

#### We'll start class at 7:05

<u>Session 2</u> Harmonic oscillators: Simple, damped, driven resonance

1/5/2023

# Course syllabus and schedule – first part...

#### See : http://courses.washington.edu/phys536/syllabus.htm

Session	date	Day	Readings:	K=Kinsler, H=Heller	Торіс
1	3-Jan	Tue	K ch. 1	H: Ch. 1, 2	Course intro, acoustics topics, overview of wave properties; pulses, transverse and longitudinal waves, overview of sound speeds
2	5-Jan	Thu	K ch. 1	H: Ch. 9, 10	harmonic oscillators: simple, damped, driven; complex exponential solutions, electrical circuit analogy, resonance, Q factor
3	10-Jan	Tue	K ch. 1	H: Ch. 3	Fourier methods: Fourier series, integrals, Fourier transforms, discrete FTs, sampling and aliasing
4	12-Jan	Thu	K. chs 10	H: Ch. 4, 11	Frequencies and aliasing; convolution and correlation; discrete convolution; digital filtering, optimal filters, FIR filters, noise spectra; power spectra. REPORT 1 PROPOSED TOPIC DUE
5	17-Jan	Tue	K. ch. 2, 3, 4	H: Ch. 13, 15	waves in strings, bars and membranes; Acoustic wave equation; speed of sound; Harmonic plane waves, intensity, impedance.
6	19-Jan	Thu	K. Ch. 5, 6	H: Ch. 1	Spherical waves; transmission and reflection at interfaces
7	24-Jan	Tue	K. Ch. 8	H: Ch. 7	Radiation from small sources; Baffled simple source, piston radiation, pulsating sphere;
8	26-Jan	Thu	K: Ch. 10	H: Chs. 13-15	Near field, far field; Radiation impedance; resonators, filters
9	31-Jan	Tue	K. Ch. 9-10	H: Chs. 16-19	Musical instruments: wind, string, percussion
10	2-Feb	Thu	K. Ch 14		Transducers for use in air: Microphones and loudspeakers
11	7-Feb	Tue	K. Ch 11	H: Chs. 21-22	The ear, hearing and detection
12	9-Feb	Thu	K. Chs 5,11		Decibels, sound level, dB examples, acoustic intensity; noise, detection thresholds. REPORT 1 PAPER DUE by 7 PM; REPORT 2 PROPOSED TOPIC DUE

#### From last time:

- T-Th, 7:00-8:50 pm, A110 Physics-Astronomy, and/or Zoom
  - I will attend by Zoom only for most sessions
  - In-person (optional) meetings on a few later dates for demonstrations
- R. J. Wilkes
  - 206-543-4232 , wilkes@uw.edu
     Office hrs: after class, or by appointment via zoom/phone
- Website: <u>http://courses.washington.edu/phys536</u>
- Books:
  - Fundamentals of Acoustics 3<sup>rd</sup> ed. (1982) or 4<sup>th</sup> ed. (2000), Lawrence E. Kinsler, A. R. Frey, A. B. Coppens, J. V. Sanders; Wiley
  - Why you hear what you hear, Eric J. Heller, Princeton University Press, 2013, ISBN: 978-0691148595
  - Books are on 2 hr reserve in the UW Odegaard Undergraduate Library see http://www.lib.washington.edu/about/hours/
- Grades see class calendar on website for due dates
  - Two 5 p term papers (100 points each) submit proposed topics by email
  - End-of-term exam (100 pts, take-home; no final exam in exam week)

#### Announcements

- SPECIAL: Next Tuesday, class will start at 7:30 pm, not 7 pm.
  - Most sessions thereafter will be Zoom only (I will not come in)
    - HOWEVER: you are quite welcome to come to A110 PAB to meet with fellow students and attend the zoom sessions together
    - Later, I will come in and some sessions in-person, when demonstrations are part of the show – I'll notify you a week in advance of these dates
      - You can watch me do the demos on Zoom, of course

# Questions from a student last time

Bubba C. figured out the answers for himself later, but for benefit of everyone else:

- In air, the density will be smaller when temp is higher, so why is the speed of sound faster in hotter air? Or is the speed of sound faster in hotter air only if the density is constant between the hot and the cold air?
  - The plots shown were for density and other parameters held constant
- For the SOFAR layer, I can see why there would be total internal reflection at 1000 m below the surface, but why would there be reflection at 100 m below the surface?
- The channel is centered on the sound speed minimum and reflection occurs because the sound speed increases both above and below the minimum around 1000 m compare to index of refraction in optics. PS: Thanks for the nice picture



#### Sound speed and frequency

- Speed of sound does not vary much with *f* 
  - If c depended on f, sound signals would change significantly depending upon how far away you are
    - This is called "dispersion"
  - Small *f* dependence can be observed, for example in undersea sound transmission
    - A pulse with many frequencies in it will spread out in time as it travels
    - Pitch will vary pulse spreads; ping becomes a "chirp"

Pulse moving in a dispersive medium

20

40

80

60

#### Frequency range terminology

- Audible/"Acoustic" nominally 20 Hz to 20 kHz (actual range for most people is closer to 50Hz-15kHz)
- Infrasonic below audible (below about 0.1 Hz we call it "vibration" !)
- Ultrasonic Above 20 kHz





#### Simple harmonic oscillator

Simple harmonic oscillator  
• SHM: position and speed of mass  
– Initial conditions give constants needed  
Initial conditions : 
$$At t = 0$$
,  $x = x_0$ ,  $speed$   $u_0 = \frac{dx(t)}{dt}\Big|_{t=0}$   
Substitute in II :  $x = A\cos(\omega_0 t + \phi_0) \rightarrow x_0 = A\cos(\phi_0)$ ,  $u_0 = -A\omega_0\sin(\phi_0)$   
 $x_0^2 = A^2\cos^2(\phi_0)$ ,  $u_0^2 = -A^2\omega_0^2\sin^2(\phi_0) \rightarrow A^2(\cos^2(\phi_0) + \sin^2(\phi_0)) = x_0^2 + (u_0/\omega_0)^2$   
 $A = x_0/\cos(\phi_0) = -u_0/\sin(\phi_0) \rightarrow -u_0/\omega_0 x_0 = \tan(\phi_0)$   
So  $A = \sqrt{x_0^2 + (u_0/\omega_0)^2}$ ,  $\phi_0 = \tan^{-1}(-u_0/\omega_0 x_0)$   
Substitute in III :  $x = A_1 e^{+i\omega_0 t} + A_2 e^{-i\omega_0 t} \rightarrow x_0 = A_1 + A_2$ ,  $u_0 = (A_1 - A_2)i\omega_0$   
So  $A_1 = \frac{1}{2}(x_0 - i\frac{u_0}{\omega_0})$ ,  $A_2 = \frac{1}{2}(x_0 + i\frac{u_0}{\omega_0}) \rightarrow x(t) = x_0\cos(\omega_0 t) + \frac{u_0}{\omega_0}\sin(\omega_0 t)$   
 $x_0$ ,  $u_0$  real  $\rightarrow \text{Im}(x(t)) = 0$ , and  $\text{Re}(x(t)) = a\cos(\omega_0 t) - b\sin(\omega_0 t)$   
Treating x, u and A as complex, can write solution compactly as  $x = Ae^{+i\omega_0 t}$   
Then speed  $u = \frac{dx}{dt} = i\omega_0 x = i\omega_0 Ae^{+i\omega_0 t}$ , acceleration  $a = \frac{du}{dt} = -\omega_0^2 x = -\omega_0^2 Ae^{+i\omega_0 t}$ 



# Damped harmonic oscillator

- Next, more realistic case: damped harmonic oscillator
  - Damping = friction or resistance  $\rightarrow$  dissipates energy in oscillator
  - Total energy (K + V) decreases with time until oscillator stops
- Compare behavior of free vs damped oscillator:





Damping force (resistance) opposes motion, most commonly proportional to speed:

$$f_r = -R_m \frac{dx}{dt} \rightarrow m \frac{d^2x}{dt^2} + R_m \frac{dx}{dt} + sx = 0$$
 damped oscillator

General complex form of solution:  $x = Ae^{\gamma t}$ 

Put this into eqn: 
$$m\frac{d^2x}{dt^2} + R_m\frac{dx}{dt} + sx = 0 \implies \left(\gamma^2 + \frac{R_m}{m}\gamma + \frac{s}{m}\right)Ae^{\gamma t} = 0$$

Must be true for any t, so : 
$$\left(\gamma^2 + \frac{R_m}{m}\gamma + \frac{s}{m}\right) = 0$$
; recall natural f :  $\omega_0^2 = \frac{s}{m}$ 

Solution of quadratic in  $\gamma$ :  $\gamma = -\beta/2 \pm \sqrt{\beta^2 - 4\omega_0^2}/2$ ; with  $\beta = R_m/2m$ 

### Damped oscillators

• Notice: If  $R_m = 0$ , we recover undamped case, and;

$$\gamma = \pm \sqrt{-\omega_0^2} = \pm i\omega_0$$

• Also, in most acoustics applications damping is relatively weak,  $so \omega_{0} > \beta; \quad define \omega_{d}$   $\omega_{d} = \sqrt{\omega_{0}^{2} - \beta^{2}} \implies \gamma = -\beta \pm i\omega_{d} \frac{x}{x_{0}}$ So solution is  $x = e^{-\beta t} \left( A_{1}e^{i\omega_{0}t} + A_{2}e^{-i\omega_{0}t} \right)^{\frac{1}{2}}$ With real part  $x = Ae^{-\beta t} \left( \cos(\omega_{0}t) + \phi \right);$ 

Get the real constants  $A, \phi$  from initial conditions.

• Exponential envelope has decay factor  $\beta$ , so the characteristic time for damping (time to drop by factor 1/e)  $\tau_d$ = 1/ $\beta$ = 2m/R<sub>m</sub>

# Damped harmonic oscillator

- If damping (R<sub>m</sub>) is small, oscillations continue, with slowly diminishing amplitude
- If damping is large, no oscillations, just slow return to equilibrium x
- If damping is "juuust right" (critical damping), returns to equilibrium x=0 smoothly and in shortest possible time
  - Near-critical damping: few oscillations, and a relatively prompt return



hyperphysics.phy-astr.gsu.edu

critical damping occurs when  $R_m = 2m\omega_0$ 

# Damped harmonic oscillator example

- At t = 0, damped harmonic oscillator is displaced from equilibrium by 0.2 m, where F=4 N, and released. Displacement vs t is shown below:
  - Estimate (a) The mass of the oscillator, (b) The decay factor  $\beta$ , (c) The frequencies  $\omega_d$  and  $\omega_0$



Damped harmonic oscillator example



19 cycles in 60 sec so period  $T = 3.15s \rightarrow T = \frac{1}{f} = \frac{2\pi}{\omega_d} = \frac{2\pi}{\sqrt{\omega_0^2 - \beta^2}}$ 



////////////

m

$$\omega_0^2 = k/m \quad \Rightarrow \quad T = \frac{2\pi}{\sqrt{(k/m) - \beta^2}} \quad \Rightarrow \quad \omega_d = \frac{2\pi}{T} = 2rad/s$$

 $decay: A(t) / A(0) = e^{-\beta t}; \text{ Initial amplitude } A(0)=0.2 \text{m drops by } 1/2 \text{ at } 20 \text{s}$   $\Rightarrow 1/2 = e^{-\beta(20)} \Rightarrow -\ln 2 = -\beta(20s) \Rightarrow \beta = \ln 2 / (20s) = 0.035$   $\omega_d = \sqrt{(k/m)} - \beta^2 \Rightarrow \omega_d^2 = (k/m) - \beta^2 \Rightarrow k/m = \omega_d^2 + \beta^2$   $m = k / (\omega_d^2 + \beta^2) = 20 / (4\pi^2 / T^2 + 0.035^2) \sim 5kg$  $\omega_0 = \sqrt{k/m} = \sqrt{20/5} = 2rad / s \Rightarrow f = \omega_0 / 2\pi = 0.32Hz$ 

• Notice that  $\beta$  is small, so  $\omega_{d} \sim \omega_{0}$ 

Oscillator with driving force  
• Driven oscillator: force applied to m  

$$m\frac{d^{2}x}{dt^{2}} + R_{m}\frac{dx}{dt} + sx = f(t) = F\cos(\omega t)$$
driving force applied to oscillator  
(Assume F is sinusoidal)  

$$f = Fe^{i\omega t} \rightarrow \text{Again assume general complex form of solution: } x(t) = Ae^{i\omega t}$$
Put into  $m\frac{d^{2}x}{dt^{2}} + R_{m}\frac{dx}{dt} + sx = f(t) \rightarrow (-A\omega^{2}m + iA\omega R_{m} + As)e^{i\omega t} = Fe^{i\omega t}$   
Solve for  $A : A = \frac{F}{i\omega(i\omega m + R_{m} - is/\omega)} \rightarrow x(t) = \frac{Fe^{i\omega t}}{i\omega[R_{m} + i(\omega m - s/\omega)]}$   
Speed :  $u(t) = \frac{\partial x}{\partial t} = \frac{Fe^{i\omega t}}{[R_{m} + i(\omega m - s/\omega)]}$ 

x and u are still treated as complex quantities: define *complex mechanical impedance* 

$$Z_m = R_m + iX_m$$
; mechanical reactance  $X_m = (\omega m - s / \omega)$ 

### Analogy - Electrical oscillators: RLC

- In electrical circuits, for the driven oscillator:
- $L\frac{d^2q}{dt^2} + R\frac{dq}{dt} + \frac{1}{C}q = V(t) \quad \text{driving voltage applied to RLC circuit}$

Solution for charge  $\rightarrow q(t) = \frac{V(t)e^{i\omega t}}{i\omega \left[R + i(\omega L - 1/\omega C)\right]}$ 

Current:  $I(t) = \frac{Fe^{i\omega t}}{Z}$  with Z the *complex* electrical *impedance* 

$$Z = R + iX = |Z|e^{i\Theta}; \operatorname{Re}[Z] = R; \operatorname{Im}[Z] = reactance X = (\omega L - 1/\omega C)$$

$$Z = \sqrt{R^2 + (\omega L - 1/\omega C)^2}; \quad \Theta = \tan^{-1} \frac{X}{Z}; \quad \text{Resonant frequency} \quad \omega_0 = \sqrt{\frac{1}{LC}}$$

– This is a *series* RLC circuit: same *I* through all components

– In mechanical oscillator: same x and u for all parts

### Driven damped mechanical oscillator

Analogy to electrical circuits: mechanical impedance complex impedance  $Z_m = R_m + iX_m = |Z_m|e^{i\Theta}$  $\operatorname{Re}[Z_m] = R_m; \quad \operatorname{Im}[Z_m] = \operatorname{reactance} X_m = (\omega m - s / \omega)$  $\left|Z_{m}\right| = \sqrt{R_{m}^{2} + \left(\omega m - s / \omega\right)^{2}},$  $Z_{e}$  = ratio of V to I  $\Theta = \tan^{-1} \frac{X_m}{Z_m}$  $Z_m$  = ratio of driving force to speed "mechanical ohm" has Displacement:  $x(t) = \frac{Fe^{i\omega t}}{i\omega \left[R_m + i\left(\omega m - s / \omega\right)\right]}$ units of force/speed Speed:  $u(t) = \frac{Fe^{i\omega t}}{\left[R_m + i\left(\omega m - s/\omega\right)\right]} = \frac{f(t)}{Z_m} \rightarrow Z_m = \frac{f(t)}{u(t)}$ 

### Driven damped mechanical oscillator

• Driven oscillator differential eqn and solutions:

$$m\frac{d^{2}x}{dt^{2}} + R_{m}\frac{dx}{dt} + sx = f(t) = Fe^{i\omega t} \quad \text{.but actual displacement has to be real!}$$

$$\Rightarrow \text{ complex form of solution } x = \frac{Fe^{i\omega t}}{i\omega [R_{m} + i(\omega m - s/\omega)]} = \frac{f}{i\omega Z_{m}}$$
Actual displacement :  $x(t) = \operatorname{Re}\left[\frac{f}{i\omega Z_{m}}\right] = \frac{Fe^{i\omega t}}{i\omega |Z_{m}|e^{i\Theta}} = \frac{-iFe^{i(\omega t - \Theta)}}{\omega |Z_{m}|} = \frac{F\sin(\omega t - \Theta)}{\omega |Z_{m}|}$ 

$$\left(\operatorname{Recall:} |Z_{m}| = \sqrt{R_{m}^{2} + (\omega m - s/\omega)^{2}}, \quad \Theta = \tan^{-1}\frac{X_{m}}{Z_{m}}\right)$$
Speed :  $u(t) = \operatorname{Re}\left[\frac{f(t)}{Z_{m}}\right] = \frac{F\cos(\omega t - \Theta)}{|Z_{m}|} \Rightarrow \frac{F}{|Z_{m}|} = \operatorname{Amplitude of } u(t) = \max \text{ speed}$ 

 Notice: find the (complex) impedance and you have solved the differential equation of motion

#### Transient response

- Transient response of driven, damped oscillator: Full solution includes
  - Transient term that depends on initial conditions, and damping
  - Steady-state term that depends on driving force magnitude, and  $\boldsymbol{\omega}$

General complex solution  $x = Ae^{-\beta t}e^{i\omega}d^{t} + \frac{Fe^{i\omega t}}{i\omega Z_{m}}$ With real part  $x = Ae^{-\beta t}\cos(\omega_{d}t + \phi) + \frac{F}{\omega Z_{m}}\sin(\omega t - \phi)$ 

We get the real constants  $A, \phi$  from initial conditions;

$$\omega_{d} = \sqrt{\omega_{0}^{2} - \beta^{2}}; \quad \beta = R_{m}/2m$$
For  $x = u = 0$  at  $t = 0$ , and  $\beta << \omega$ , we get
$$A = \frac{F}{Z_{m}^{2}} \sqrt{\frac{X_{m}^{2} + \frac{R_{m}^{2}}{\omega_{d}^{2}} + \frac{R_{m}^{2}}{\omega_{d}^{2}}}, \text{ and } \phi = \tan^{-1} \left(\frac{\omega R_{m}}{\omega_{d} X_{m}}\right)^{-0.5}$$

$$(10)$$

### Resonance

- Resonance in a driven, damped oscillator:
  - Resonant frequency = f at which reactance X goes to 0 (Z=R)
    - Minimum of Z  $\rightarrow$  maximum amplitude of speed u

At resonance 
$$\omega_0 m = s / \omega_0 \rightarrow \omega_0^2 = s / m$$
  
 $u_{res} = \frac{F \cos(\omega_0 t)}{R_m} \rightarrow \text{Amplitude } \frac{F}{R_m} = \text{max speed}$   
displacement:  $x(t) = \frac{F \sin(\omega_0 t)}{\omega_0 R_m}$ 

 $\omega_0$  is *not* the max displacement frequency; max displacement occurs for  $\omega$  such that  $\omega \left[ R_m^2 + \left( \omega m - s / \omega \right)^2 \right] = \text{minimum} \rightarrow \omega_{\max - x} = \sqrt{\omega_0^2 - 2\beta^2}$ (...homework exercise)

### Resonance

- Resonance in a driven oscillator:
  - Identical damped oscillators, all with natural frequency  $f_0=1$ .
  - Harmonic driving force  $F=F_0\cos(2 \pi f t)$  is applied
  - The driving frequencies of the applied forces are (matching colors)

f1=0.4, f2=1.01, f3=1.6



www.acs.psu.edu/drussell/

### Resonance

Time plots for oscillators (matching colors) f1=0.4, f2=1.01, f3=1.6





t axis on these plots seems to be 1 sec =  $\sim$ 6 units

# Displacement amplitude vs damping $\beta$ and $\omega/\omega_0$

• Resonance in a driven oscillator: frequency for max displacement



# Phase shift vs ( $\omega / \omega_0$ )



• Resonance amplitude and phase shift in a driven oscillator

Watch <a href="https://www.youtube.com/watch?v=aZNnwQ8HJHU">https://www.youtube.com/watch?v=aZNnwQ8HJHU</a>

## Resonant behavior and Q

• Sharpness of resonance peak is described by the 'quality factor' Q

 $Q = \frac{\omega_0}{\omega_U - \omega_L}$ ,  $\omega_U$ ,  $\omega_L$  are points above and below resonance

where average power drops to 1/2 the resonance peak value.

This happens when 
$$Z_m^2 = 2R_m^2 \rightarrow X_m = \omega m - s / \omega = \pm R_m$$
  
 $\omega_U m - s / \omega_U = R_m$ , and  $\omega_L m - s / \omega_L = -R_m \rightarrow \omega_U - \omega_L = R_m / m$   
So  $Q = \frac{\omega_0 m}{R_m} = \frac{\sqrt{mk}}{R_m} = \omega_0 (\tau / 2) = (2\pi / T)(\tau / 2) = \pi \left(\frac{\tau}{T}\right)$ 

So

- Q is directly proportional to decay time of the undriven oscillator au
- Q is related to (energy stored)/(energy lost) ~ X/R

# Resonant behavior and Q

- Q is dimensionless (ratio of times or energies)
- Low resistance (dissipation)  $\rightarrow$  High Q



#### Displacement amplitude vs time for resonance: human ear

 Example of resonance in a driven oscillator: Amplitude vs t, for natural frequency 1 kHz and Q = 12.7 (values reflecting those of the cochlea). a = delay before start, b = resonance build-up time

The oscillator takes  $Q/\pi$  cycles (~4 cycles) to reach the half-power amplitude of 0.707 and Q cycles to reach the 96% criterion. - *A. Bell, PLoS One* 7(11):e47918, 2012



# Stiffness, Resistance, Mass dominance

Often want some response to be 'flat' over a range of frequencies
 Stiffness-controlled system

 $s/\omega >> \omega \text{ m and } R_m \rightarrow x(t) \sim (F/s) \cos(\omega t)$ 

- Amplitude of *displacement* ~ independent of  $\omega$
- Resistance-controlled system

 $R_m >> X_m$  and  $R_m \rightarrow x \sim (F/\omega R_m) \sin(\omega t), u \sim (F/R_m) \cos(\omega t)$ 

- Amplitude of *speed* ~ independent of  $\omega$
- Mass-controlled system

ω m >> s/ω and  $R_m \rightarrow x \sim (F/ω^2 R_m) cos(ωt)$ ,  $u \sim (F/ωR_m) sin(ωt)$ 

- Neither amplitude of u or x is independent of  $\omega$  (but amplitude of *acceleration* is)
- Driven oscillators are
  - stiffness-controlled for  $\omega \ll \omega_0$
  - Resistance-controlled for  $\omega \sim \omega_0$
  - mass-controlled for  $\omega >> \omega_0$

# Discussion of resonance wouldn't be complete...

• ...without the Tacoma Narrows Bridge 1940 https://www.youtube.com/watch?v=XggxeuFDaDU

# Reminder

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