



Entry losses, ducts and hoods



I' ll never design an LEV system. Why do I need to know this?

- Almost nobody know about it either!
- So you' ll need to explain these concepts
- Developing control recommendations and conceptual designs
- Assessing ventilation effectiveness
- Enhancing LEV performance & troubleshooting
- Easy CIH exam points!



Types of losses

- Friction Losses:
 - Fluid in motion encounters drag along the surface
 - Energy is needed to overcome the drag force
 - The drag force is due to the fluid viscosity
- Dynamic losses
 - Turbulence and eddies in the flow
 - Momentum losses due to change in direction
 - Found in expansions, contractions, elbows, junctions and hood entries



Duct friction losses

- Friction losses increase linearly with duct length increasing air density, typical form:

$$H_f = F_f P_{V_1} \frac{L}{100'}$$

- Losses depend on the duct material and wall roughness
- Losses increase with V^2 (and also Q^2)
- Losses decrease \sim with square of duct area
– (proportional to $1/A^{2.5}$ but approx $1/A^2$)



Principles of LEV Design

- To protect the worker's breathing zone:
 - the contaminant is captured close to the point of release (local) and removed (exhausted) from work areas
- prevents contaminant migration to other areas
- systems are always mechanical
- volume flow rate is much less than general or dilution ventilation



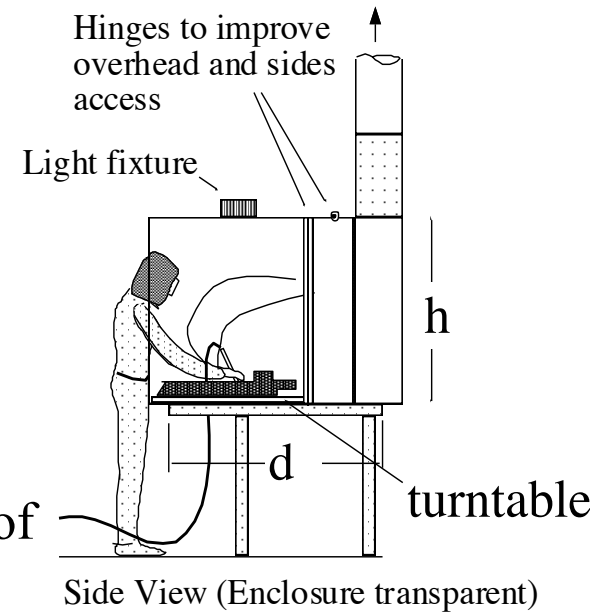
Local Exhaust Hoods

- Purpose
 - Capture and remove contaminant at the source
- Effectiveness determined by
 - Hood configuration & shape
 - The extent to which the hood encloses the contaminant source
 - Cardinal rule: *enclose source to the extent possible*
 - Amount of air flow into hood (i.e. Q_{hood})



Hood Types

- Enclosing Hood
 - contaminant source contained within hood
 - examples:
 - lab fume hood
 - glove box, paint booth
 - good for:
 - contaminants with high toxicity
 - areas where there is a high cross draft potential
 - Airflow requirements determined by the product of velocity x area of enclosure
 - The more complete the enclosure – the less airflow requirement needed
 - Less susceptible to outside air currents

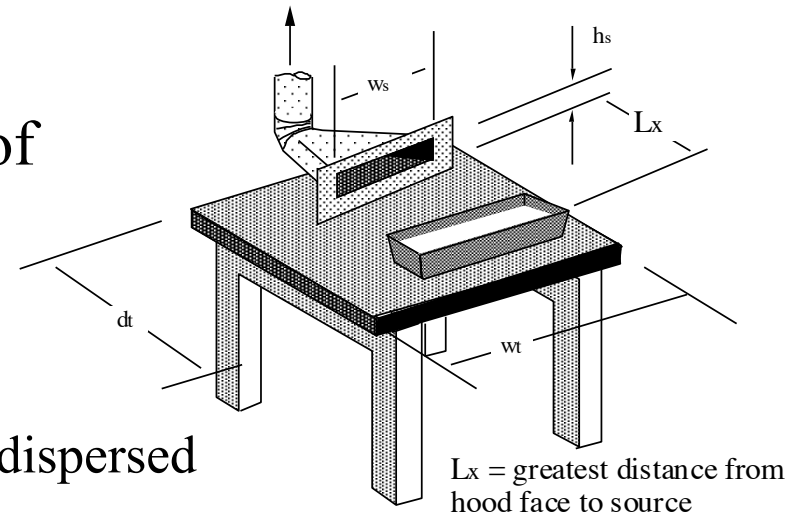




Hood Types

• Capture Hood

- creates exhaust airflow in front of opening to capture & remove contaminant
- capture velocity or V_c
 - a factor of how the contaminant is dispersed
 - room air currents
 - how far the source is from the hood opening
- Disadvantages
 - May require large airflow requirements
 - Subject to crossdrafts
 - The effective “reach” is limited to ~ 1 diameter or less





Basic Hood Types



Enclosing



Capture



Hood Types

- Receiving or Capture Hoods: utilize natural movement of contaminant toward hood opening
 - good for:
 - canopy over hot process (range hood)
 - radial arm saw hood
 - not good for:
 - fine particles
 - high toxicity contaminants
 - cold processes



Hood Selection Factors

- Potential for outside air currents
- nature of the process which generates the contaminant
- Potential for contaminating the breathing zone (canopy hoods)
- Worker compatibility

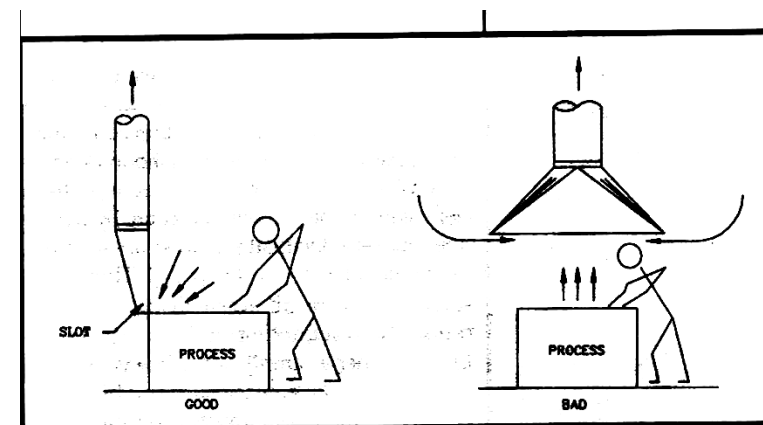
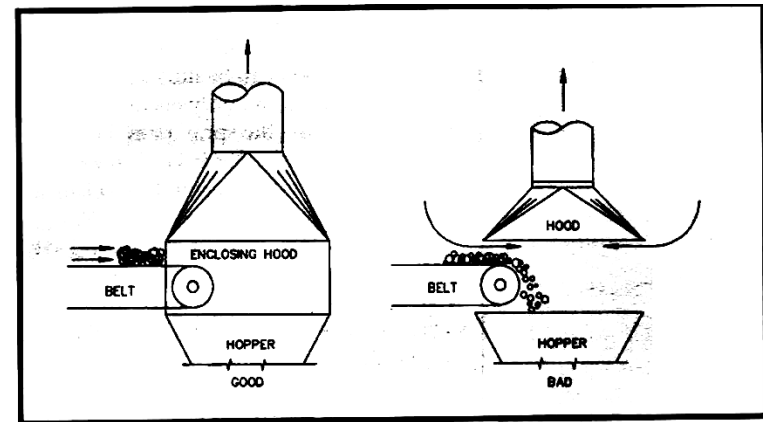


Figure 10.4 – Canopy hood. (From American Conference of Governmental

Source: Dinardi (1998)



Enclosing Hoods

- Control velocity = V_f = face velocity
 - What velocity across hood face is necessary for proper contaminant control?
 - Nature of the process and contaminants generated
 - Hood shape and size
 - Magnitude of cross drafts
 - Higher is not always better
- Getting an even distribution of airflow at the face
 - Making the booth deeper
 - Using a baffle
 - Use of filters/air cleaning devices



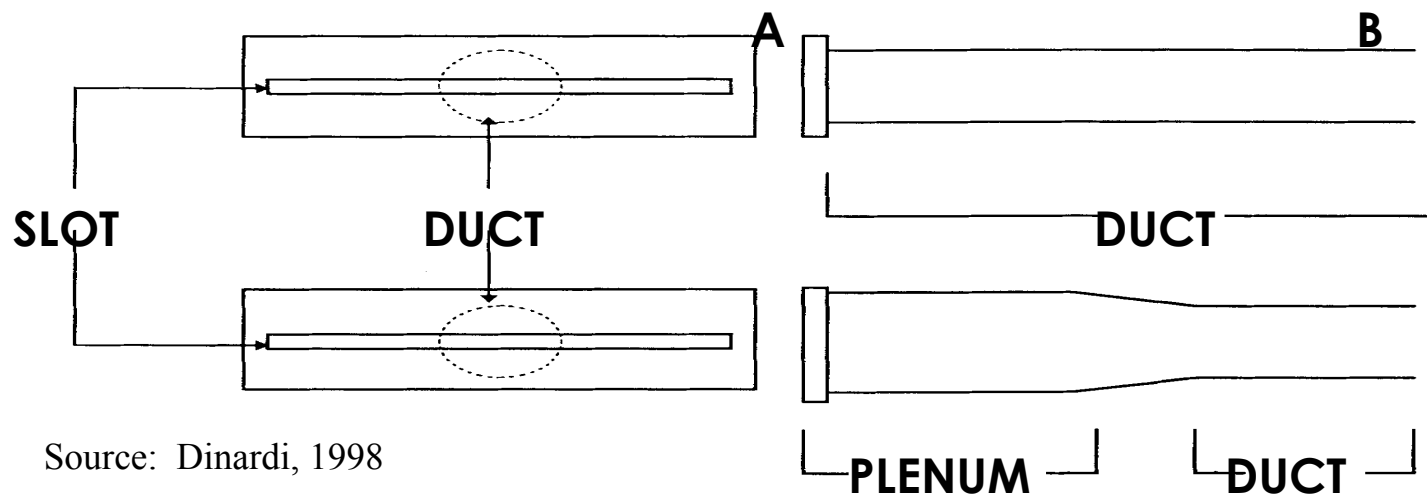
Enclosing hood: Lab fume hood

- Recommended face velocity: 60 – 100 ft/min depending on
 - Room air currents
 - Location of equipment in hood relative to face
- Face velocity: > 150 ft. min
 - Air turbulence at hood face
 - Reverse airflow
 - Contaminants may exit at hood face



Slots, plenums & baffles

- Slot hoods with plenums
 - Useful for processes where contaminant is released across a large surface area
 - Degreasing tanks
 - Plating tanks
 - Welding tables
 - Distributes airflow more evenly across the surface
- Slot hood
 - A hood with a width-to-length ratio of 0.2 or less
 - Purpose – to provide uniform distribution of airflow
- Plenum
 - A large chamber or compartment that distributes airflow



Source: Dinardi, 1998



Hood Design

- Design parameters for hoods

Hood geometry/shape

Hood size

Q = volumetric flow rate (CFM)

$$Q = VA$$

V = air velocity in fpm

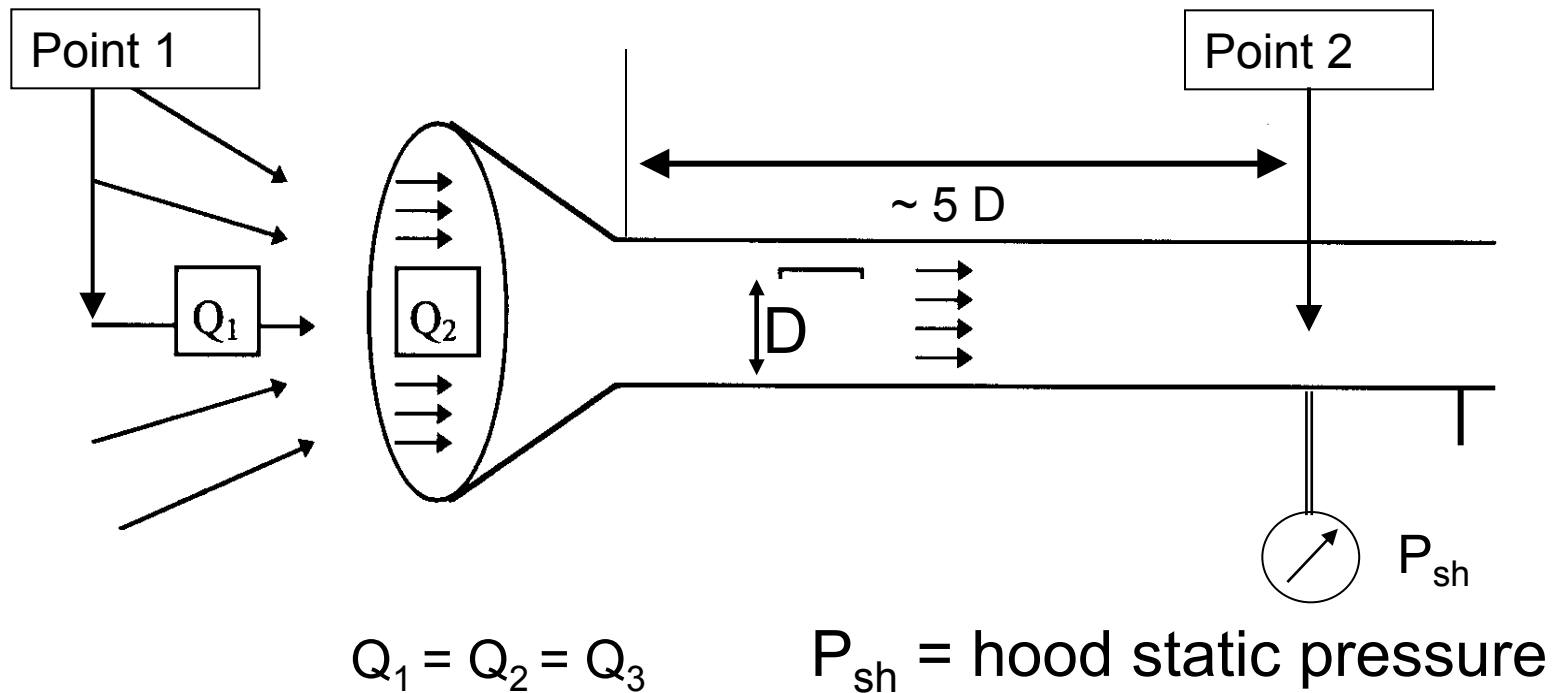
A = area of face in square feet

- flow is not measured directly
- determined by measuring face velocity (V) & knowing cross sectional area of flow (A)



Simple Hood

$$P_{T1} = P_{T2} + \text{losses}$$



Note: outside $P_{T1} = 1 \text{ atm}$ and $P_{V1} = 0$, so $P_{T1 \text{ gauge}} = 0$



Hood entry losses, P_{sh}

$$0 = P_{T1}$$

$$0 = P_{T2} + losses$$

$$0 = P_{sh} + P_{V2} + losses$$

$$\boxed{-P_{sh} = P_{V2} + losses}$$

If we apply the sign convention,
 P_{V2} and losses are + terms

- The P_{sh} is the pressure needed to:
 - Set the air into motion (P_v part) aka “acceleration loss”
 - Overcome any losses in the hood
- Note ideally when no losses, $P_{sh} = P_v$; that is all the potential energy is converted into kinetic energy of the moving fluid



Hood static pressure

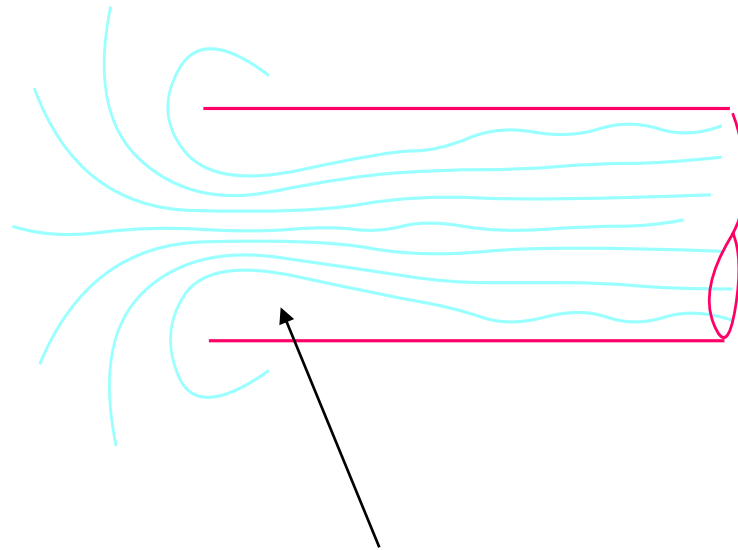
- Other forms: $|P_{sh}| = P_V + losses$
 - The losses are characteristic of the hood shape and are defined as the hood entry loss H_e (e=entry)

$$|P_{sh}| = P_V + H_e$$

- H_e is caused by dynamic losses and turbulence in the inlet. Air can't follow perfectly into the inlet and contracts to a flow stream that is smaller than the actual duct cross section -- known as the Vena Contracta. This creates turbulence and energy loss



Vena contracta



About $d/2$ is max effect



Hood entry losses

- Entry loss is proportional to P_v
- The loss factors have been tabulated for various shapes

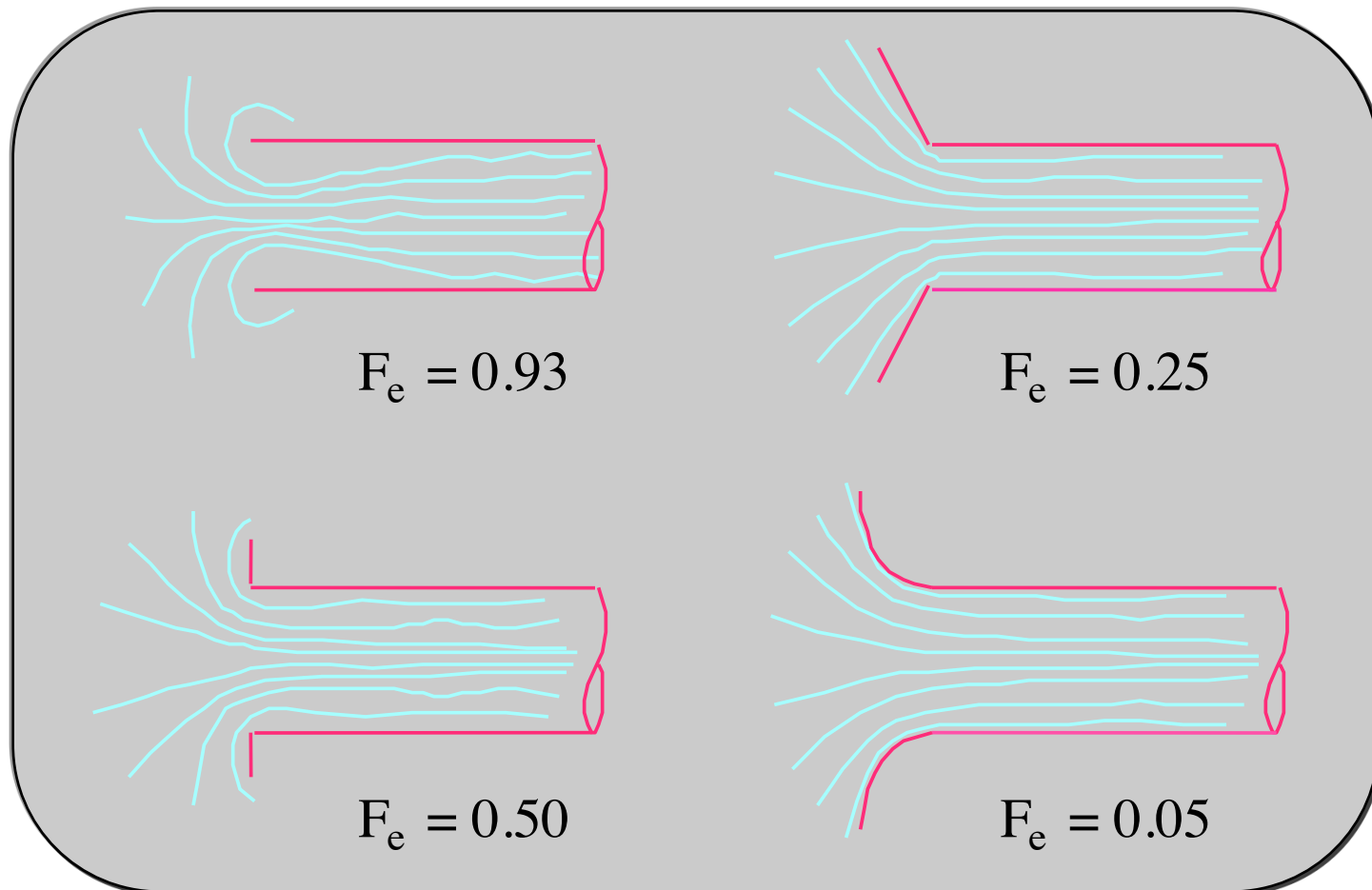
$$|P_{sh}| = P_v + H_e$$

$$H_e = F_e P_v$$

$$P_{sh} = P_v + F_e P_v$$

$$P_{sh} = P_v (1 + F_e)$$

$$\frac{P_{sh}}{P_v} = 1 + F_e$$



Vena contracta and F_e



Hood Efficiency

- Hood efficiency can be evaluated in terms of the energy loss at the entry
- Say we had a perfect hood, then all potential energy would be converted to kinetic energy
- So: $P_{sh} = P_v + 0$ (no losses)
- If we define C_e as the coefficient of entry

$$C_e = \frac{Q_{actual}}{Q_{ideal}}$$

← Actual flow

← Ideal flow with no losses



C_e represents efficiency

- Recall C_e = ratio of actual flow to ideal flow

$$C_e = \frac{Q_{actual}}{Q_{ideal}}$$

- So:
$$C_e = \frac{4005\sqrt{P_v} \cdot (area)}{4005\sqrt{P_{sh}} \cdot (area)} = \sqrt{\frac{P_v}{P_{sh}}}$$

- C_e represents the efficiency of the hood – it is unitless and measures how well the hood converts potential energy (P_s) into kinetic energy (P_v) in the flow



C_e is related to F_e

- Recall F_e gives hood loss in terms of P_v

$$\frac{P_{sh}}{P_v} = 1 + F_e$$

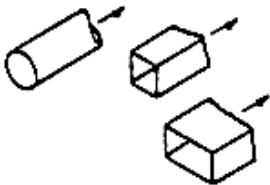
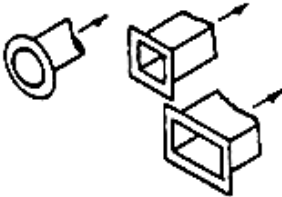
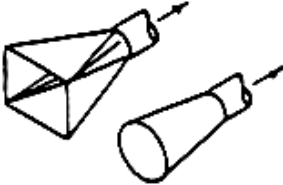
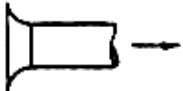
- So if: $C_e = \sqrt{\frac{P_v}{P_{sh}}}$ then $C_e^2 = \frac{1}{[1 + F_e]}$

- So the efficiency of the hood is directly related to the flow rate, and the square of the efficiency is a measure of the entry loss factor



Efficiency for different entries

- C_e depends on the hood geometry
- Unlike H_e it does not depend on Q the flow rate

HOOD TYPE	DESCRIPTION	COEFFICIENT OF ENTRY, C_e	ENTRY LOSS
	PLAIN OPENING	0.72	0.93 VP
	FLANGED OPENING	0.82	0.49 VP
	TAPER or CONE HOOD	Varies with angle of taper or cone. See Fig. 6-10	
	BELL MOUTH INLET	0.98	0.04 VP



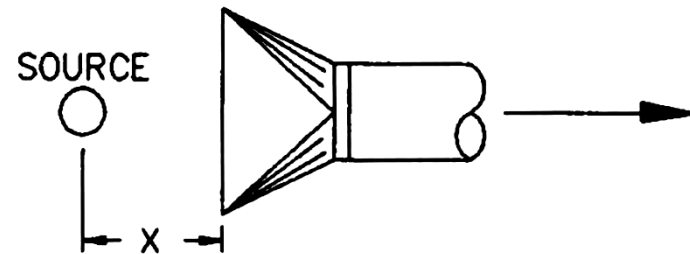
Concept of capture velocity

- Capture velocity: the velocity at a point in front of the hood, that is needed to oppose room air currents and capture the contaminants
- It is an old concept that only partially works
- Ignores:
 - Mass generation at source
 - Turbulence at the inlet
- Still widely used
- Many formulas for different shapes
- DallaValle equations are an example



Capture Hoods

- Control velocity = V_c or capture velocity
 - Velocity needed to overcome opposing forces
 - Cross drafts
 - Motion imparted by process, etc.
- Design parameter = Q
 - To determine the Q needed, we can use the velocity V_c needed to capture contaminant at point x in front of the hood

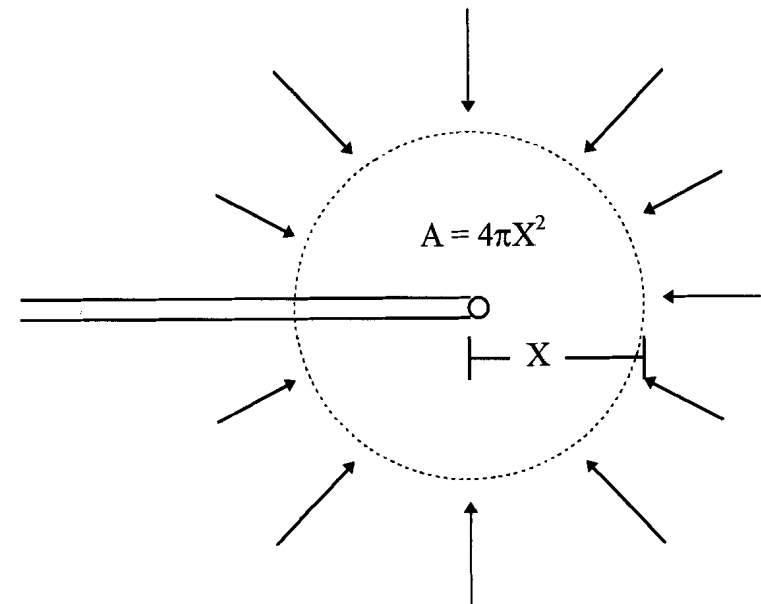


Source: Dinardi SR. (1998)



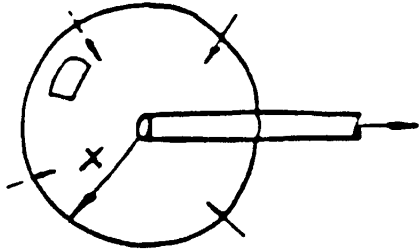
Capture velocity

- Relationship between Q , V_c and X
 - Assumptions
 - Contaminant source at point X
 - Point suction source
 - Air flows into point source from all directions

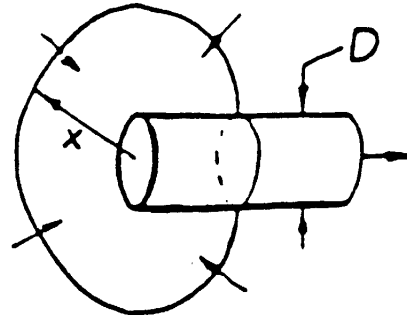




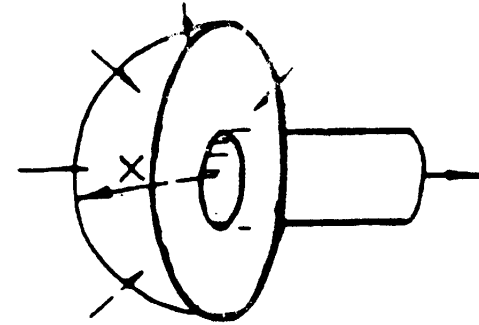
Capture velocity equations



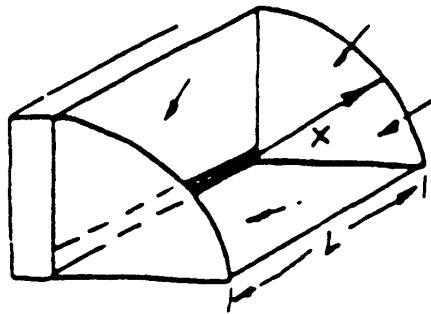
Point Source
Shape - Sphere
Area $\cong 4\pi X^2$



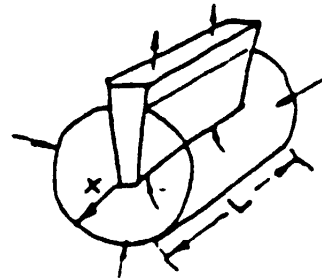
Plain Duct
Shape - ~Sphere
Area $\cong 4\pi X^2 - (\pi D^2 \div 4)$



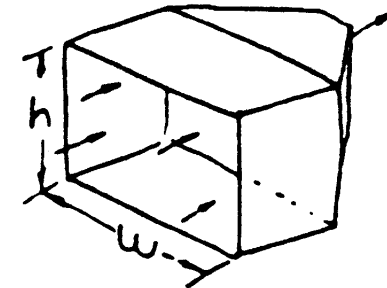
Flanged Duct
Shape ~ Half Sphere
Area $\cong 2\pi X^2$



Slot With Sides
Shape ~ 1/4 Cylinder
Area $\cong 1/2 \pi XL$



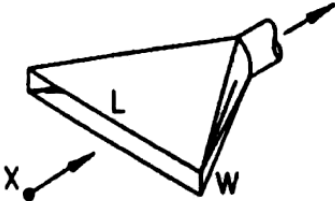
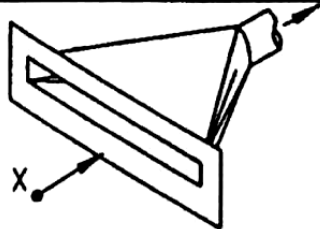
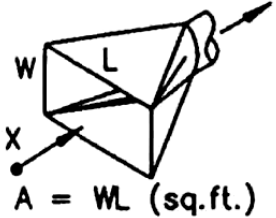
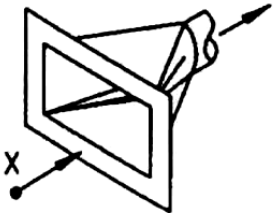
Free-Standing Slot
Shape ~ Cylinder
(+ Sphere)
Area $\cong 2\pi XL (+4\pi X^2)$



5-Sided Hood
Shape - Plane
Area = $h \times w$



More capture velocity equations

HOOD TYPE	DESCRIPTION	ASPECT RATIO, W/L	AIR FLOW
	SLOT	0.2 OR LESS	$Q = 3.7 LVX$
	FLANGED SLOT	0.2 OR LESS	$Q = 2.6 LVX$
	PLAIN OPENING	0.2 OR GREATER AND ROUND	$Q = V(10X^2 + A)$
	FLANGED OPENING	0.2 OR GREATER AND ROUND	$Q = 0.75V(10X^2 + A)$

Source: Plog, page 619

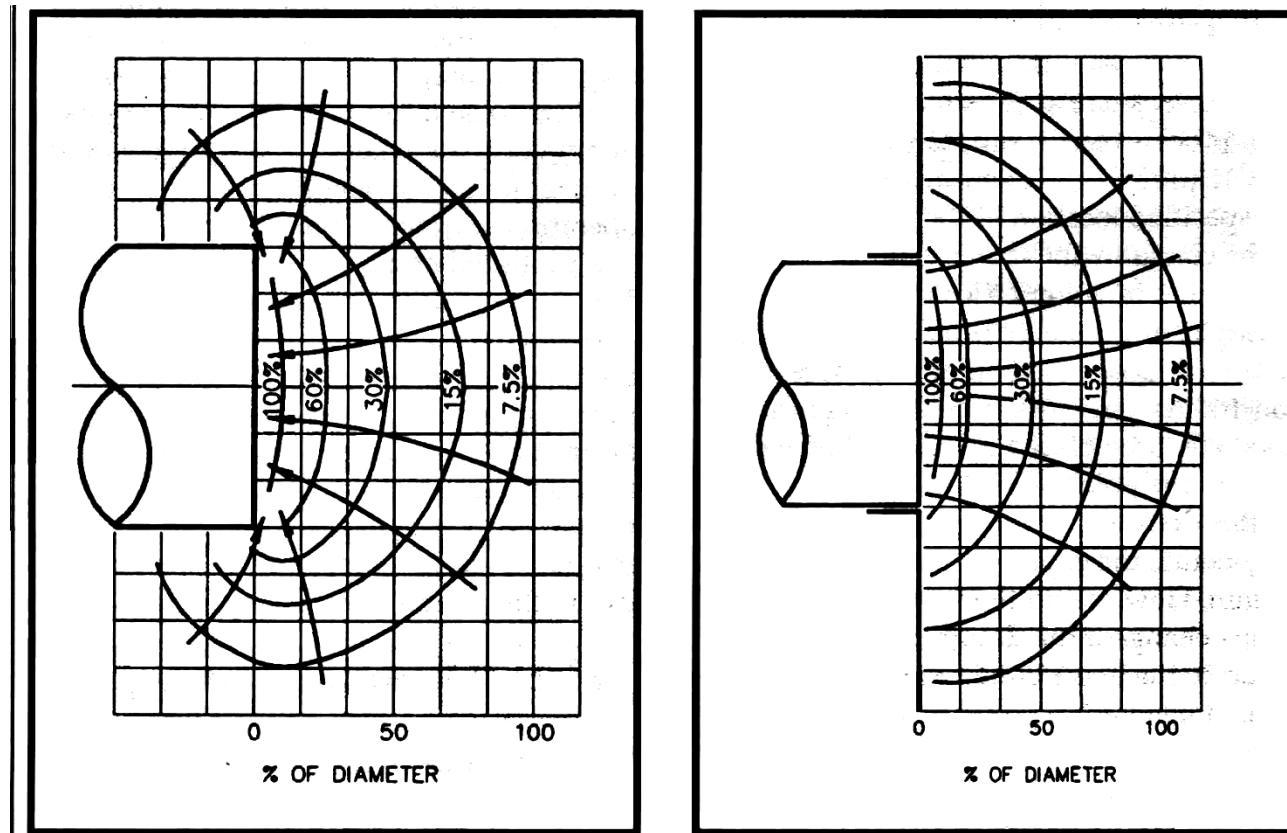


Effect of Flanging

- A surface parallel to the hood face to prevent unwanted air flow behind the hood
- Effects of flange:
 - Decreasing the Q needed to achieve contaminant capture (reduce by $\sim 25\%$)
 - Improving the capture velocity of a hood



Velocity profiles (non-flanged vs flanged)



Source: Plog, 2002, p 620



Range of capture velocities

Table 19–A. *Range of Capture Velocities*

Dispersion of Contaminant	Examples	Capture Velocity, ft/
Released with practically no velocity into quiet air.	Evaporation from tank; degreasing.	50–100
Released at low velocity into moderately still air.	Spray booths; intermittent container filling; low-speed conveyor transfers; welding; plating; pickling.	100–200
Active generation into zone of rapid air motion.	Spray painting in shallow booths; barrel filling; conveyor loading; crushers.	200–500
Released at high initial velocity into zone of very rapid air motion.	Grinding; abrasive blasting; tumbling.	500–2000

In each category above, a range of capture velocities is shown. The proper choice of values depends on several factors:

Lower End of Range

1. Room air currents minimal or favorable to capture.
2. Contaminants low toxicity or of nuisance value only.
3. Intermittent, low production.
4. Large hood-large air mass in motion.

Upper End of Range

1. Disturbing room air currents.
2. Contaminants of high toxicity.
3. High production, heavy use.
4. Small hood-local control only.

(Source: From American Conference of Governmental Industrial Hygienists (ACGIH®) *Industrial Ventilation: A Manual of Recommended Practice*, 23rd ed. Copyright

Source: Plog (2002).



END here

- Four example problems for homework follow



Example Problem 1

- Exterior hood with plain round opening
 - 14 inches in diameter, 24 inches deep
- Round duct leading up to hood
 - 6 inches in diameter,
- Transition section to hood
 - conical taper over 2 feet
- Required Q for system = 1000 ft^3
- What are the velocities at the hood face and within the duct leading to the hood?



Example Problem 2

- A 4" x 8" flanged hood is drawing 500 ft³/min of air. What is the velocity 6" in front of the hood?
- Hint: where.... Centerline!



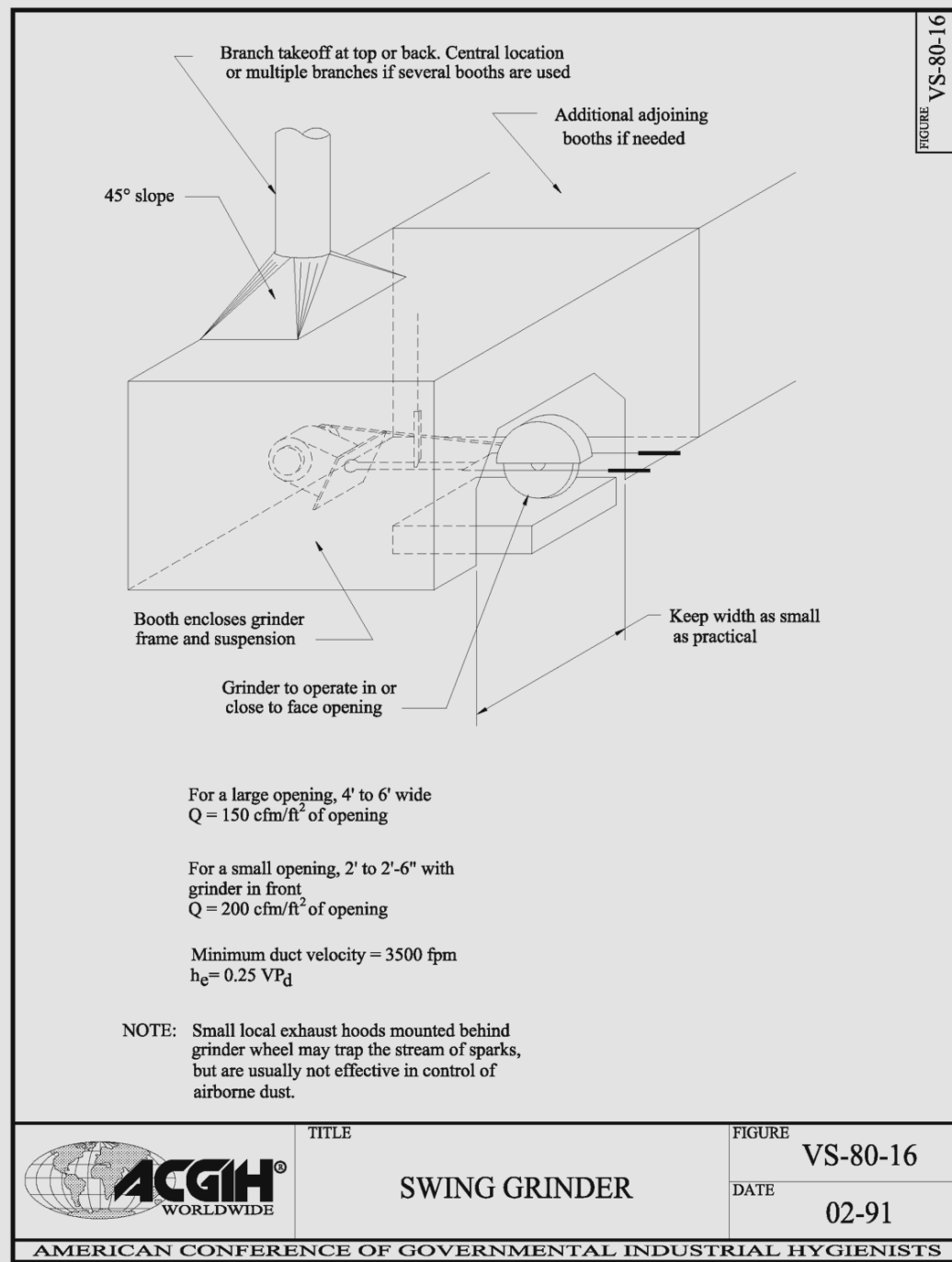
Example Problem 3

- Find P_{sh} and C_e for a plain end duct and $V=2000$ fpm (assume no friction loss and NTP)
- Hint: $F_e=0.93$



Example Problem 4 Swing grinder hood

- Hood dimensions; 3 ft high x 5 ft wide
- What Q is needed to get the recommended face velocity of 150 FPM?
- What Q is needed if the opening is 4 x 6 ft?
- Refer to Vent Manual, page 10-138 (25th ed)



Paint Booth





**Another, albeit more sophisticated
Paint Booth**



Air Flow

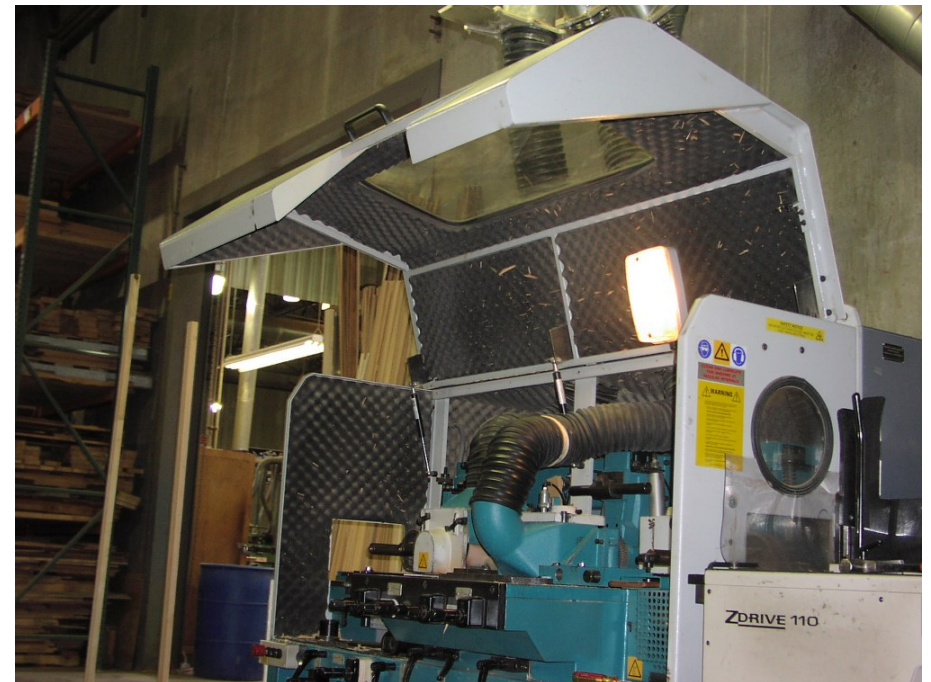


Abrasive Blasting Booth





Wood Products Manufacturing



Enclose device, draw air from points where dust is generated



Furniture Stripping

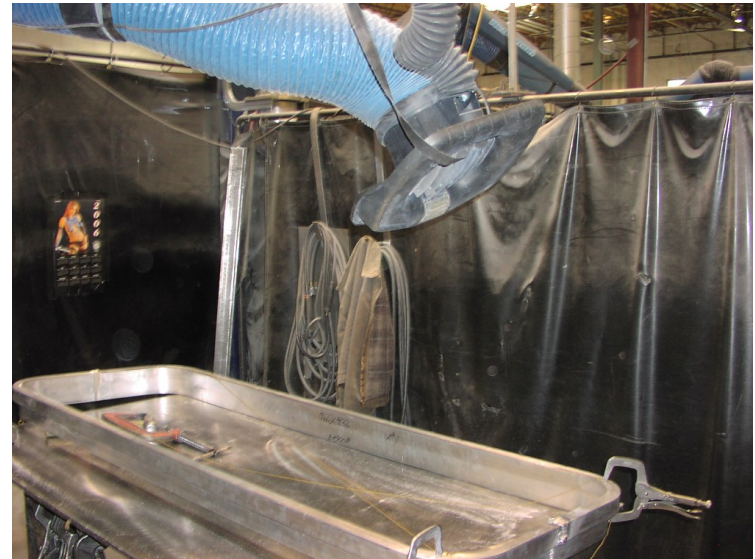


Local Exhaust Ventilation - Welding





Local Exhaust Ventilation - Welding



LEV is ineffective unless hood is proximal to particulate generation point (~ 1 duct dia.)





Push – Pull Hood - Electroplating

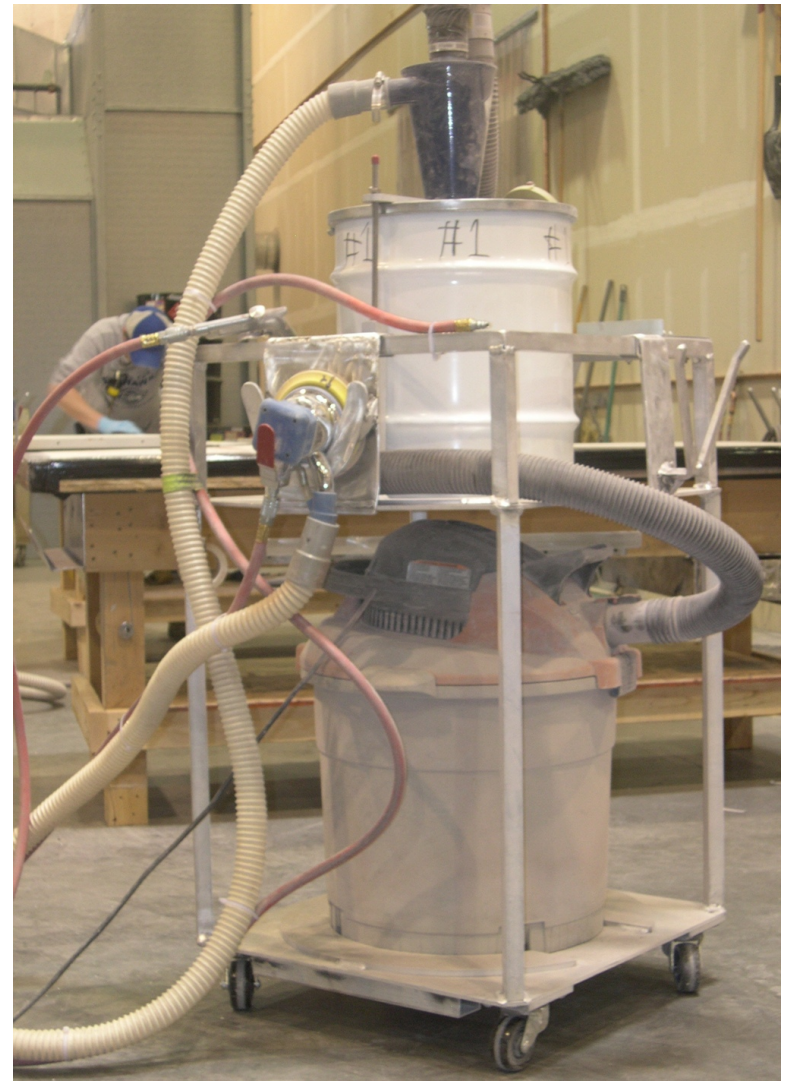


Metal Grinding Process





Tool Equipped LEV



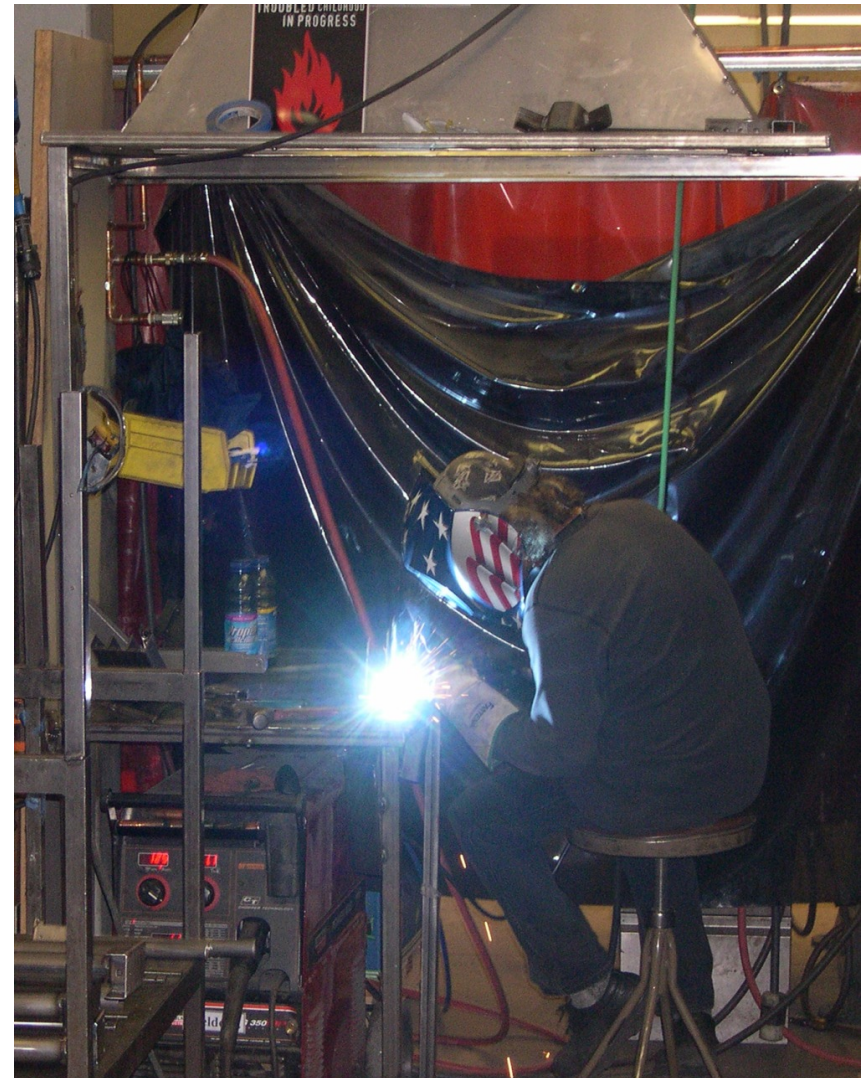


Canopy Hood – Glass Art



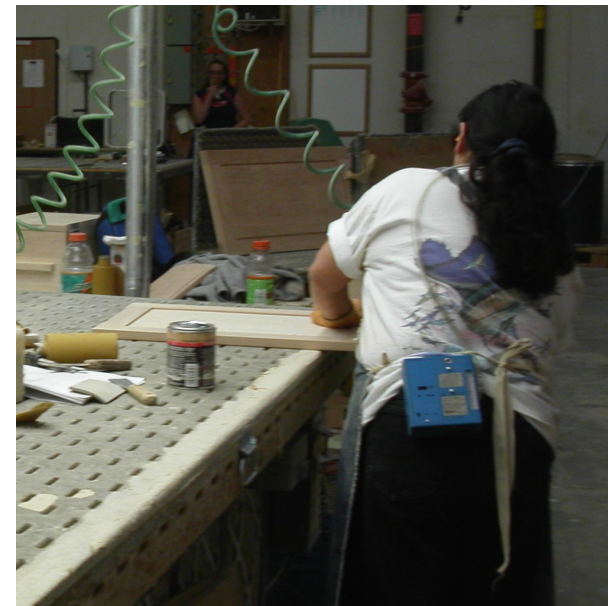


Inappropriate Use of Canopy Hood



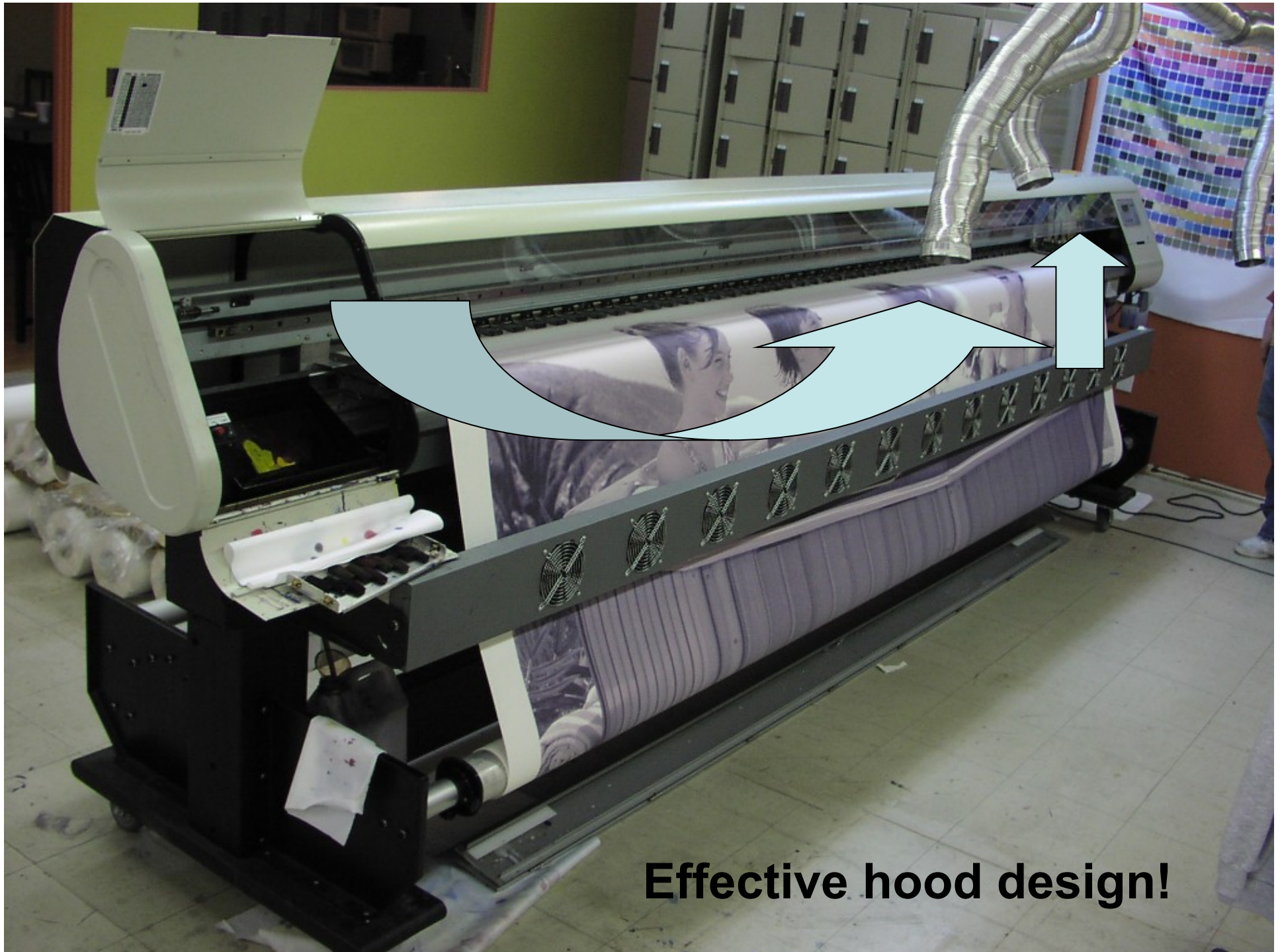


Downdraft Tables





Effective hood design?



Effective hood design!

