ESS 524 Class #6

Highlights from last Monday – Surabhi Today's highlights report on next Monday – Erich Highlights reporters – please send me your report by email.

• Great Week 2 journals. You are all doing some good thinking.

Today

- HW #2 on Matlab (Finite Difference code) due today Are there challenges to discuss now? More time needed?
- Class organization how is it going with Zoom?
- If you get stuck on HW assignments, please feel free to contact me and/or classmates directly with your questions.
- It's great to work together on problems, just prepare your own answers in the end.
- Zoom study sessions for you to interact, compare approaches and answers?

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Today

- Project updates
- Continuing with Finite Element Method (FEM)

Next Week

- Finite Volume Method (FVM)
- We will follow Patankar fairly closely, Ch 3 and Ch 4

HW #2

Getting the analytical solution?

- FDM Handling the second derivative (diffusion term)
- Expand with Product Rule, or not?

a (k(x) de) (#) when k(x) varies with K. D Product Rule Approach. $(k) = k(x) \frac{\partial^2 \phi}{\partial x^2} + \frac{\partial k}{\partial x} \frac{\partial \phi}{\partial x}$ $\rightarrow k_{3}(\varphi_{3+1} - 2\varphi_{3} + \varphi_{3-1}) + (k_{3+1} - k_{3-1})(\varphi_{\pm} - \varphi_{3-1})(\varphi_{\pm} - \varphi_{3-1}) + (k_{3+1} - k_{3-1})(\varphi_{\pm} - \varphi_{3-1})(\varphi_{\pm} - \varphi_{3-1}) + (k_{3+1} - k_{3-1})(\varphi_{\pm} - \varphi_{3-1})(\varphi_{\pm} - \varphi_{3-1})(\varphi_{3$ Problem - First derivatives Span 25x

HW #2

- FDM – Evaluate the slope at midpoints, so that all first derivatives are taken over span Δx rather than $2\Delta x$

2) Evaluate slopes at mid points. I assume k(x) is known at mid points or can be estimated there e.g kitz = (kj+i+kj-) $(\mathbf{x}) \longrightarrow [k \stackrel{\text{def}}{=}]_{j+l_{2}} - [k \stackrel{\text{def}}{=}]_{j-l_{2}}$ $= \left(k_{j+1/2}(\varphi_{j+1}-\varphi_j) - k_{j-1/2}(\varphi_j-\varphi_{j-1})\right) /$

$$S(x) = \int_{N}^{(s)} (x) = \frac{N}{2} \frac{d}{dx} \frac{d}{n} \frac{1}{k(k)} = \int_{M}^{(k)} (k) = \frac{M}{2} \frac{d}{dx} \int_{M}^{M} \frac{d}{k(k)} \frac{d}{dx} + S(k) = 0 \quad (1)$$

$$T_{at regpost e once} = \int_{N}^{N} \frac{d}{dx} \frac{d}{dx} = a \frac{p dy nomicl}{k(k)} \frac{d}{dx} = R(k)$$

$$\frac{d}{dx} = R(k) \frac{p_{1}^{(k)}}{dx} = a \frac{p dy nomicl}{k(k)} \frac{d}{dx} = R(k)$$

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$$\int_{M}^{N} \frac{d}{dx} = \frac{p(1)}{k} - \frac{p(k)}{k(k)} = a \frac{p dy nomicl}{k(k)} \frac{d}{dx}$$

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$$\frac{d}{dx} = R(k) \frac{p_{1}^{(k)}}{k(k)} = a \frac{p dy nomicl}{k(k)} \frac{T(k)}{k(k)}$$

$$\int_{N}^{N} \frac{d}{dx} = \frac{p(1)}{k} - \frac{p(k)}{k(k)} = \int_{N}^{\infty} \frac{d}{dk} \frac{d}{dk} = u(k)$$

$$\frac{d}{dx} = \frac{p(1)}{k(k)} - \frac{p(k)}{k(k)} = \int_{N}^{\infty} \frac{d}{dk} \frac{d}{dk}$$

Product Rule and Integration by Parts

= [uv] - [w(x)du(x) NT underta) = u dry + vau

Integrate (2) from *a* to *b* to get (1)

Product Rule and Integration by Parts

hv

When v(x) is the 2nd derivative term, and u(x) does not include a derivative, after integration by parts,

- both u(x) and v(x) appear with first derivatives in the new integral term.
- In general, v(x) is differentiated one time less, and u(x) is differentiated one time more.
- boundary conditions show up naturally in the new constant term.

The challenge -

- How to represent a 2nd order differential equation with piecewise 1st order functions?
- The 2nd derivative is identically zero everywhere
- except at the nodes, where it can be infinite.

The Solution - The weak form of the differential equation

- The weak form is a weighted-integral statement that is equivalent to the governing differential equation combined with its natural boundary conditions.
- The original equation is satisfied in an average sense, rather than point by point.
- The weak form is derived from the strong form by an integration by parts.
- After integration by parts, the 2nd derivative has been replaced by a 1st derivative, which is nonzero for a piecewise linear representation.

With Equation (17), the algebraic equations (12) and (13) in element j reduce to

$$-k_{j}\left[\frac{\mathrm{d}\tilde{\phi}}{\mathrm{d}x}\right]_{x_{j-1}}^{(j)} - \frac{k_{j}}{\Delta x_{j}}\phi_{j-1} + \frac{k_{j}}{\Delta x_{j}}\phi_{j} + S_{j}\frac{\Delta x_{j}}{2} = 0$$

$$k_{j}\left[\frac{\mathrm{d}\tilde{\phi}}{\mathrm{d}x}\right]_{x_{j}}^{(j)} + \frac{k_{j}}{\Delta x_{j}}\phi_{j-1} - \frac{k_{j}}{\Delta x_{j}}\phi_{j} + S_{j}\frac{\Delta x_{j}}{2} = 0$$
(18)

Note that if these two equations were added together, we would get an expected finite-volume expression for conservation of ϕ in element j, i.e.

$$k_j \left[\frac{\mathrm{d}\tilde{\phi}}{\mathrm{d}x} \right]_{x_j}^{(j)} - k_j \left[\frac{\mathrm{d}\tilde{\phi}}{\mathrm{d}x} \right]_{x_{j-1}}^{(j)} = S_j \ \Delta x_j \tag{19}$$

i.e. the difference in fluxes across the boundaries must equal the integrated production rate inside element j.

Equations for 3 linear elements, with 4 nodes

We have 6 weighting equations for 4 nodes.

- We need only 4 equations.
- The first and last equations are just the boundary conditions
- Add together the two equations that apply to the same boundary, but from the elements on opposite sides.
- This effectively isolates the residuals around that node
- Combining the equations at nodes 2 and 3 reduces the number of equations by 2
- We are left with 4 equations.

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 The flux terms will also cancel and vanish.