

Solutions for Homework set 1 – chapters 1–5 in Kinsler

1. (a)  $\mathbf{AB} = AB \exp[j(2\omega t + \theta + \phi)]$  and  $\text{Re}\{\mathbf{AB}\} = \underline{AB \cos(2\omega t + \theta + \phi)}$   
 (b)  $\mathbf{A/B} = (A/B) \exp[j(\theta - \phi)]$  and  $\text{Re}\{\mathbf{A/B}\} = \underline{(A/B) \cos(\theta - \phi)}$   
 (c)  $\text{Re}\{\mathbf{A}\} \text{Re}\{\mathbf{B}\} = \underline{AB \cos(\omega t + \theta) \cos(\omega t + \phi)}$   
 (d) From (a), phase =  $\underline{2\omega t + \theta + \phi}$   
 (e) From (b), phase =  $\underline{\theta - \phi}$

2.  $m = 0.5 \text{ kg}$     $m' = 0.2 \text{ kg}$     $\tau = 1 \text{ s}$     $g = 9.8 \text{ m/s}^2$     $\Delta x = 0.04 \text{ m}$

$$\Delta F = s' \Delta x = m' g$$

$$s = 0.2 \cdot 9.8 / 0.04 = 49 \text{ N/m}$$

$$\omega_0 = \sqrt{s/m} = \sqrt{49/0.5} = 9.90 \text{ rad/s}$$

$$\beta = 1/\tau = 1 \text{ s}^{-1}$$

$$R_m = 2m\beta = \underline{1.0 \text{ kg/s}} \quad \text{or} \quad \underline{1.0 \text{ N}\cdot\text{s/m}}$$

$$\omega_d = \sqrt{\omega_0^2 - \beta^2} = \sqrt{98 - 1} = \underline{9.85 \text{ rad/s}} \quad \text{or, alternatively,}$$

$$\omega_d = \omega_0 \sqrt{1 - (\beta/\omega_0)^2} \approx \omega_0 \left[ 1 - \frac{1}{2} (\beta/\omega_0)^2 \right] \approx 9.90 [1 - 1/(2 \cdot 9.8)]$$

$$\approx 9.90(1 - 0.05) \approx \underline{9.85 \text{ rad/s}}$$

$$x = A e^{-\beta t} \cos(\omega_d t + \phi)$$

$$\dot{x} = -A \omega_d e^{-\beta t} \sin(\omega_d t + \phi) - A \beta e^{-\beta t} \cos(\omega_d t + \phi)$$

$$x(0) = A \cos \phi = 0.04$$

$$\dot{x}(0) = -A \omega_d \sin \phi - \beta A \cos \phi = 0$$

$$\therefore \tan \phi = -\beta/\omega_d = -0.1015$$

$$\phi = \underline{-5.8^\circ}$$

$$A = 0.04/\cos \phi = \underline{0.0402 \text{ m}}$$

3.  $f = F \sin \omega_0 t \quad t \geq 0 \quad \text{and} \quad \beta \ll \omega_0$

$$\mathbf{f} = -jF e^{j\omega_0 t}$$

In this approximation  $\omega_d = \omega_0 \sqrt{1 - (\beta/\omega_0)^2} \approx \omega_0 - \frac{1}{2} \beta^2/\omega_0$

The steady state (homogeneous) solution is  $\mathbf{u}_h = \mathbf{f}/\mathbf{Z}_m = j\omega_0 \mathbf{x}_h$  whence

$$\mathbf{x}_h = \frac{1}{j\omega_0} \frac{-jF e^{j\omega_0 t}}{\mathbf{Z}_m} = -\frac{F}{\omega_0 \mathbf{Z}_m} e^{j\omega_0 t} \quad \text{But} \quad \mathbf{Z}_m = R_m \quad \text{for} \quad \omega = \omega_0 \quad \text{so}$$

$$x_h = -\frac{F}{\omega_0 R_m} \cos \omega_0 t$$

Substituting into (1.8.1) yields the complete solution

$$x = A e^{-\beta t} \cos(\omega_d t + \phi) - \frac{F}{\omega_0 R_m} \cos \omega_0 t \quad \text{with constants to be determined}$$

Applying the initial conditions  $x(0) = 0$  and  $\left. \frac{dx}{dt} \right|_{t=0} = 0$  gives

$$A \cos \phi - \frac{F}{\omega_0 R_m} = 0$$

$$-\beta A \cos \phi - \omega_d A \sin \phi = 0$$

From the second equation  $\frac{\sin \phi}{\cos \phi} = -\frac{\beta}{\omega_d}$  but  $\frac{\beta}{\omega_d} \ll 1$  so that  $\phi \approx -\frac{\beta}{\omega_d}$

and then the first gives  $A \approx \frac{F}{\omega_0 R_m \cos(\beta/\omega_d)} \approx \frac{F}{\omega_0 R_m}$

Substitution into the complete solution gives

$$\begin{aligned} x &\approx \frac{F}{\omega_0 R_m} \left[ e^{-\beta t} \cos(\omega_d t - \beta/\omega_d) - \cos \omega_0 t \right] \\ &\approx \frac{F}{\omega_0 R_m} \left[ e^{-\beta t} \left( \cos \omega_d t + \frac{\beta}{\omega_d} \sin \omega_d t \right) - \cos \omega_0 t \right] \end{aligned}$$

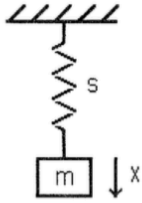
Now for  $\omega_0 t < 1$  with  $\beta/\omega_0 \ll 1$  this becomes

$$x \approx \frac{F}{\omega_0 R_m} (e^{-\beta t} - 1) \cos \omega_0 t$$

and for  $\omega_0 t \geq 1$  the  $\exp(-\beta t)$  makes the first term in the complete solution negligibly small, so the above approximation is valid for all  $t$ .

5. 
$$U(t) = \int_{-\infty}^{\infty} \frac{\delta(\omega - \omega_0)}{Z(\omega)} F e^{j\omega t} d\omega = \frac{F}{Z} e^{j\omega_0 t}$$

6.



$$f = mg \cdot 1(t)$$

$$Z(\omega) = j(\omega m - s/\omega)$$

$$\omega_0 = (s/m)^{1/2}$$

With the help of Table 1.15.1, we have

$$G(\omega) = \frac{mg}{2\pi} \frac{1}{j\omega}$$

Then, again using Table 1.15.1

$$\begin{aligned} U(t) &= \int_{-\infty}^{\infty} \frac{mg}{2\pi} \frac{1}{j\omega} \frac{e^{j\omega t}}{j(\omega m - s/\omega)} dt = \frac{-mg}{2\pi m} \int_{-\infty}^{\infty} \frac{e^{j\omega t}}{\omega^2 - \omega_0^2} dt \\ &= g \int_{-\infty}^{\infty} \frac{1}{2\pi} \frac{1}{\omega_0^2 - \omega^2} e^{j\omega t} dt = \frac{g}{\omega_0} \sin \omega_0 t \cdot 1(t) \end{aligned}$$

and integration over time yields the displacement

$$X(t) = \int_0^t U(t) dt = \frac{g}{\omega_0} \frac{-1}{\omega_0} \cos \omega_0 t \Big|_0^t = \frac{mg}{s} (1 - \cos \omega_0 t)$$

8.  $y = 4 \cos(3t - 2x)$       $\rho_L = 0.1 \text{ g/cm}$
- (a)  $A = 4 \text{ cm}$       $c = \omega/k = 3/2 = 1.5 \text{ cm}$       $f = \omega/2\pi = 3/2\pi = 0.48 \text{ Hz}$   
 $\lambda = 2\pi/k = \pi = 3.1 \text{ cm}$       $k = 2 \text{ cm}^{-1}$
- (b)  $u = \partial y/\partial t = -12 \sin(3t - 2x)$      so  $u(0,0) = 0 \text{ m/s}$
9.  $m_L = 0.2 \text{ kg}$ ,  $m_s = 0.05 \text{ kg}$ ,  $L = 1.0 \text{ m}$ , so that  $\rho_L = 0.05 \text{ kg/m}$
- (a)  $c^2 = T/\rho_L = 0.2 \cdot 9.8/0.05 = 39.2$      so  $c = 6.26 \text{ m/s}$
- (b)  $\cot kL = \frac{m_L}{m_s} kL = \frac{0.2}{0.05 \cdot 1} kL = 4kL$   
By trial and error, or tables,  $kL = 0.48$      so  $f = 0.48c/2\pi L = 0.48 \text{ Hz}$   
The first overtone has  $kL = 3.219$      so  $f = 3.21 \text{ Hz}$
- (c)  $y = A \sin kL e^{j\omega t}$  from which we obtain  $\frac{A}{|y(L)|} = \frac{1}{|\sin 3.219|} = 12.9$
- 
10.  $y = 2 \sin(x/5) \cos 3t$  with all units in cgs
- (a)  $c = \omega/k = 3/(1/5) = 15 \text{ cm/s}$   
 $f = 3/(2\pi) = 0.48 \text{ Hz}$   
 $k = 1/5 = 0.2 \text{ cm}^{-1}$
- (b)  $x = L/2 = 31.4/2 \approx 5\pi$   
 $y = 2 \sin \pi \cos \omega t = 0$   
amplitude =  $0 \text{ cm}$      speed =  $0 \text{ cm/s}$   
 $x = L/4 = 31.4/4 \approx 5\pi/2$   
 $y = 2 \cos 3t = 0$   
amplitude =  $2 \text{ cm}$      speed =  $6 \text{ cm/s}$
- (c)  $\frac{dE}{dx} = \frac{1}{2} \rho_L \left[ c^2 \left( \frac{\partial y}{\partial x} \right)^2 + \left( \frac{\partial y}{\partial t} \right)^2 \right]$   
 $= \frac{1}{2} \rho_L \left( \frac{225 \cdot 4}{25} \cos^2 \frac{x}{5} \cos^2 3t + 36 \sin^2 \frac{x}{5} \sin^2 3t \right)$   
 $= 1.8 \left( \cos^2 \frac{x}{5} \cos^2 3t + \sin^2 \frac{x}{5} \sin^2 3t \right)$   
at  $x = L/2 = 5\pi$       $\frac{dE}{dx} = -1.8 \cos^2 3t$   
at  $x = L/4 = 5\pi/2$       $\frac{dE}{dx} = 1.8 \sin^2 3t$

10. cont'd (d) Since the total energy remains constant, we can choose any time for the integration over  $x$ . For convenience, choose  $3t = \pi/2$ .

$$\begin{aligned}
 E &= 1.8 \int_0^L \sin^2 \frac{x}{5} dx = 1.8 \int_0^{10\pi} \sin^2 \frac{x}{5} dx \\
 &= 1.8 \cdot 5 \left[ \frac{1}{2} \frac{x}{5} - \frac{1}{4} \sin \frac{2x}{5} \right]_0^{10\pi} = 9\pi \\
 &= 28.3 \text{ ergs} = \underline{2.83 \times 10^{-6} \text{ J}}
 \end{aligned}$$

11.  $S = 1 \times 10^{-4} \text{ m}^2$  free at  $x = 0$   
 $L = 0.25 \text{ m}$  loaded with 0.15 kg at  $L$   
 $m = 0.15 \text{ kg}$

$$m_b = 7700 \times 10^{-4} \cdot 0.25 = 0.1925 \text{ kg}$$

$$(a) \quad \tan kL = -\frac{m}{m_b} kL = -0.78 kL \quad \text{so that} \quad kL = 2.12 = \frac{2\pi f}{c} L$$

$$f = 2.12 \frac{5050}{2\pi \cdot 0.25} = \underline{6.8 \text{ kHz}}$$

- (b)  $\xi = 2A \cos kx e^{j\omega t}$  and clamp the bar where  $\cos kx = 0$

$$kx = \frac{\pi}{2} \quad x = \frac{\pi \cdot 0.25}{2 \cdot 2.12} = \underline{0.185 \text{ m}}$$

$$(c) \quad \frac{\cos 0}{\cos kL} = \frac{1}{\cos 2.12} = \underline{1.91}$$

$$(d) \quad \tan kL = -0.78 kL \quad kL = 4.965 \quad f = 6800 \frac{4.965}{2.12} = \underline{15.9 \text{ kHz}}$$

Alternate 11. A steel bar of cross section  $0.0001 \text{ m}^2$  and  $0.25 \text{ m}$  length is clamped at both ends.

a) what is its fundamental frequency for longitudinal vibrations? b) what is the fundamental frequency for the same bar but free at both ends?

$c = \sqrt{Y/\rho}$ ; for common steel we can take  $Y = 200 \text{ GPa} = 2 \times 10^{11} \text{ Pa}$ ,  
density =  $7900 \text{ kg/m}^3$ , so  $c = \sqrt{2 \times 10^{11} / 7900} = 5030 \text{ m/s}$ .

For longitudinal waves, cross-section does not matter as long as bar is "slender" ( $L \gg$  diameter) as in this case. For ends clamped,

$$f_1 = c / 2L = 5030 \text{ m/s} / 0.5 \text{ m} = 10 \text{ kHz}$$

for ends free, result is same - difference is that clamped ends must be nodes, free ends must be anti-nodes, but fundamental  $f$  has  $L = \lambda/2$ .

12.  $\omega c \kappa = [\text{rad/s}][\text{m/s}][\text{m}] = [\text{m}]^2/[\text{s}]^2$  so  $\sqrt{\omega c \kappa}$  has the dimensions of speed

$$v = \sqrt{\omega c \kappa} \quad \text{and if } v = c \quad \text{then } \omega = \frac{c}{\kappa}$$

A circular rod of radius  $a$  has  $\kappa = a/2$  so that  $f = c/\pi a$  and for this aluminum

$$\text{rod } f = \frac{5.15 \times 10^3}{\pi \cdot 0.005} = \underline{328 \text{ kHz}}$$

13. Let  $L_x = a$  and  $L_y = 2a$  Then  $f_{nm} = \frac{c}{2} \sqrt{\left(\frac{n}{a}\right)^2 + \left(\frac{m}{2a}\right)^2} = \frac{c}{2a} \sqrt{n^2 + \frac{m^2}{4}}$

$$\left\{ \begin{array}{ll} f_{11} = \frac{c}{2a} \sqrt{1.25} \\ f_{11}/f_{11} = \sqrt{1.25/1.25} = 1.000 & f_{21}/f_{11} = \sqrt{4.25/1.25} = 1.844 \\ f_{12}/f_{11} = \sqrt{2/1.25} = 1.265 & f_{14}/f_{11} = \sqrt{5/1.25} = 2.000 \\ f_{13}/f_{11} = \sqrt{3.25/1.25} = 1.612 & f_{22}/f_{11} = \sqrt{5/1.25} = 2.000 \end{array} \right.$$

14.  $a = 2.0 \text{ cm}$   $d = 0.02 \text{ cm}$   $\rho = 7700 \text{ kg/m}^3$

$$Y = 19.5 \times 10^{10} \text{ N/m}^2 \quad \sigma = 0.28$$

$$(a) \quad f_1 = 0.47 \frac{d}{a^2} \sqrt{\frac{Y}{\rho(1-\sigma^2)}} = 0.47 \frac{2 \times 10^{-4}}{0.02^2} \sqrt{\frac{19.5 \times 10^{10}}{7700 \cdot (1-0.28^2)}} = \underline{1230 \text{ kHz}}$$

$$(b) \quad \text{If } d = 0.04 \text{ cm} \quad \text{then } \underline{f_1 = 2460 \text{ Hz}}$$

$$(c) \quad \text{If } a = 4 \text{ cm} \quad \text{then } \underline{f_1 = 307 \text{ Hz}}$$

15.  $\mathbf{p} = \frac{A}{r} \cos kr e^{j\omega t}$  and so  $\Phi = -\frac{A}{j\omega\rho_0 r} \cos kr e^{j\omega t}$

$$(a) \quad \mathbf{u} = \nabla\Phi = \frac{\partial\Phi}{\partial r} = -j \frac{A}{\rho_0 c r} \left[ \sin kr + \frac{\cos kr}{kr} \right] e^{j\omega t}$$

$$(b) \quad \mathbf{z} = \frac{\mathbf{p}}{\mathbf{u}} = j\rho_0 c \frac{\cos kr}{\left[ \sin kr + \frac{\cos kr}{kr} \right]}$$

$$(c) \quad I(t) = pu = \frac{A}{r} \cos kr \cos \omega t \frac{A}{r \rho_0 c} \left[ \sin kr + \frac{\cos kr}{kr} \right] \sin \omega t$$

$$= \frac{\left(\frac{A}{r}\right)^2}{\rho_0 c} \cos kr \left[ \sin kr + \frac{\cos kr}{kr} \right] \cos \omega t \sin \omega t$$

$$(d) \quad \text{Because } \frac{1}{T} \int_0^T \cos \omega t \sin \omega t dt = 0 \quad \text{we have } \langle I(t) \rangle_T = \underline{I = 0}$$

16.  $P = 2 \text{ Pa}$     $f = 100 \text{ Hz}$    in air

(a)  $I = \frac{P^2}{2\rho_0 c} = \frac{2^2}{2 \cdot 415} = \underline{4.8 \times 10^{-3} \text{ W/m}^2}$

$IL = 10 \log(4.8 \times 10^{-3} / 10^{-12}) = \underline{96.8 \text{ dB re } 10^{-12} \text{ W/m}^2}$

(b)  $U/\omega = P/(\rho_0 c \omega) = 2/(415 \cdot 2\pi \cdot 100) = \underline{7.7 \times 10^{-6} \text{ m}}$

(c)  $U = P/(\rho_0 c) = 2/415 = \underline{4.82 \times 10^{-3} \text{ m/s}}$

(d)  $P_e = P/\sqrt{2} = \underline{1.41 \text{ Pa}} = 14.1 \text{ } \mu\text{bar}$

(e)  $SPL = 20 \log(14.1/0.0002) = \underline{97 \text{ dB re } 20 \text{ } \mu\text{bar}}$

17. (a)  $ML = -80 \text{ dB re } 1 \text{ V}/\mu\text{bar} = 20 \log[M/(1 \text{ V}/\mu\text{bar})]$

$M = 10^{-4} \text{ V}/\mu\text{bar} = 10^{-9} \text{ V}/\mu\text{Pa}$

$ML = 20 \log[10^{-9}/(1 \text{ V}/\mu\text{Pa})] = \underline{-180 \text{ dB re } 1 \text{ V}/\mu\text{Pa}}$

(b)  $SPL = 80 \text{ dB re } 1 \text{ } \mu\text{bar} = 20 \log(P/1 \text{ } \mu\text{bar})$

$P = 10^4 \text{ } \mu\text{bar}$

$ML = -80 = 20 \log[(V/10^4)/(1 \text{ V}/\mu\text{bar})] = 20 \log(V/10^4)$

$V = \underline{1 \text{ V}}$