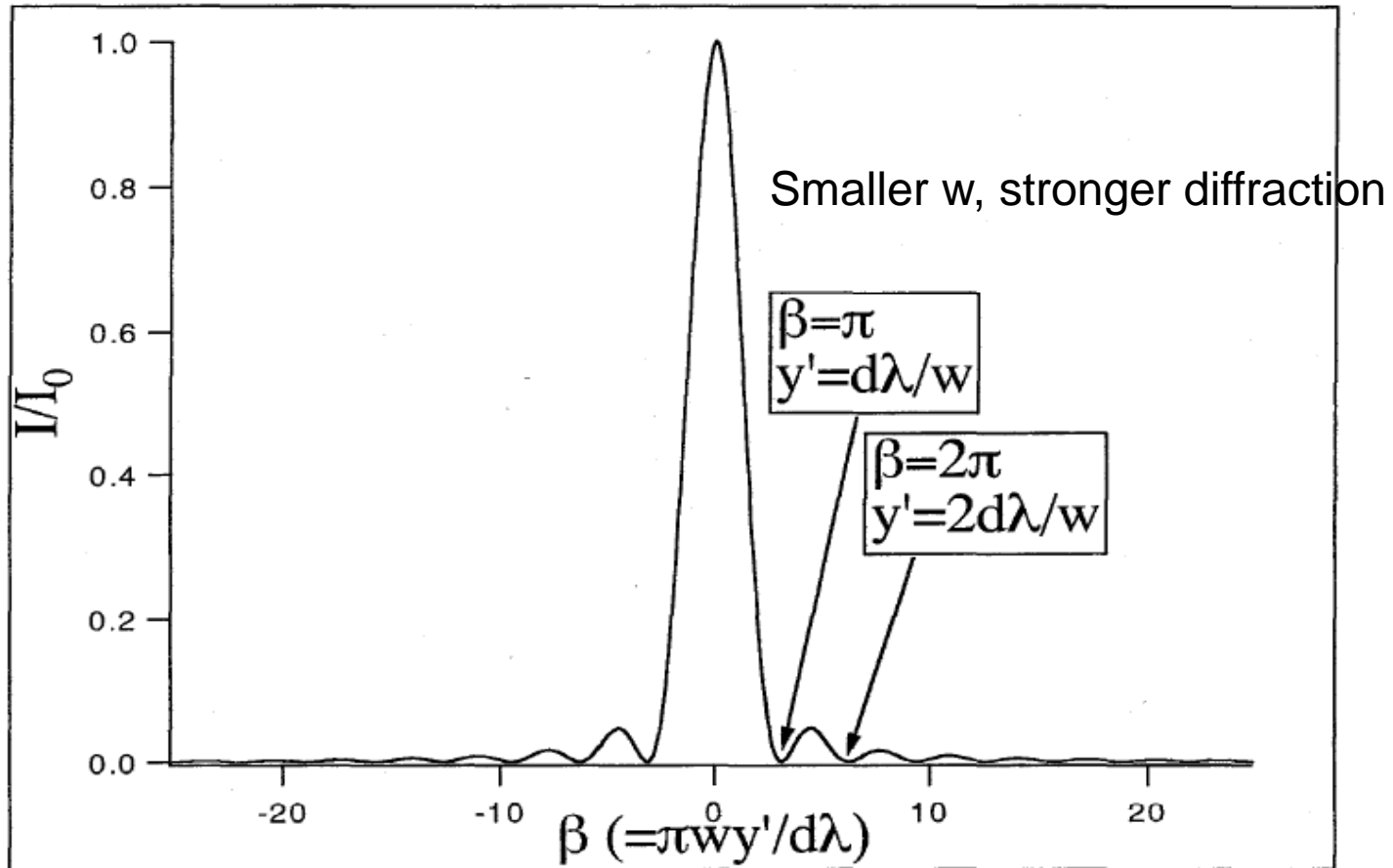
$$I(y') = I_0 \left( \frac{\sin \beta}{\beta} \right)^2, \quad \beta \equiv \frac{kwy'}{2d}$$

$$E \propto \left[ \frac{d}{iky'} e^{\frac{iky'y}{d}} \right]_{y=-w/2}^{y=+w/2} = \frac{d}{iky'} \left[ e^{\frac{ikwy'}{2d}} - e^{\frac{-ikwy'}{2d}} \right] = \frac{2d}{iky'} \sin \frac{kwy'}{2d}$$



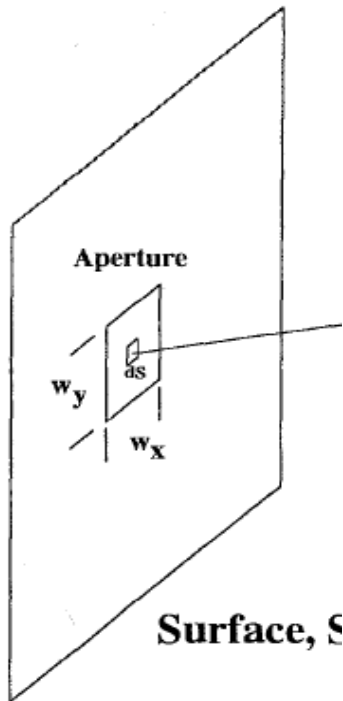
# Single Slit Diffraction Pattern

$$I(y') = I_0 \left( \frac{\sin \beta}{\beta} \right)^2, \quad \beta \equiv \frac{kwy'}{2d}$$



Can determine width  $w$   
from minima location

# Fraunhofer Diffraction – Rectangular Aperture



$$E = \frac{E_o}{d} \iint e^{\frac{-ik(xx'+yy')}{d}} ds$$

Slit widths =  $w_x$  (along x),  $w_y$  (along y)

From Huygens-Fresnel Principle:

$$E \propto \int_S \frac{e^{ikr}}{r} dS \approx \int_S e^{ik \frac{x'x+y'y}{d}} dS = \int_{-w_y/2}^{+w_y/2} \int_{-w_x/2}^{+w_x/2} e^{ik \frac{x'x+y'y}{d}} dx dy$$

For Rectangular Aperture x and y directions are Independent :

$$E \propto \left( \int_{-w_y/2}^{+w_y/2} e^{\frac{iky'y}{d}} dy \right) \left( \int_{-w_x/2}^{+w_x/2} e^{\frac{ikx'x}{d}} dx \right)$$

These are familiar integrals from **1-dimensional case**:

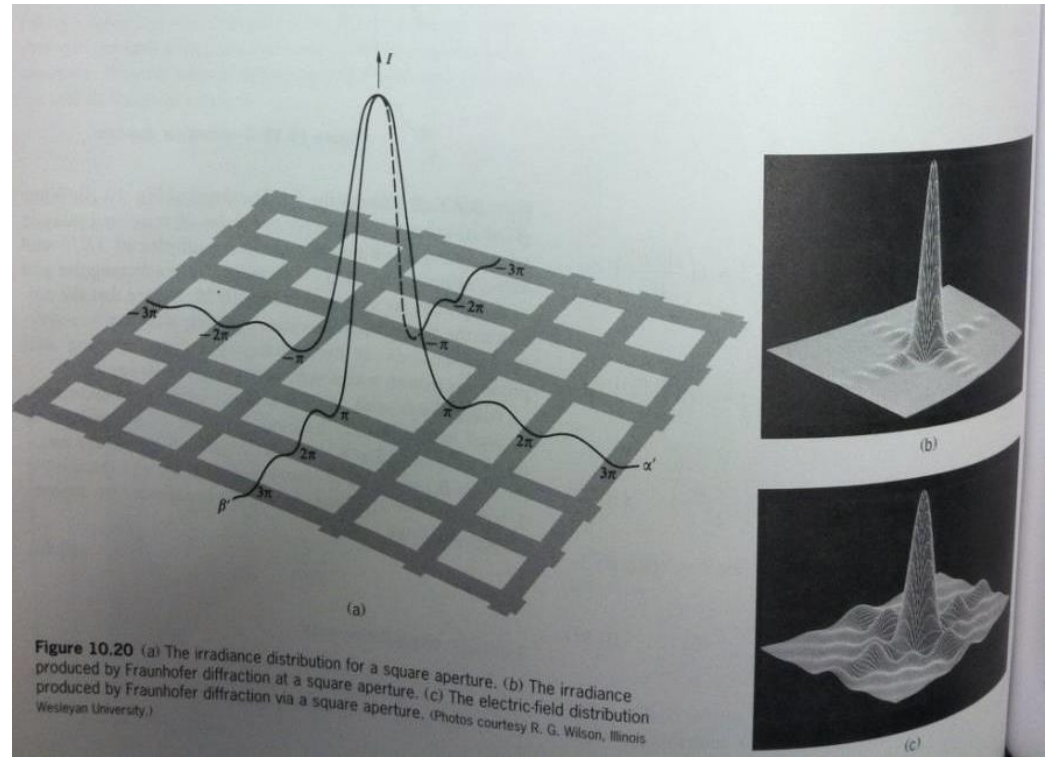
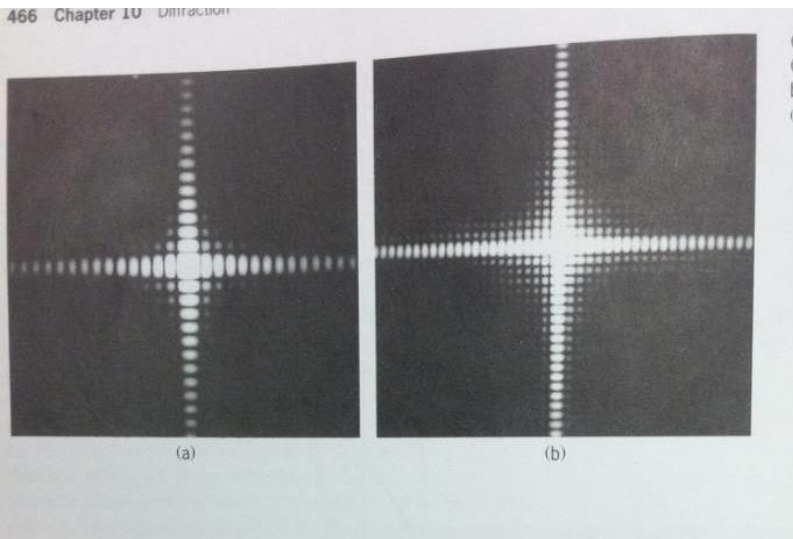
$$E \propto \left( \frac{\sin \beta_x}{\beta_x} \right) \left( \frac{\sin \beta_y}{\beta_y} \right), \quad \beta_x \equiv \frac{kw_x x'}{2d}, \quad \beta_y \equiv \frac{kw_y y'}{2d}$$

Intensity  $I \propto |E|^2$

$$I = I_0 \left( \frac{\sin \beta_x}{\beta_x} \right)^2 \left( \frac{\sin \beta_y}{\beta_y} \right)^2$$

# Fraunhofer Diffraction – Rectangular Aperture

$$I = I_0 \left( \frac{\sin \beta_x}{\beta_x} \right)^2 \left( \frac{\sin \beta_y}{\beta_y} \right)^2$$



$$\frac{I_m}{I(0)} = \frac{1}{\beta_i^2}, \beta_i = (n + 1/2)\pi$$

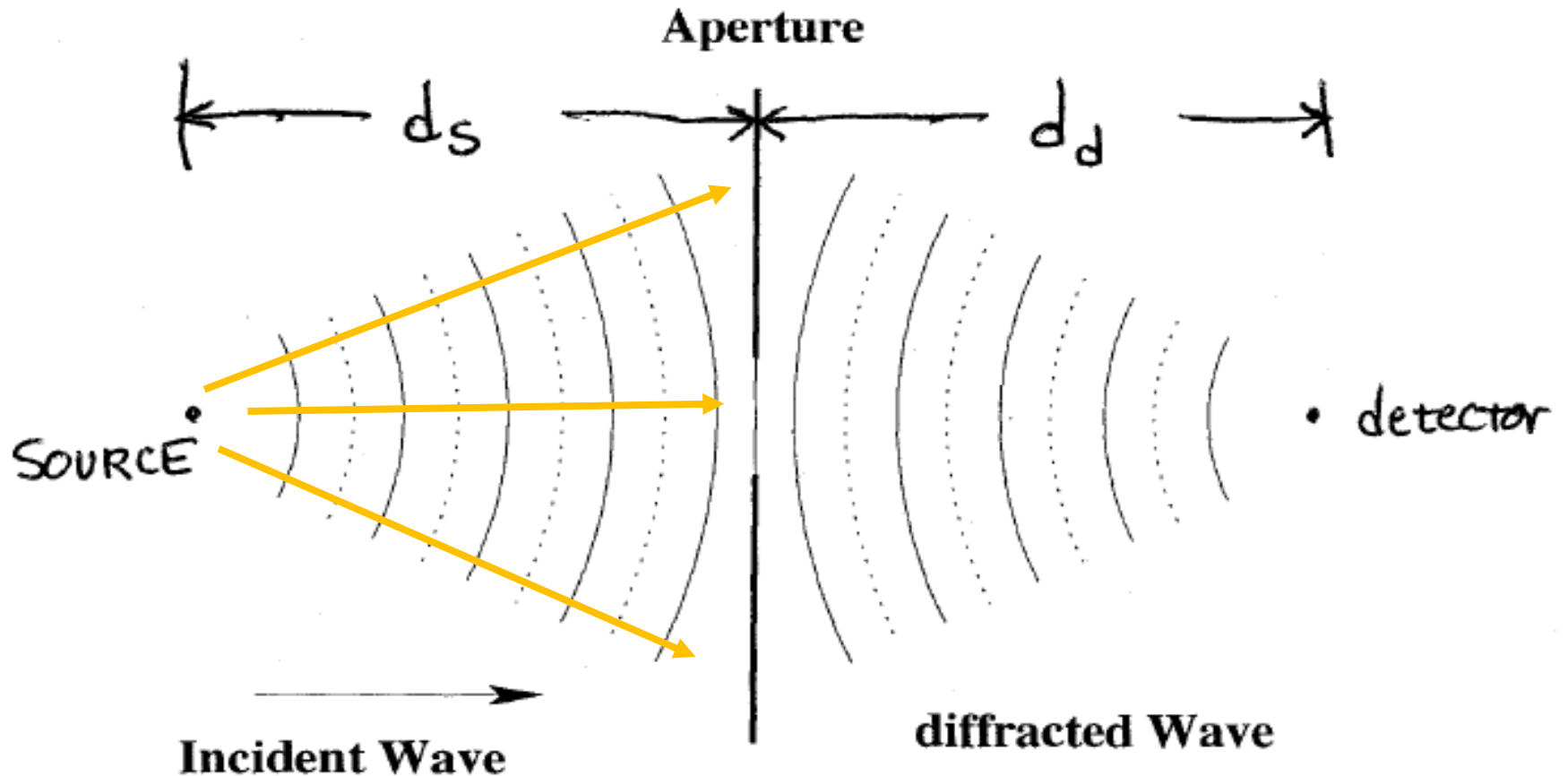
$$\beta_x \equiv \frac{k w_x x'}{2d}, \beta_y \equiv \frac{k w_y y'}{2d}$$

# Fresnel Diffraction

Occurs when  $w^2/d\lambda \gg 1$

Near Field Effect  $\Leftrightarrow$

Wavefront curvature  
is important.



# Fresnel Diffraction

All Waves are Spherical and Aperture is Rectangular:  $(x_1, x_2)$  by  $(y_1, y_2)$

Source Wave:  $E \propto \frac{e^{ikr_s}}{r_s}$ , where  $r_s$  = distance from source to wavefront.

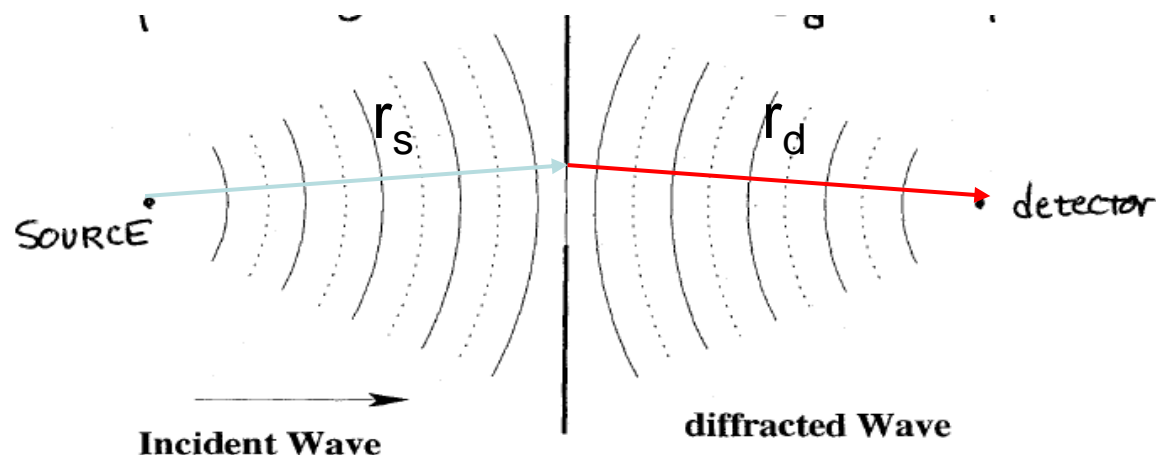
Diffracted Wave:  $E \propto \frac{e^{ikr_d}}{r_d}$ , where  $r_d$  = distance from observer to wavefront.

Using Huygen's Principle surface element  $dS$  produces contribution  $dE$  seen by observer:

$$dE \propto \frac{1}{r_s r_d} e^{ik(r_s + r_d)} dS$$

Total field at observing point:

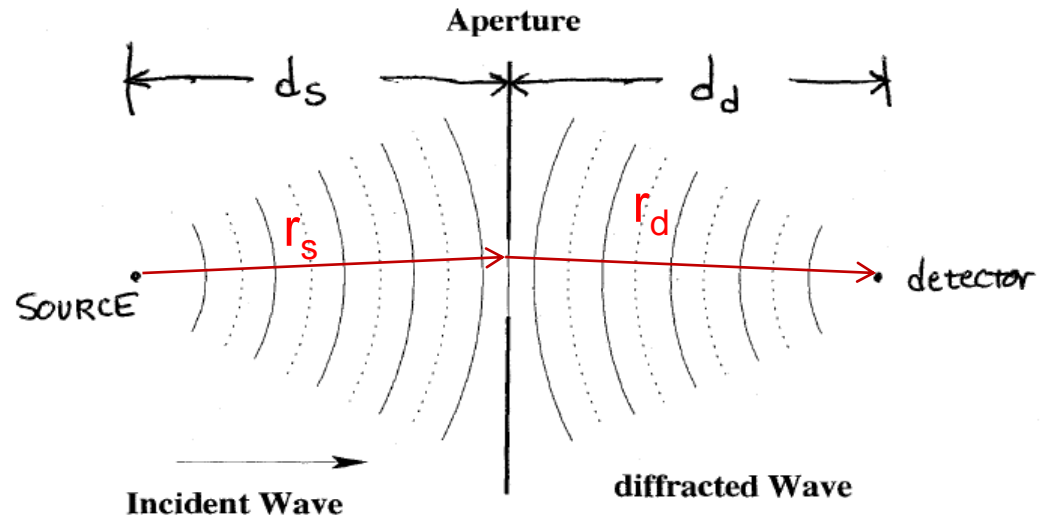
$$E \propto \frac{1}{r_s r_d} \int_S e^{ik(r_s + r_d)} dS$$



# Fresnel Diffraction

Occurs when  $w^2/d\lambda \gg 1$   
 Near Field Effect  $\Leftrightarrow$   
 Wavefront curvature  
 is important.

(keep quadratic terms)



If  $d_s$  = distance of source to **aperture plane** and  $d_d$  is distance from observer to **aperture plane**:

$$ik(r_s + r_d) \approx ik \left( d_s + d_d + (x^2 + y^2) \frac{d_s + d_d}{2d_s d_d} \right) = ik(d_s + d_d) + i\pi u^2/2 + i\pi v^2/2$$

where  $x$  and  $y$  are in aperture plane (as in Fraunhofer case) and:

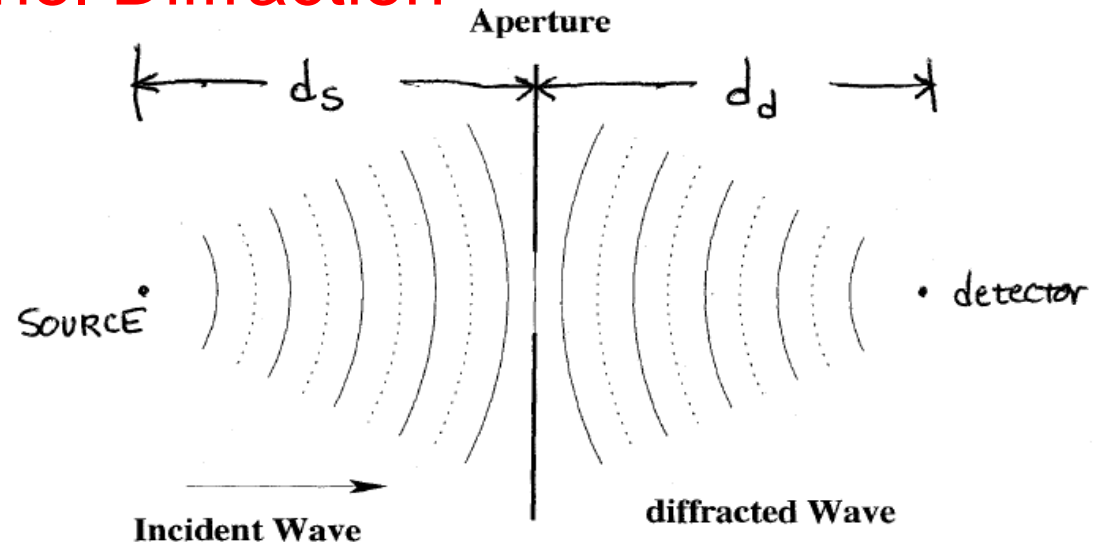
$$u \equiv x \left[ \frac{2(d_s + d_d)}{\lambda d_s d_d} \right]^{1/2} \text{ and } v \equiv y \left[ \frac{2(d_s + d_d)}{\lambda d_s d_d} \right]^{1/2}$$

$$\boxed{\frac{1}{d} = \frac{1}{d_s} + \frac{1}{d_d}} \\ \boxed{u = x \left[ \frac{2}{\lambda d} \right]^{1/2}}$$

$$E \propto \frac{1}{r_s r_d} \int_S e^{ik(r_s + r_d)} dS \approx \frac{1}{d_s d_d} \int_{x_1}^{x_2} \int_{y_1}^{y_2} e^{ik(r_s + r_d)} dx dy \propto \int_{u_1}^{u_2} e^{i\pi u^2/2} du \int_{v_1}^{v_2} e^{i\pi v^2/2} dv$$

# Fresnel Diffraction

Occurs when  $w^2/d\lambda \gg 1$   
 Near Field Effect  $\Leftrightarrow$   
 Wavefront curvature  
 is important.



**Intensity (2 dimensions)**

$$I \propto \left| \int_{u_1}^{u_2} e^{i\pi u^2/2} du \right|^2 \left| \int_{v_1}^{v_2} e^{i\pi v^2/2} dv \right|^2$$

$$u \equiv x \left[ \frac{2(d_s + d_d)}{\lambda d_s d_d} \right]^{1/2} \text{ and } v \equiv y \left[ \frac{2(d_s + d_d)}{\lambda d_s d_d} \right]^{1/2}$$

Either source or  
 Detector in near field

**One Dimension:**

$$I \propto \left| \int_{u_1}^{u_2} e^{i\pi u^2/2} du \right|^2, \quad u \equiv x \left[ \frac{2(d_s + d_d)}{\lambda d_s d_d} \right]^{1/2}$$

$$\frac{1}{d} = \frac{1}{d_s} + \frac{1}{d_d}$$

$$u = x \left[ \frac{2}{\lambda d} \right]^{1/2}$$

**NOTE:** This expression is for an observation point at  $x' = 0$ : the origin of the observer's coordinate system.

# Fresnel Integrals

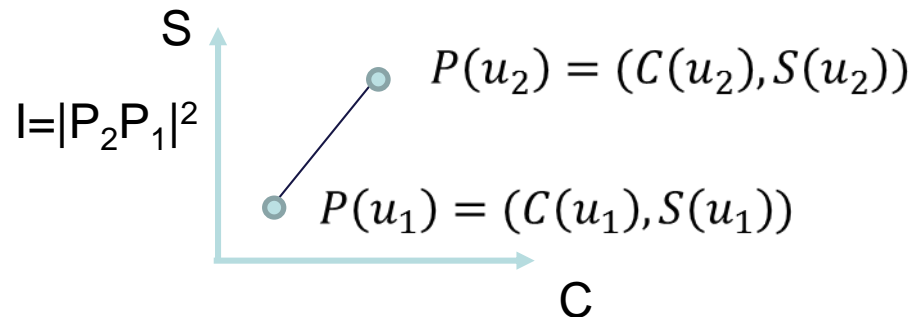
$$\text{FRESNEL COSINE INTEGRAL} \equiv C(u) = \int_0^u \cos(\pi u'^2/2) du'$$

$$\text{FRESNEL SINE INTEGRAL} \equiv S(u) = \int_0^u \sin(\pi u'^2/2) du'$$

$$\begin{aligned} \text{Thus, } \int_0^u e^{i\pi u'^2/2} du' &= \int_0^u \cos(\pi u'^2/2) du' + i \int_0^u \sin(\pi u'^2/2) du' \\ &= C(u) + iS(u) \end{aligned}$$

$$\begin{aligned} I &\propto \left| \int_{u_1}^{u_2} e^{i\pi u^2/2} du \right|^2 = \left| \int_{u_1}^0 e^{i\pi u^2/2} du + \int_0^{u_2} e^{i\pi u^2/2} du \right|^2 \\ &= \left| -\int_0^{u_1} e^{i\pi u^2/2} du + \int_0^{u_2} e^{i\pi u^2/2} du \right|^2 \\ &= |C(u_2) - C(u_1) + i(S(u_2) - S(u_1))|^2 \\ &= [C(u_2) - C(u_1)]^2 + [S(u_2) - S(u_1)]^2 \end{aligned}$$

$$\text{Thus, } I \propto [C(u_2) - C(u_1)]^2 + [S(u_2) - S(u_1)]^2$$





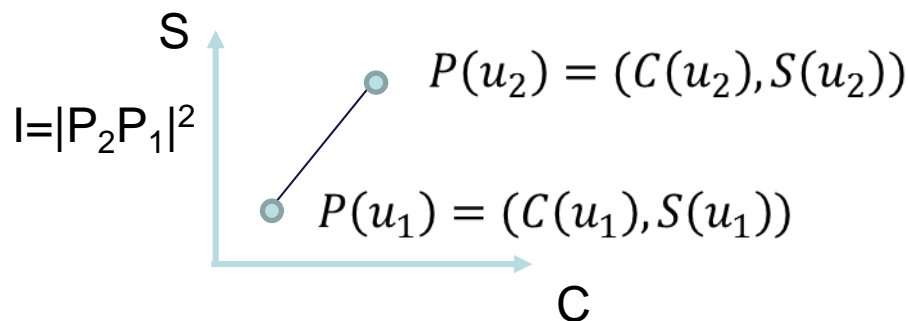
# The Cornu Spiral

**CORNU SPIRAL:** graphic representation of  $C(u) + iS(u)$  **Properties of Cornu Spiral:**

1. **Length along curve is proportional to slit width:** Once width is fixed,  
the length of the  
curve is fixed

$$(dl)^2 = (dC(u))^2 + (dS(u))^2 = \cos^2(\pi u^2/2)(dw)^2 + \sin^2(\pi u^2/2)(dw)^2 = (dw)^2$$

2. **Intensity** is proportional to square of length of chord between end-points of slit.
3. **Move Observation Point** by moving **end points** of chord in opposite direction.

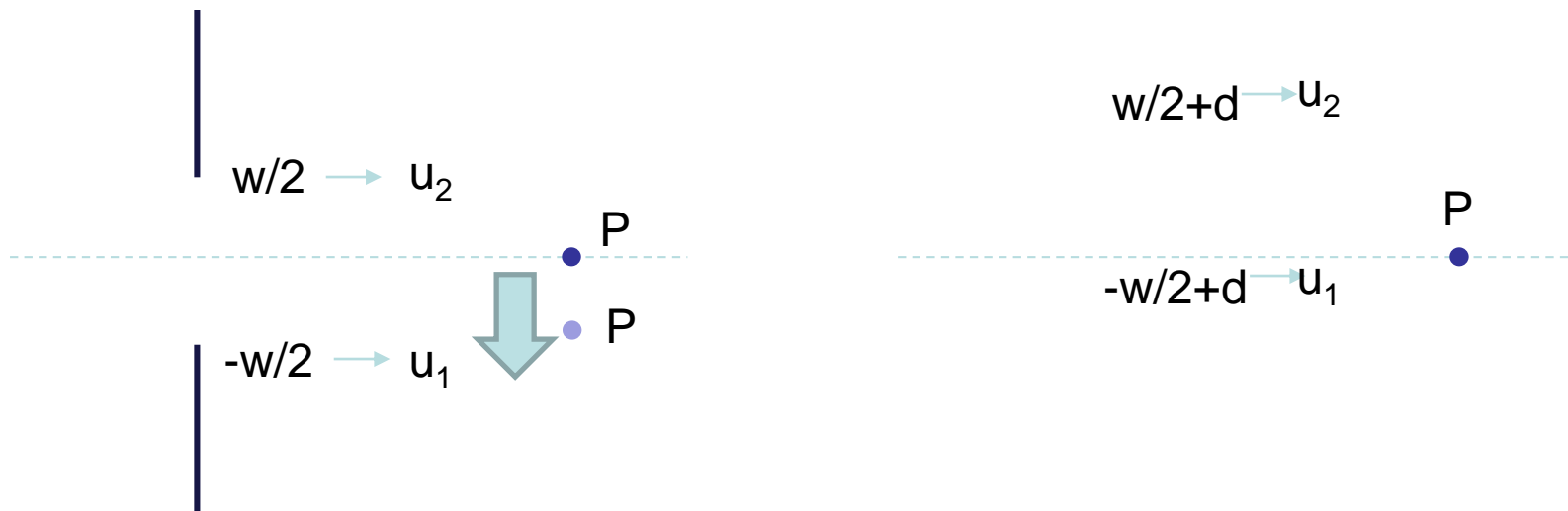


# Fresnel Diffraction

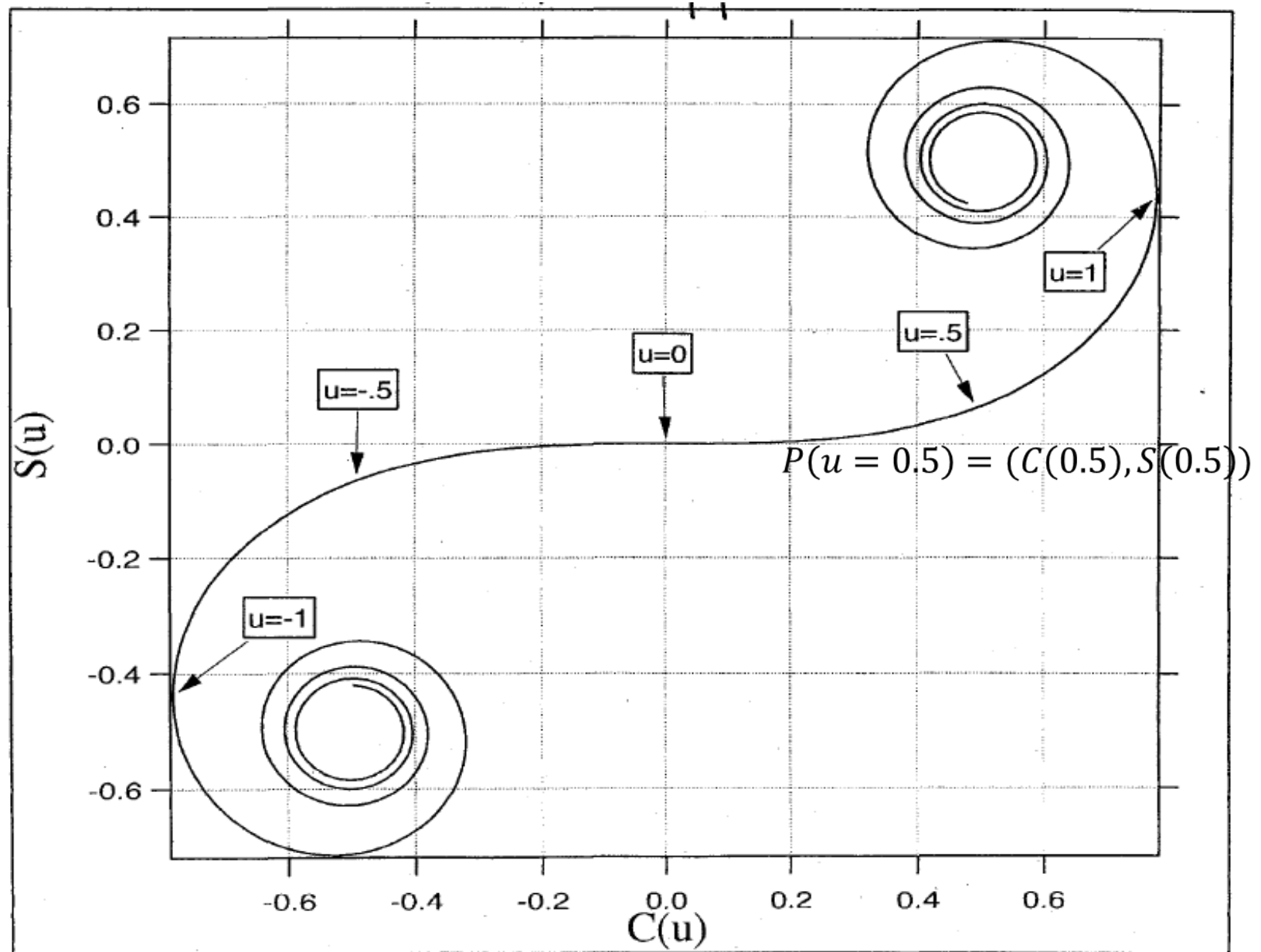
3. Move Observation Point by moving end points of chord in opposite direction.

**Thus,**  $I \propto [C(u_2) - C(u_1)]^2 + [S(u_2) - S(u_1)]^2$

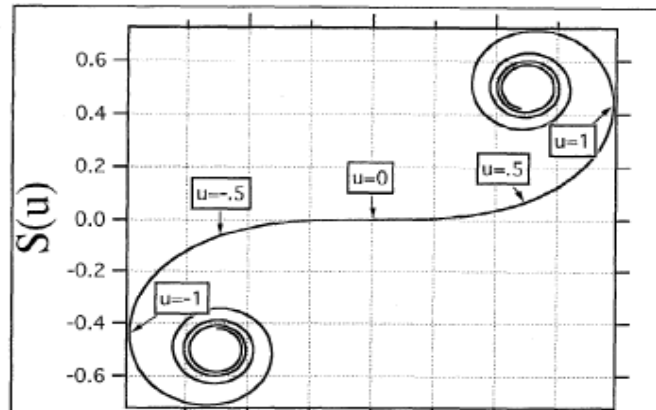
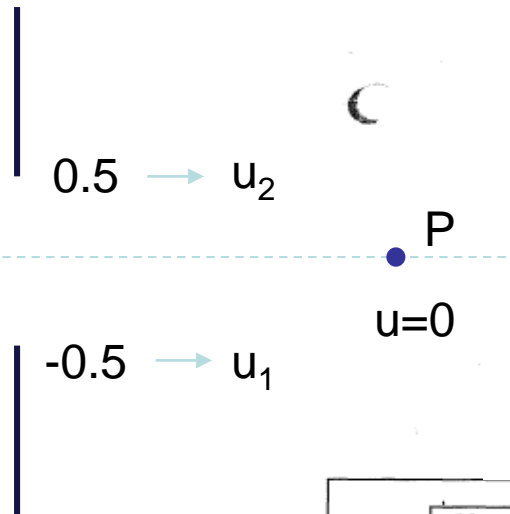
All the equations are derived for  $X' = 0$ .



# The Cornu Spiral



# 1. Length along curve is proportional to slit width:

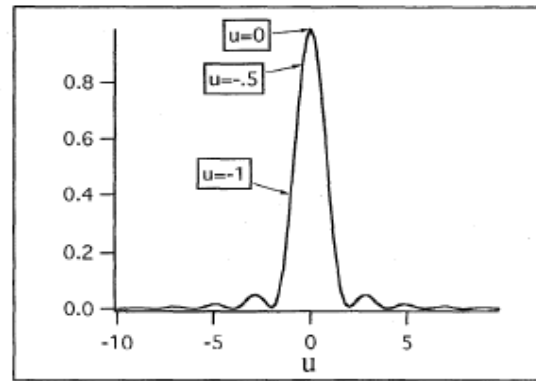
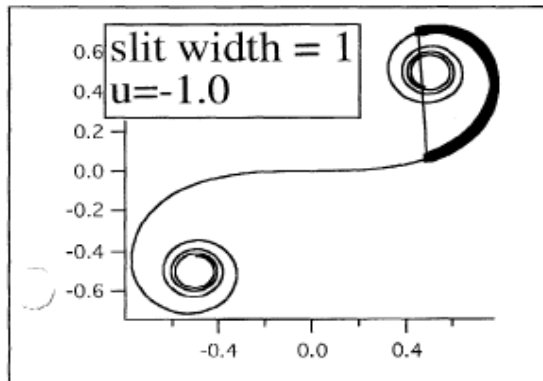
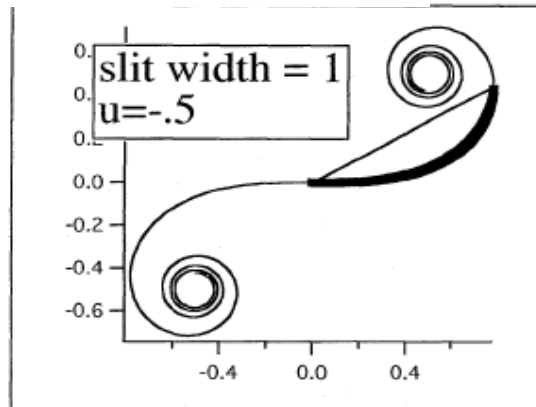
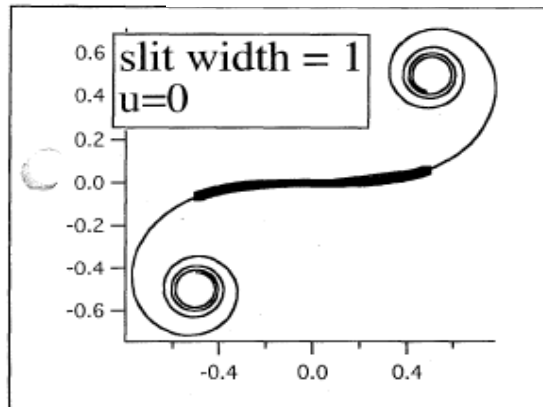


Normalized slit width  
 $= w \left( \frac{2}{d\lambda} \right)^{1/2}$

where  
 $\frac{1}{d} = \frac{1}{d_s} + \frac{1}{d_d}$   
source distance      detector distance

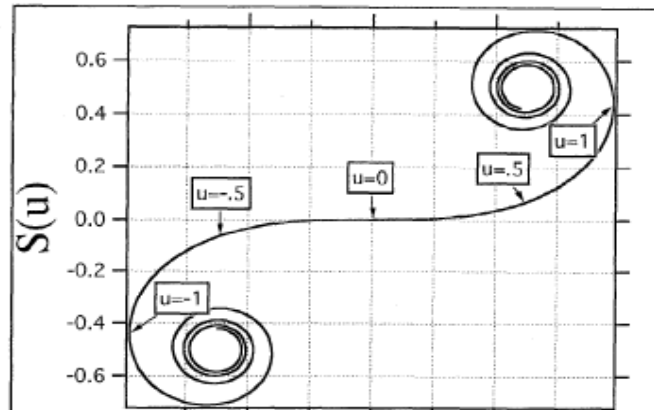
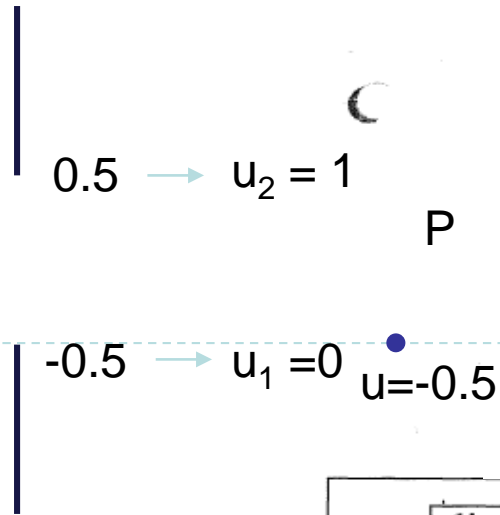
$$\frac{1}{d} = \frac{1}{d_s} + \frac{1}{d_d}$$

$$u = x \left[ \frac{2}{\lambda d} \right]^{1/2}$$



Fraunhofer  
 Diffraction  
 on Cornu  
 Spiral

# 1. Length along curve is proportional to slit width:

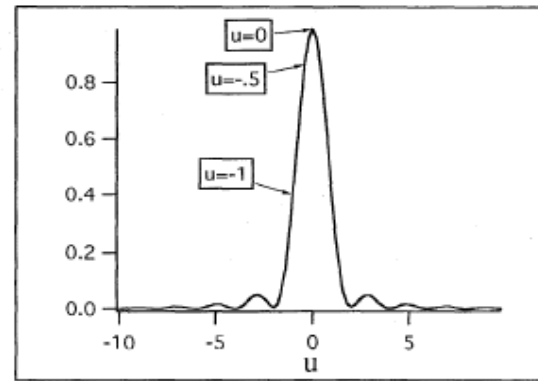
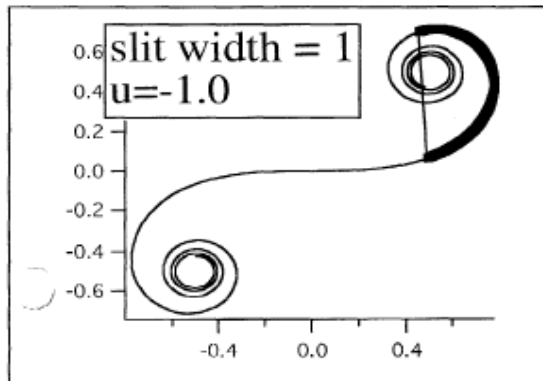
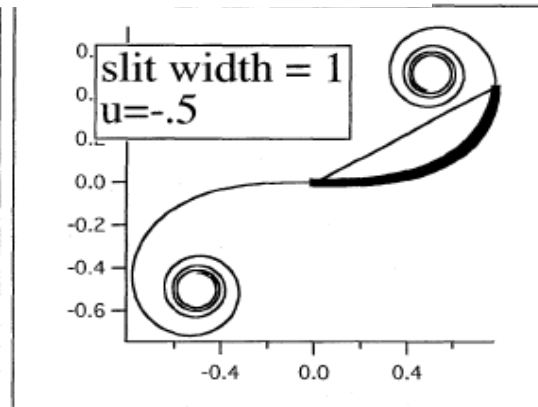
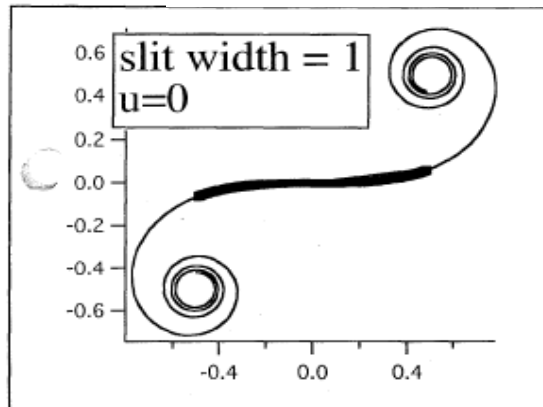


Normalized  
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source distance      detector distance

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Fraunhofer  
Diffraction  
on Cornu  
Spiral

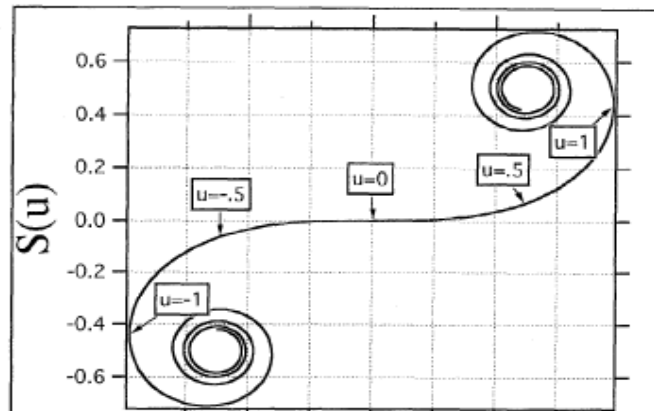
# 1. Length along curve is proportional to slit width:

$$0.5 \rightarrow u_2 = 1.5$$

P

$$-0.5 \rightarrow u_1 = 0.5$$

u=-1

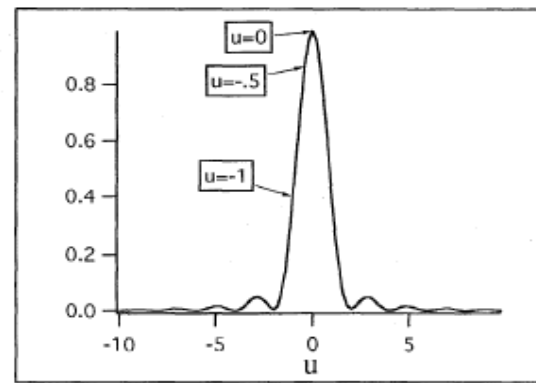
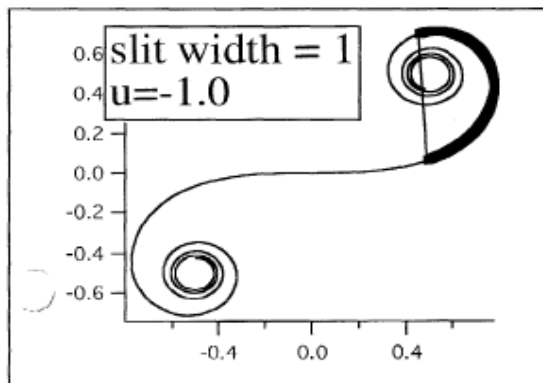
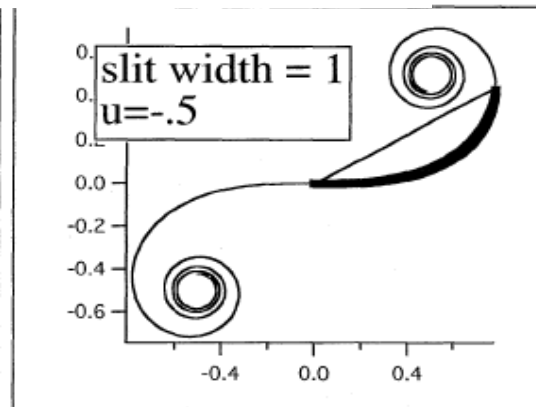
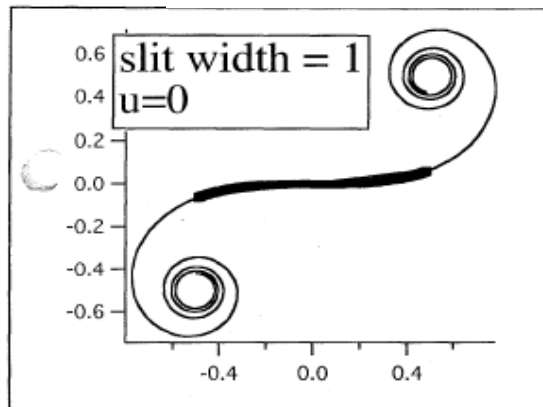


Normalized  
slit width  
 $= w \left( \frac{2}{d\lambda} \right)^{1/2}$

where  
 $\frac{1}{d} = \frac{1}{d_s} + \frac{1}{d_d}$   
source      detector

$$\frac{1}{d} = \frac{1}{d_s} + \frac{1}{d_d}$$

$$u = x \left[ \frac{2}{\lambda d} \right]^{1/2}$$



Fraunhofer  
Diffraction  
on Cornu  
Spiral

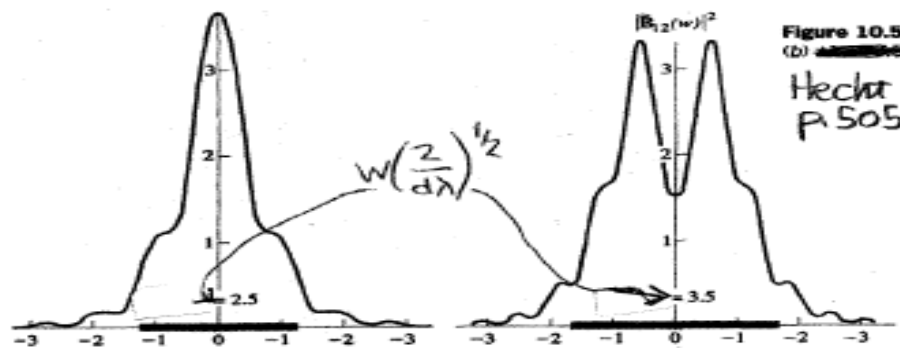


Figure 10.5  
(b) Hecht p.505

horizontal axis

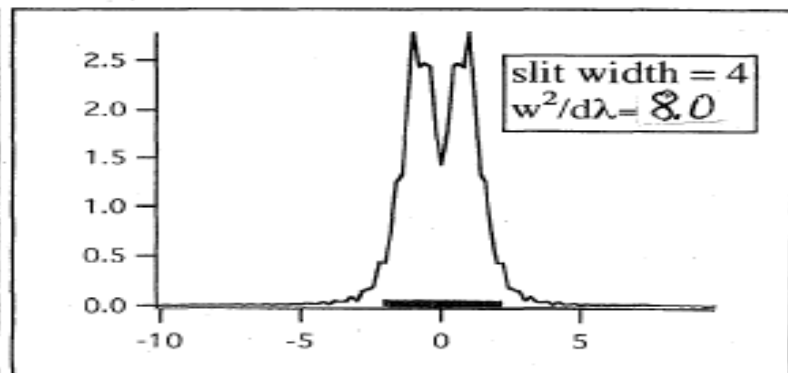
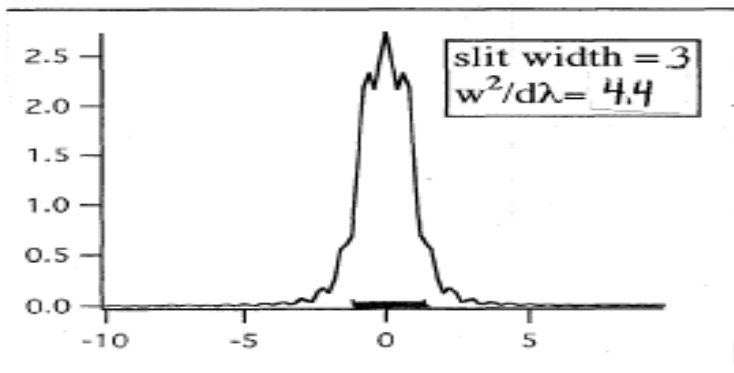
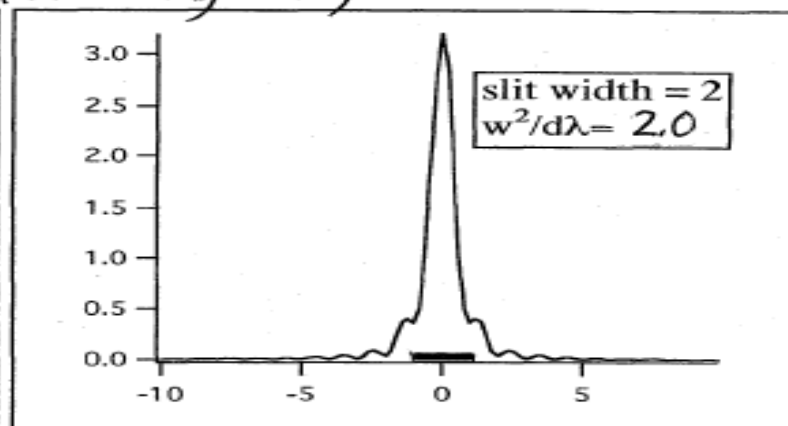
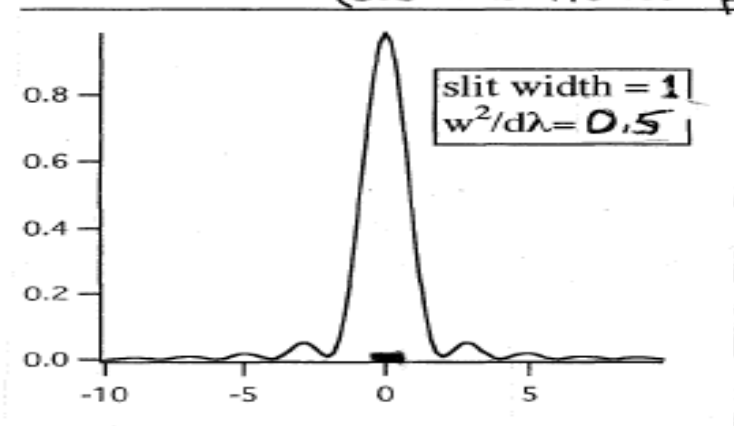
$$u = x \left( \frac{2}{d\lambda} \right)^{1/2}$$

normalized slit width =  $w \left( \frac{2}{d\lambda} \right)^{1/2}$

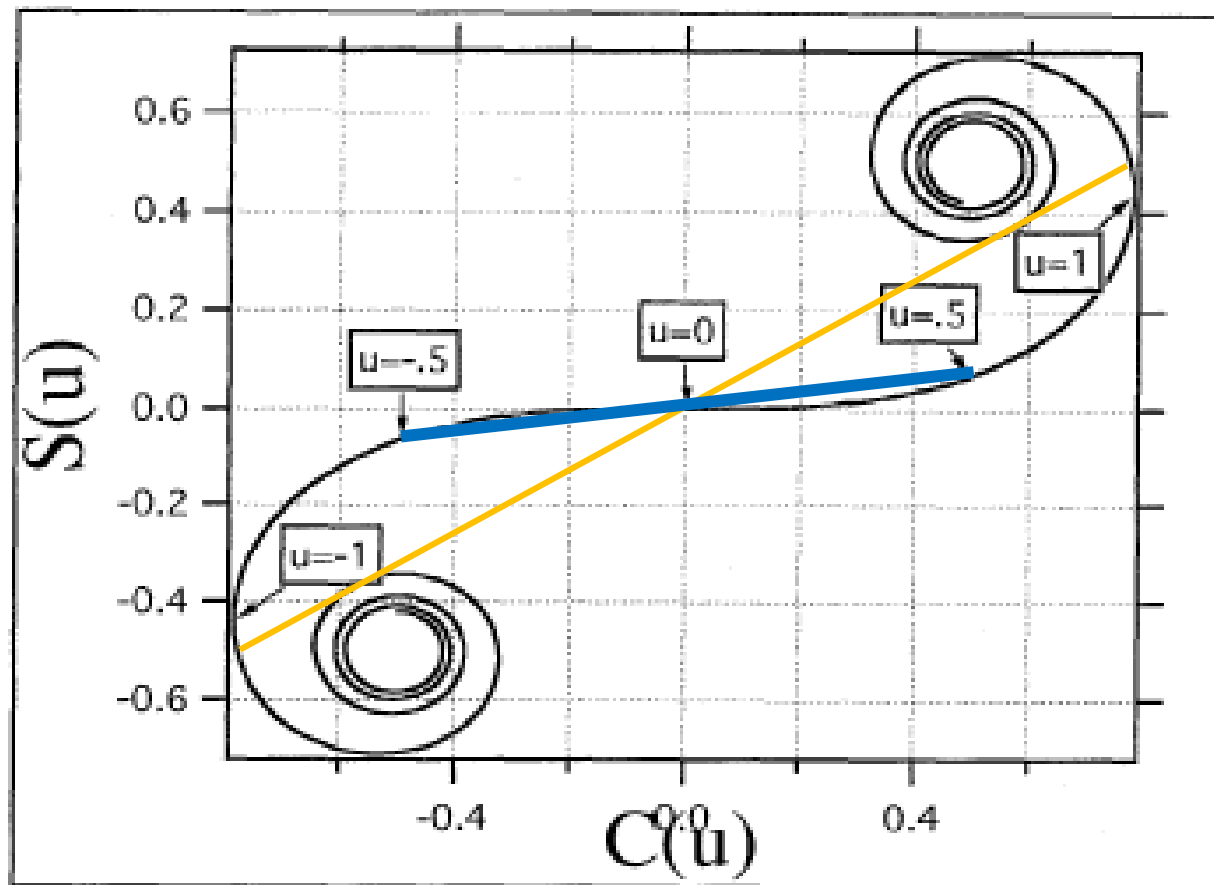
where  $\frac{1}{d} = \frac{1}{d_s} + \frac{1}{d_d}$   
 source  $\rightarrow$  detector

Below, we show the progression from  $w=1$  (Fraunhofer) to  $w=4$  (Fresnel). (horizontal bar is geometric shadow of slit)

(see also Hecht p.447 Fig 10.2)



p.10



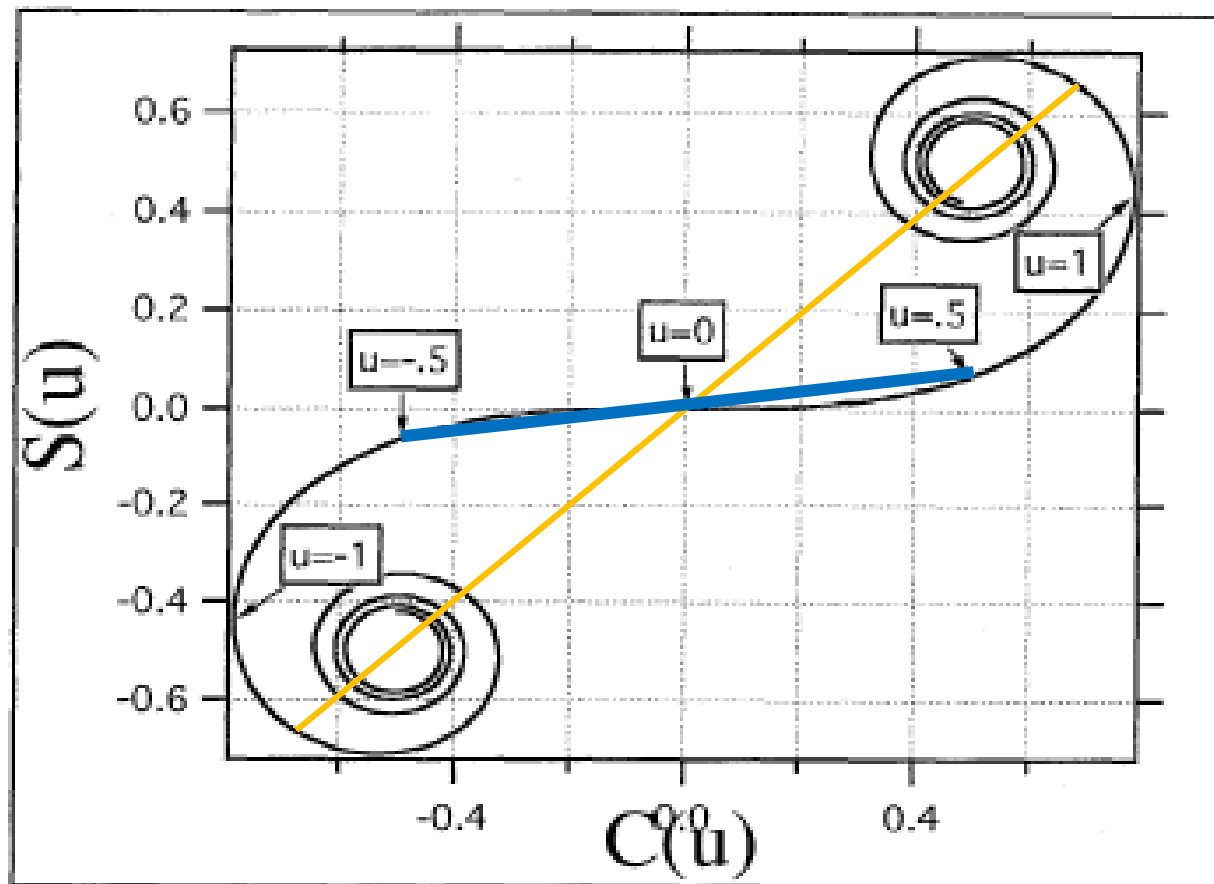
Normalized  
slit width  
 $= w \left( \frac{2}{d\lambda} \right)^{\frac{1}{2}}$

where  
 $\frac{1}{d} = \frac{1}{d_s} + \frac{1}{d_d}$   
source detector

Detector is at the  $u=0$ .

Start with slit width =1. We continuously increase the slit width.



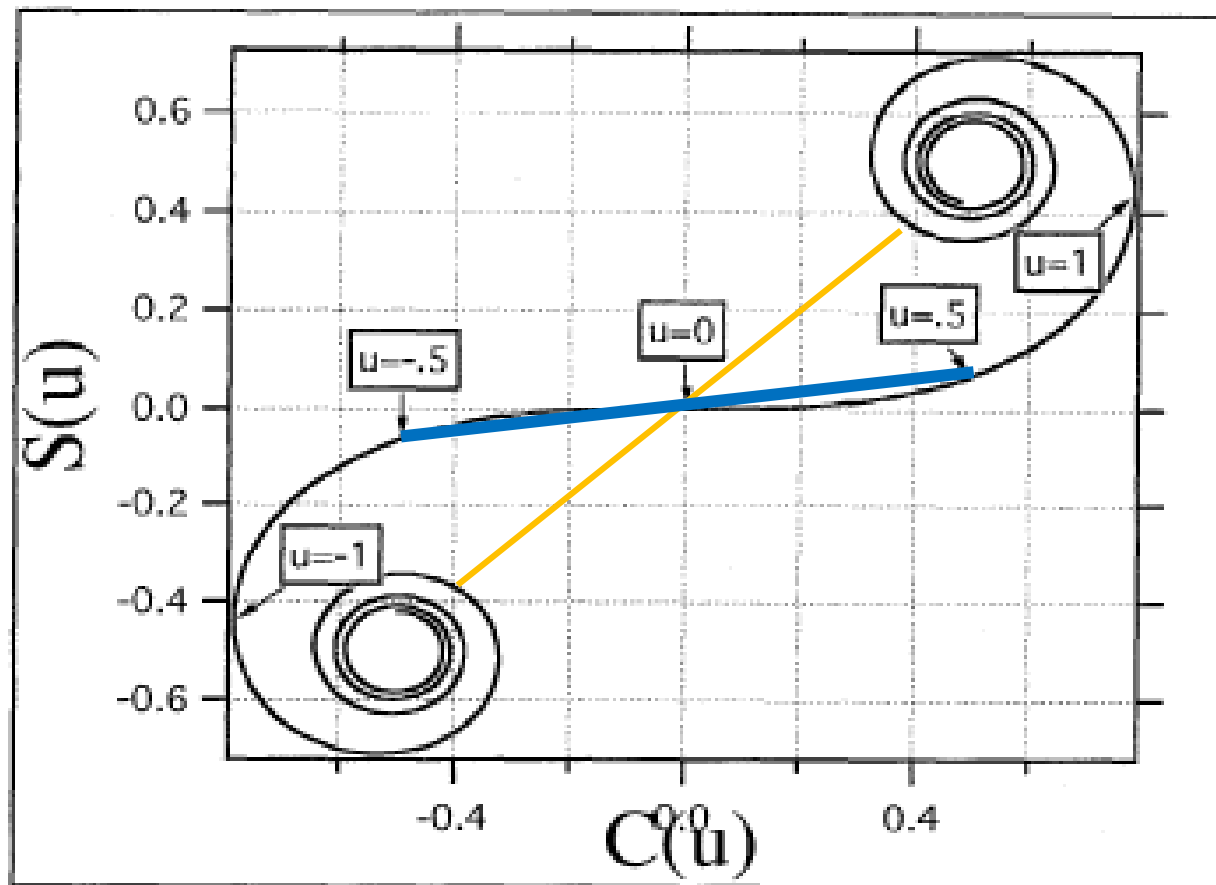


Normalized  
slit width  
 $= w \left( \frac{2}{d\lambda} \right)^{\frac{1}{2}}$

where  
 $\frac{1}{d} = \frac{1}{d_s} + \frac{1}{d_d}$   
source detector

Detector is at the  $u=0$ .

Start with slit width =1. We continuously increase the slit width.



p.10

Normalized  
slit width  
 $= w \left( \frac{2}{d\lambda} \right)^{\frac{1}{2}}$

where  
 $\frac{1}{d} = \frac{1}{d_s} + \frac{1}{d_d}$   
source detector

Detector is at the  $u=0$ .

Start with normalized slit width =1. We continuously increase the slit width.