# **Chapter 8: Mechanical Failure**

#### Topics

- How do flaws in a material initiate failure?
- How is fracture resistance quantified; how do different material classes compare?
- How do we estimate the stress to fracture?





### **Fracture mechanisms**

- Ductile fracture
  - Occurs with plastic deformation
- Brittle fracture
  - Little or no plastic deformation
  - Catastrophic



### **Ductile vs Brittle Failure**



### **Example: Failure of a Pipe**

#### Ductile failure:

--one piece--large deformation



#### • Brittle failure: --many pieces

--small deformation

Figures from V.J. Colangelo and F.A. Heiser, *Analysis of Metallurgical Failures* (2nd ed.), Fig. 4.1(a) and (b), p. 66 John Wiley and Sons, Inc., 1987. Used with permission.



# **Moderately Ductile Failure**

#### • Evolution to failure: void growth shearing void necking fracture and linkage at surface nucleation ۸O 000 $\sim$ 50 mm Resulting fracture surfaces (steel) 100 mm particles From V.J. Colangelo and F.A. Heiser, Fracture surface of tire cord wire serve as void Analysis of Metallurgical Failures (2nd loaded in tension. Courtesy of F.

nucleation

pp. 347-56.)

sites.

Analysis of Metallurgical Failures (2ndIoaced.), Fig. 11.28, p. 294, John Wiley andRoeSons, Inc., 1987. (Orig. source: P.OH.Thornton, J. Mater. Sci., Vol. 6, 1971,OH.

Roehrig, CC Technologies, Dublin, OH. Used with permission.



### **Ductile vs. Brittle Failure**



cup-and-cone fracture

brittle fracture

Adapted from Fig. 8.3, Callister 7e.



### **Brittle Failure**

Arrows indicate pt at which failure originated



Adapted from Fig. 8.5(a), *Callister 7e.* 



### **Brittle Fracture Surfaces**

• Intergranular (between grains)



304 S. Steel (metal)  Intragranular (within grains)
 316 S. Steel (metal)





Polypropylene (polymer) Al Oxide (ceramic)



(Orig. source: K. Friedrick, *Fracture 1977*, Vol. 3, ICF4, Waterloo, CA, 1977, p. 1119.)

# **Ideal vs Real Materials**

• Stress-strain behavior (Room T):



- DaVinci (500 yrs ago!) observed...
  - -- the longer the wire, the smaller the load for failure.
- Reasons:
  - -- flaws cause premature failure.
  - -- Larger samples contain more flaws!

### Flaws are Stress Concentrators!



Results from crack propagation

Griffith Crack

$$\sigma_m = 2\sigma_o \left(\frac{a}{\rho_t}\right)^{1/2} = K_t \sigma_o$$

where

 $\rho_t$  = radius of curvature  $\sigma_o$  = applied stress  $\sigma_m$  = stress at crack tip

Adapted from Fig. 8.8(a), Callister 7e.

#### **Concentration of Stress at Crack Tip**



### **Engineering Fracture Design**

Avoid sharp corners!



### **Crack Propagation**

Cracks propagate due to sharpness of crack tip

A plastic material deforms at the tip, "blunting" the crack.



#### Energy balance on the crack

- Elastic strain energy-
  - energy stored in material as it is elastically deformed
  - this energy is released when the crack propagates
  - creation of new surfaces requires energy



### When Does a Crack Propagate?

Crack propagates if above critical stress

i.e., 
$$\sigma_m > \sigma_c$$
  
or  $K_t > K_c$   $\sigma_c = \left(\frac{2E\gamma_s}{\pi a}\right)^{1/2}$ 

where

- E = modulus of elasticity
- $-\gamma_s$  = specific surface energy
- a = one half length of internal crack
- $K_c = \sigma_c / \sigma_0$

For ductile => replace  $\gamma_s$  by  $\gamma_s + \gamma_p$ where  $\gamma_p$  is plastic deformation energy

#### **Fracture Toughness**



### **Design Against Crack Growth**

• Crack growth condition:

 $K \geq K_c = Y_{O}\sqrt{\pi a}$ 

- Largest, most stressed cracks grow first!
  - --Result 1: Max. flaw size dictates design stress.



--Result 2: Design stress dictates max. flaw size.



# **Design Example: Aircraft Wing**

- Material has K<sub>c</sub> = 26 MPa-m<sup>0.5</sup>
- Two designs to consider...
  - Design A --largest flaw is 9 mm
    - --failure stress = 112 MPa

 $\sigma_c =$ 

• Use...

R

Design B --use same material --largest flaw is 4 mm --failure stress = ?

• Key point: Y and K<sub>c</sub> are the same in both designs. --Result: 112 MPa 9 mm

$$\begin{pmatrix} 4 \text{ mm} \\ \sigma_c \sqrt{a_{\text{max}}} \end{pmatrix}_A = \begin{pmatrix} \sigma_c \sqrt{a_{\text{max}}} \\ \sigma_c \sqrt{a_{\text{max}}} \end{pmatrix}_B$$
Answer:  $(\sigma_c)_B = 168 \text{ MPa}$ 
Reducing flaw size pays off!

### **Loading Rate**

- Increased loading rate...
  - -- increases  $\sigma_y$  and TS
  - -- decreases %EL

• Why? An increased rate gives less time for dislocations to move past obstacles.





### **Impact Testing**



### **Temperature**

- Increasing temperature... --increases %*EL* and *K<sub>c</sub>*
- Ductile-to-Brittle Transition Temperature (DBTT)...



### Design Strategy: Stay Above The DBTT!

• Pre-WWII: The Titanic



• WWII: Liberty ships



• Problem: Used a type of steel with a DBTT ~ Room temp.



### **SUMMARY**

- Engineering materials don't reach theoretical strength.
- Flaws produce stress concentrations that cause premature failure.
- Sharp corners produce large stress concentrations and premature failure.
- Failure type depends on *T* and stress.

