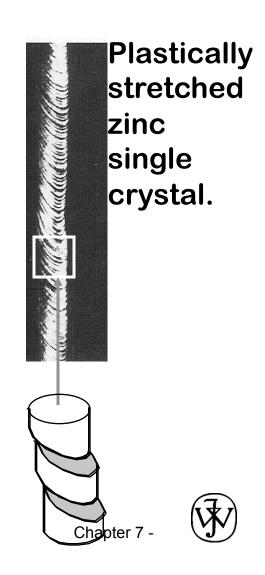
Chapter 7: Dislocations and strengthening mechanisms

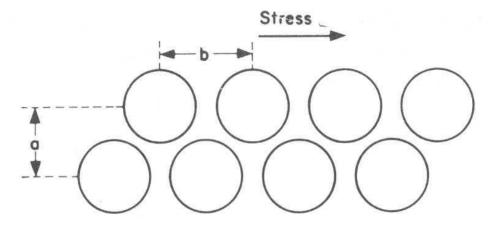
- Introduction
- Basic concepts
- Characteristics of dislocations
- Slip systems
- Slip in single crystals
- Plastic deformation of polycrystalline materials



Theoretical stress

Theoretical stress (Frenkel in 1926)

$$\tau = \frac{Gb}{2\pi a} \sin \frac{2\pi x}{b}$$



G: shear modulus

b: spacing between atoms in the direction of shear stress

a: spacing of the rows of atoms

x: shear translation

Theoretical stress (continued)

Hook's law

assumption: small strain

$$\tau = \frac{Gb}{2\pi a} \times \frac{2\pi x}{b} = G\frac{x}{a} = G\gamma$$

Theoretical critical shear stress (maximum stress):

$$\tau_{th} = \frac{b}{a} \frac{G}{2\pi}$$



Theoretical & experimental strength

There is much difference between theoretical and experimental strength

Reasons are:

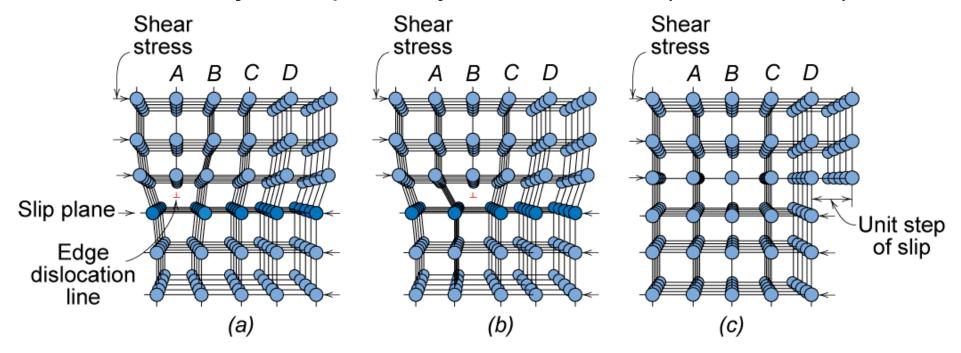
- Defects are present in all perfect crystal
- Dislocation movement makes plastic deformation easier than that predicted by the Frenkel calculation



Dislocation Motion

Dislocations & plastic deformation

 Cubic & hexagonal metals - plastic deformation by plastic shear or slip where one plane of atoms slides over adjacent plane by defect motion (dislocations).



 If dislocations don't move, deformation doesn't occur!

Adapted from Fig. 7.1,

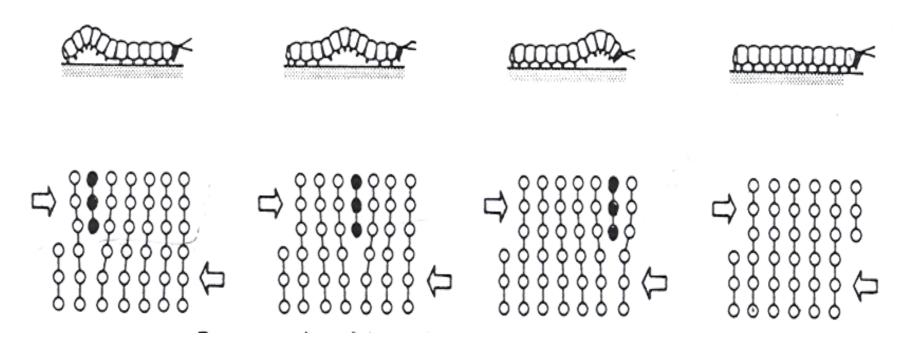
Callister 7e.

Chapter 7 - 5



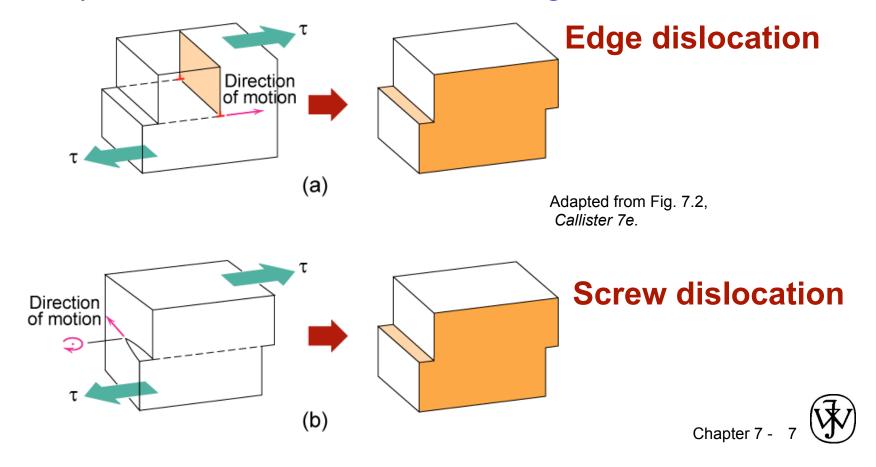
Analogy between caterpillar and dislocation motion

- Dislocation density: total dislocation length per unit volume
- 10³ mm⁻² for pure metal crystals; 10⁹-10¹⁰mm⁻² for heavily deformed metals; 10⁵-10⁶mm⁻² for heat-treated deformed metals



Dislocation Motion

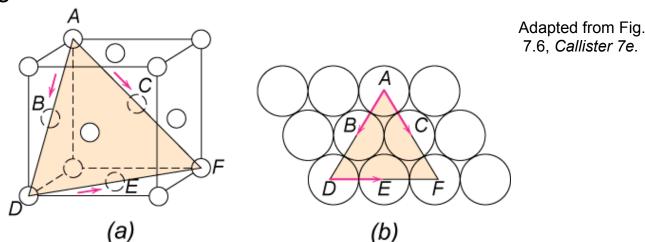
- Dislocation moves along slip plane in slip direction perpendicular to dislocation line
- Slip direction same direction as Burgers vector



Deformation Mechanisms

Slip System

- Slip plane plane allowing easiest slippage
 - Wide interplanar spacings highest planar densities
- Slip direction direction of movement Highest linear densities



- FCC Slip occurs on {111} planes (close-packed) in <110> directions (close-packed)
 - => total of 12 slip systems in FCC
- in BCC & HCP other slip systems occur

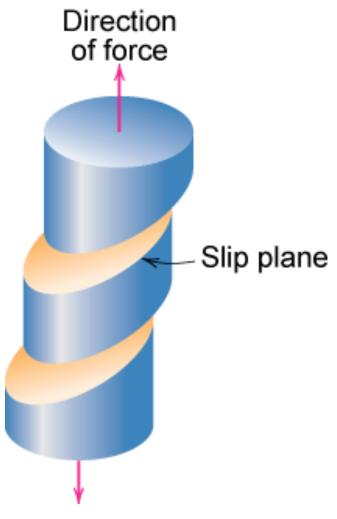


Slip planes and directions for common crystal structure

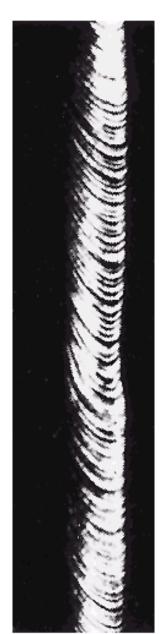
Table 7.1 Slip Systems for Face-Centered Cubic, Body-Centered Cubic, and Hexagonal Close-Packed Metals

Metals	Slip Plane	Slip Direction	Number of Slip Systems
	Face-Cente	red Cubic	
Cu, Al, Ni, Ag, Au	{111}	$\langle 1\overline{1}0 \rangle$	12
	Body-Cente	ered Cubic	
α -Fe, W, Mo	{110}	$\langle \overline{1}11 \rangle$	12
α-Fe, W	{211}	$\langle \overline{1}11 \rangle$	12
α-Fe, K	{321}	$\langle \overline{1}11 \rangle$	24
	Hexagonal C	lose-Packed	
Cd, Zn, Mg, Ti, Be	{0001}	$\langle 11\overline{2}0\rangle$	3
Ti, Mg, Zr	$\{10\overline{1}0\}$	$\langle 11\overline{2}0\rangle$	3
Ti, Mg	$\{10\overline{1}1\}$	$\langle 11\overline{2}0\rangle$	6

Single Crystal Slip



Adapted from Fig. 7.8, Callister 7e.

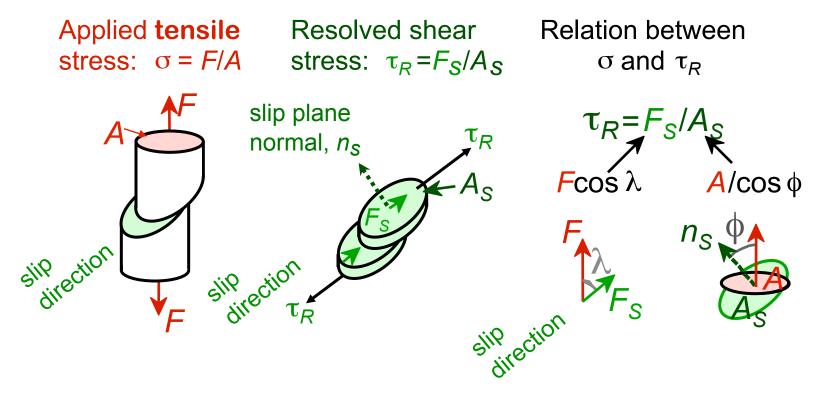


Adapted from Fig. 7.9, *Callister 7e.*



Stress and Dislocation Motion

- Crystals slip due to a resolved shear stress, τ_R .
- Applied tension can produce such a stress.

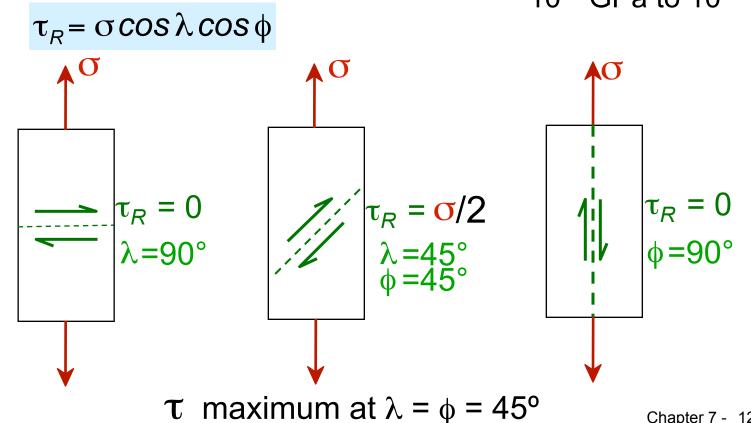


$$\tau_R = \sigma \cos \lambda \cos \phi$$

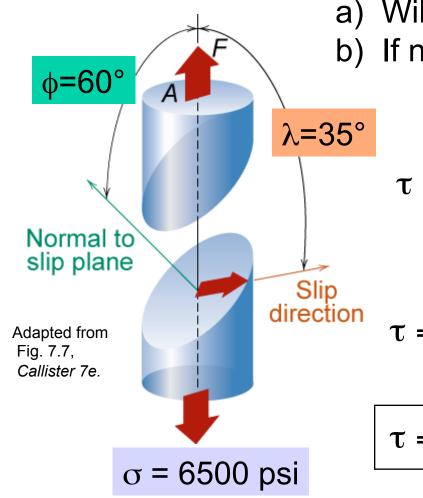
Critical Resolved Shear Stress

- Condition for dislocation motion:
- Crystal orientation can make it easy or hard to move dislocation

 $\tau_R > \tau_{CRSS}$ ftypically 10^{-4} GPa to 10^{-2} GPa



Ex: Deformation of single crystal



- a) Will the single crystal yield?
- b) If not, what stress is needed?

$$\tau_{crss}$$
 = 3000 psi

$$\tau = \sigma \cos \lambda \cos \phi$$

$$\sigma = 6500 \text{ psi}$$

$$\tau = (6500 \text{ psi}) (\cos 35^{\circ})(\cos 60^{\circ})$$

$$= (6500 \text{ psi}) (0.41)$$

$$\tau = 2662 \text{ psi} \quad < \tau = 3000 \text{ ps}$$

$$\tau$$
 = 2662 psi $<$ τ_{crss} = 3000 psi

So the applied stress of 6500 psi will not cause the crystal to yield.



Ex: Deformation of single crystal

What stress *is* necessary (i.e., what is the yield stress, σ_v)?

$$\tau_{crss} = 3000 \text{ psi} = \sigma_y \cos \lambda \cos \phi = \sigma_y (0.41)$$

$$\therefore \sigma_y = \frac{\tau_{crss}}{\cos \lambda \cos \phi} = \frac{3000 \text{ psi}}{0.41} = \frac{7325 \text{ psi}}{0.41}$$

So for deformation to occur the applied stress must be greater than or equal to the yield stress

$$\sigma \ge \sigma_y = 7325 \, \text{psi}$$

Slip Motion in Polycrystals

- Stronger grain boundaries pin deformations
- Slip planes & directions
 (λ, φ) change from one
 crystal to another.
- τ_R will vary from one crystal to another.
- The crystal with the largest τ_R yields first.
- Other (less favorably oriented) crystals yield later.



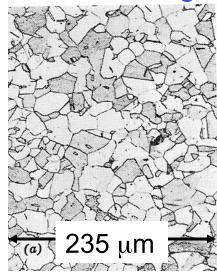
Adapted from Fig. 7.10, Callister 7e. (Fig. 7.10 is courtesy of C. Brady, National Bureau of Standards [now the National Institute of Standards and Technology, Gaithersburg, MD].)



Anisotropy in σ_y

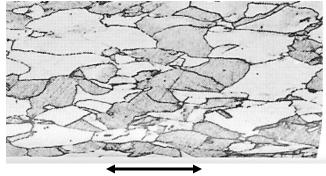
Can be induced by rolling a polycrystalline metal

before rollingafter rolling



- isotropic

since grains are approx. spherical & randomly oriented.



Adapted from Fig. 7.11, Callister 7e. (Fig. 7.11 is from W.G. Moffatt, G.W. Pearsall, and J. Wulff, The Structure and Properties of Materials, Vol. I, Structure, p. 140, John Wiley and Sons, New York, 1964.)

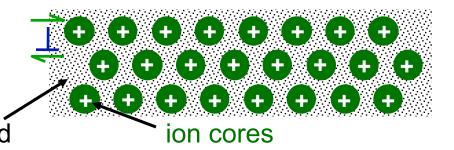
rolling direction

- anisotropic

since rolling affects grain orientation and shape.

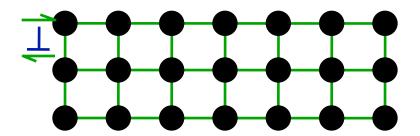
Dislocations & Materials Classes

- Metals: Disl. motion easier.
 - -non-directional bonding
 - -close-packed directions for slip. electron cloud



Covalent Ceramics

 (Si, diamond): Motion hard.
 -directional (angular) bonding



Ionic Ceramics (NaCl):

 Motion hard.
 -need to avoid ++ and - - neighbors.

